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AFWAL-TR-87-3098
PART V



UNSTEADY LOW-SPEED WINDTUNNEL TEST
OF A STRAKED DELTA WING, OSCILLATING IN PITCH

PART V: POWER SPECTRAL DENSITY PLOTS OF THE OVERALL LOADS FOR
HARMONIC OSCILLATION AND THE RESPONSE OF OVERALL LOADS
TO (1-COS) INPUTS

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APRIL 1988

FINAL REPORT FOR PERIOD JUNE 1985-AUGUST 1987

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UNCLASSIFIED
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REPORT DOCUMENTATION PAGE												
1a. REPORT SECURITY CLASSIFICATION UNCLASSIFIED		1b. RESTRICTIVE MARKINGS None										
2a. SECURITY CLASSIFICATION AUTHORITY		3. DISTRIBUTION/AVAILABILITY OF REPORT Approved for public release; distribution is unlimited										
2b. DECLASSIFICATION/DOWNGRADING SCHEDULE												
4. PERFORMING ORGANIZATION REPORT NUMBER(S)		5. MONITORING ORGANIZATION REPORT NUMBER(S) AFWAL-TR-87-3098, PART V										
6a. NAME OF PERFORMING ORGANIZATION General Dynamics	6b. OFFICE SYMBOL (If applicable)	7a. NAME OF MONITORING ORGANIZATION Air Force Wright Aeronautical Laboratories Flight Dynamics Laboratory, AFWAL/FIMM										
6c. ADDRESS (City, State, and ZIP Code) P.O. Box 748 Fort Worth TX 76101		7b. ADDRESS (City, State, and ZIP Code) Wright-Patterson AFB OH 45433-6553										
8a. NAME OF FUNDING/SPONSORING ORGANIZATION	8b. OFFICE SYMBOL (If applicable)	9. PROCUREMENT INSTRUMENT IDENTIFICATION NUMBER F33615-85-C-3013										
8c. ADDRESS (City, State, and ZIP Code)		10. SOURCE OF FUNDING NUMBERS <table border="1"><tr><td>PROGRAM ELEMENT NO.</td><td>PROJECT NO.</td><td>TASK NO.</td><td>WORK UNIT ACCESSION NO.</td></tr><tr><td>62201F</td><td>2404</td><td>10</td><td>94</td></tr></table>		PROGRAM ELEMENT NO.	PROJECT NO.	TASK NO.	WORK UNIT ACCESSION NO.	62201F	2404	10	94	
PROGRAM ELEMENT NO.	PROJECT NO.	TASK NO.	WORK UNIT ACCESSION NO.									
62201F	2404	10	94									
11. TITLE (Include Security Classification) UNSTEADY LOW-SPEED WIND TUNNEL TEST OF A STRAKED DELTA WING, OSCILLATING IN PITCH, PART V: (See Reverse)												
12. PERSONAL AUTHOR(S) Cunningham, A.M., General Dynamics* (See Reverse)												
13a. TYPE OF REPORT FINAL	13b. TIME COVERED FROM Jun 85 TO Aug 87	14. DATE OF REPORT (Year, Month, Day) 1988 April	15. PAGE COUNT 292									
16. SUPPLEMENTARY NOTATION <i>for part V</i>												
17. COSATI CODES <table border="1"><tr><th>FIELD</th><th>GROUP</th><th>SUB-GROUP</th></tr><tr><td>01</td><td>01</td><td></td></tr><tr><td>20</td><td>04</td><td></td></tr></table>	FIELD	GROUP	SUB-GROUP	01	01		20	04		18. SUBJECT TERMS (Continue on reverse if necessary and identify by block number) <i>Unsteady Flow, Vortex Flow, Wind Tunnel Test. (hd)</i>		
FIELD	GROUP	SUB-GROUP										
01	01											
20	04											
19. ABSTRACT (Continue on reverse if necessary and identify by block number) Results of a wind tunnel test of an oscillating straked wing. The report provides unsteady airloads and pressure distributions for a range of incidences (-8 to 50 deg.) and amplitudes (1 to 16 deg.). The wind speed was 80 meters/second, which provided reduced frequencies up to 0.50 based on root chord. The zeroth and first harmonic as well as the continuous time history of the pressure and overall loads were measured. Flow visualization was performed for flow of 30 meters/second using a pulsating laser light sheet. In this part V, the power spectral densities for various conditions are contained in appendix A to present the relative frequency content of selected overall loads at continuous oscillating model conditions ranging from nearly linear (first harmonic dominant) to highly nonlinear (many higher harmonics) characteristics. A survey of the selected runs and their test conditions is given in table 11 of part I including the components of the balance and the corresponding plotnumbers of the spectra presented. (See Reverse)												
20. DISTRIBUTION/AVAILABILITY OF ABSTRACT <input checked="" type="checkbox"/> UNCLASSIFIED/UNLIMITED <input type="checkbox"/> SAME AS RPT. <input type="checkbox"/> DTIC USERS		21. ABSTRACT SECURITY CLASSIFICATION UNCLASSIFIED										
22a. NAME OF RESPONSIBLE INDIVIDUAL Don W. Kinsey		22b. TELEPHONE (Include Area Code) (513) 255-2481	22c. OFFICE SYMBOL AFWAL/FIMM									

11. TITLE CONTD

PART V: POWER SPECTRAL DENSITY PLOTS OF THE OVERALL LOADS FOR HARMONIC OSCILLATION AND THE RESPONSE OF OVERALL LOADS TO (1-COS) INPUTS

12. PERSONAL AUTHOR(S) CONTD

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Retel, A.P., " " " "
Zwaan, R.J., " " " "

19. ABSTRACT CONTD

are given

Appendix B contains the time history plots of incidence and all air loads for (1-cos) pitch pulses that simulate transient aircraft maneuvers. Also included are half pulse data which represent a pitch-up and hold at a higher angle of attack as well as a pitch-down and hold at a lower angle of attack. A survey of the test conditions and their runnumbers is given in table 12 of part I. All (1-cos) pitch pulse runs were conducted three times and one of the three runs was chosen for presentation. To give an idea of the reproducibility plots for all three runs of the balance components vs. incidence for two test conditions are also enclosed at the end.

Keywords: → to file 18

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FOREWORD

This report summarizes the results of the windtunnel test of an oscillating straked wing conducted under a cooperative program of research between General Dynamics Fort Worth Division, Fort Worth, Texas, and the National Aerospace Laboratory (NLR), The Netherlands. The model and support system was designed and fabricated at NLR under a separate program with General Dynamics and NLR funding. The test preparation, windtunnel test and reporting were performed at NLR under Air Force Contract F33615-85-C-3013, for the Flight Dynamics Laboratory of the Air Force Wright Aeronautical Laboratories, Wright-Patterson Air Force Base, Ohio. The work was administered by Mr. D.W. Kinsey of the Aeromechanics Division (AFWAL/FIM). Additional technical monitoring support was provided by Mr. T. Cord of the Flight Control Division (AFWAL/FIG).

The program manager and principal investigator was Dr. A.M. Cunningham Jr. at General Dynamics and Mr. R.G. den Boer was the principal investigator at NLR. Mr. den Boer was assisted by the following NLR specialists: C.S.G. Dogger, E.G.M. Geurts, A.J. Persoon, A.P. Retel and R.J. Zwaan.

This report consists of six parts. Part I presents a general description of the model and test program and a discussion of the results. Part II contains the steady pressure distribution plots and the major part of the zeroth and first order harmonic unsteady pressure distribution plots. Part III contains the remainder of the unsteady pressure distribution plots and plots of the steady and the zeroth and first order harmonic unsteady overall loads. Part IV contains time history plots of the unsteady pressures and overall loads. Part V contains power spectral density plots of the overall loads at harmonic oscillation and time history plots of overall loads for (1-cos) model motions. Part VI contains results of the flow visualization program.

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LIST OF SYMBOLS

ALPHA, α	wing incidence	(deg)
C1	wing rolling moment coefficient	
Cm	wing pitching moment coefficient	
	ref. axis = rotation axis x/cr = 73.27 %	
Cn	wing yawing moment coefficient	
CN	wing normal force coefficient	
cr	root chord (cr = 0.7855)	(m)
CT	wing tangential force coefficient	
CY	wing side force coefficient	
DALPHA, da	harmonic oscillation: amplitude of unsteady wing incidence (1-cos) inputs: magnitude of wing incidence variation	(deg, rad)
l	wing rolling moment (figure 1, part I)	(Nm)
m	wing pitching moment (figure 1, part I)	
	ref. axis x/cr = 73.27 %	(Nm)
n	wing yawing moment (figure 1, part I)	(Nm)
N	wing normal force (figure 1, part I)	(Nm)
RUN	run number	
t	time	(s)
T	wing tangential force (figure 1, part I)	(N)
T	harmonic oscillation: period of one oscillation (1-cos) input: duration of (1-cos) input	(s)
Y	wing side force (figure 1, part I)	(N)

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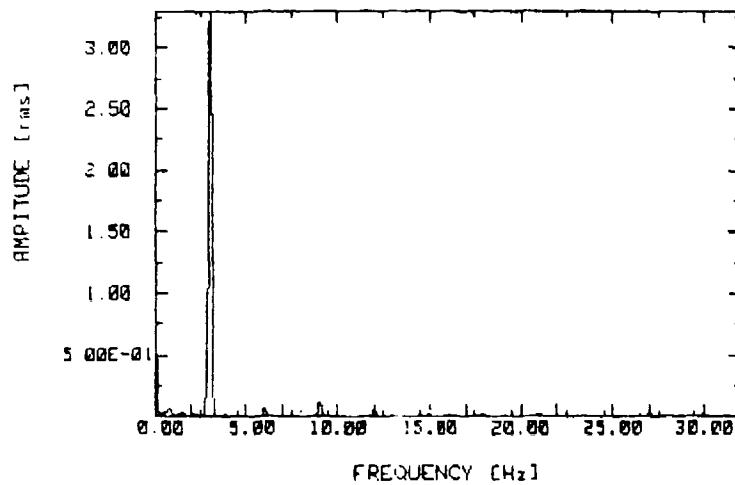
α , ALPHA	wing incidence	(deg)
da, DALPHA	harmonic oscillation: amplitude of unsteady wing incidence (1-cos) input: magnitude of wing incidence variation	(deg, rad)

SUBSCRIPT

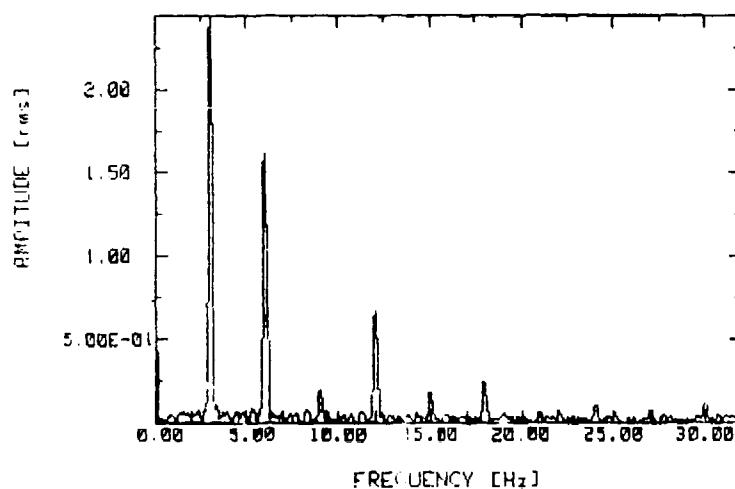
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APPENDIX A
POWER SPECTRAL DENSITY PLOTS OF OVERALL LOADS

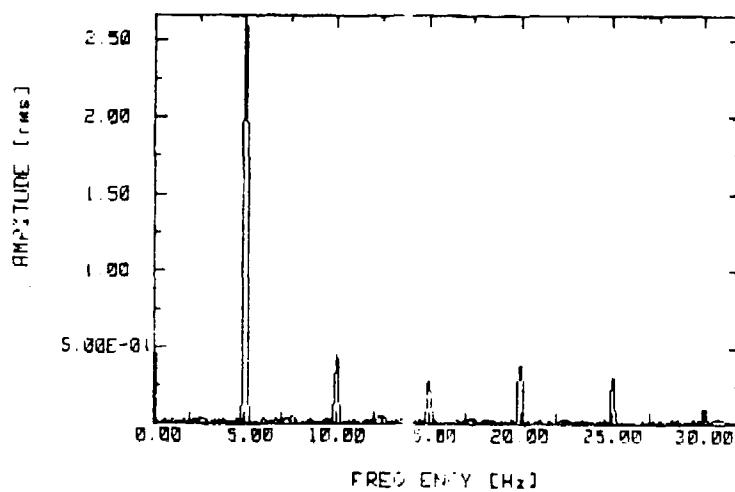
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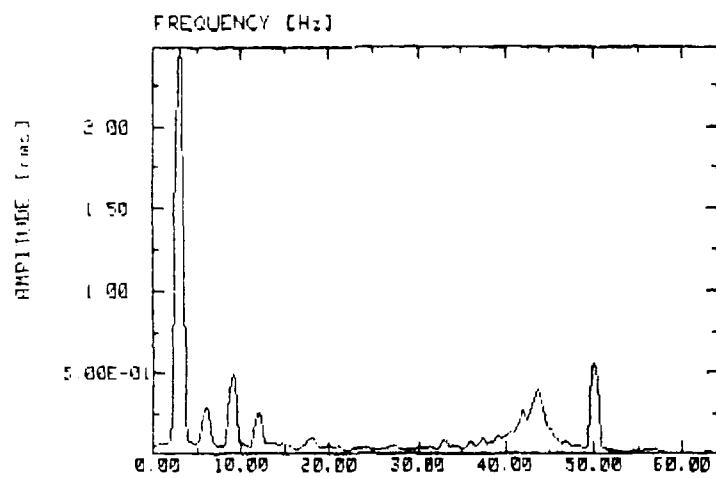


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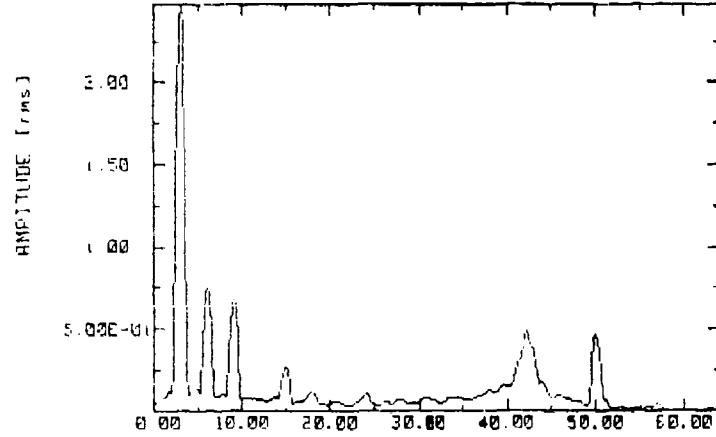


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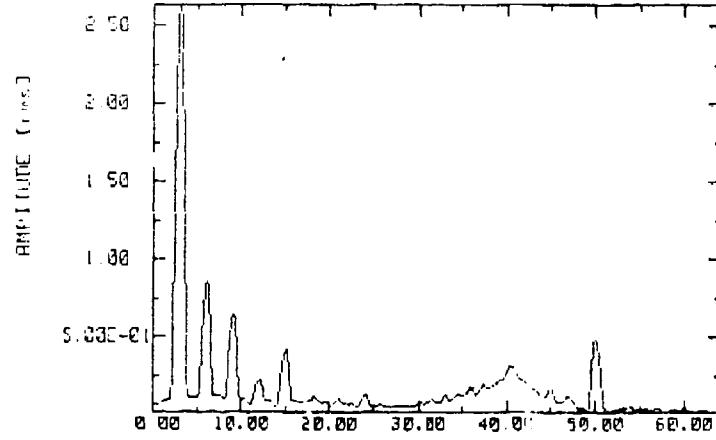




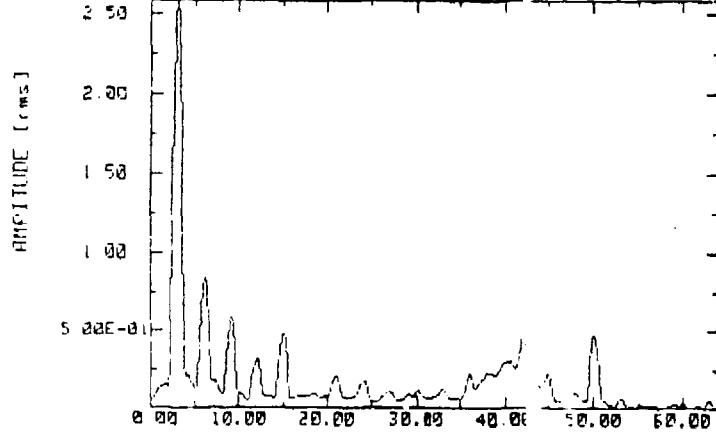
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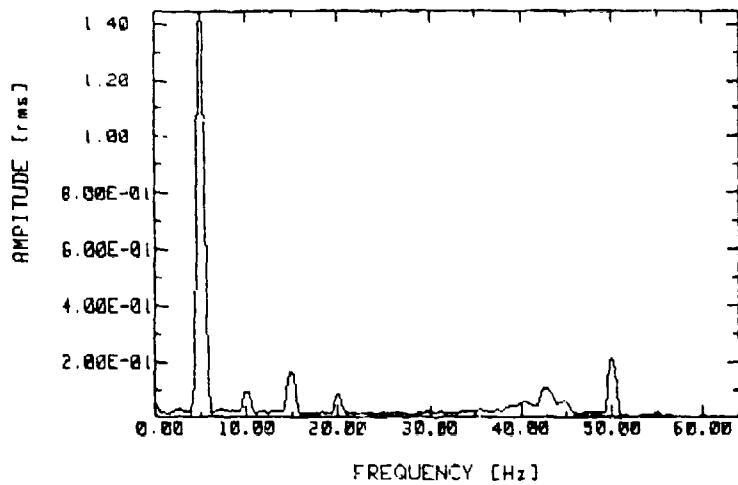


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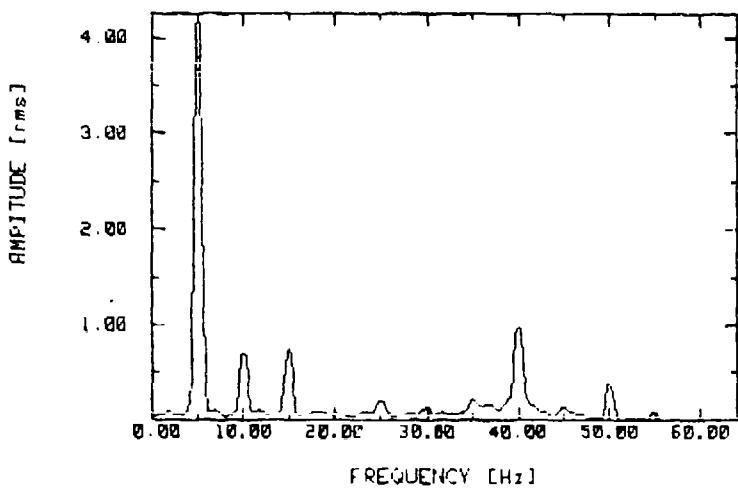


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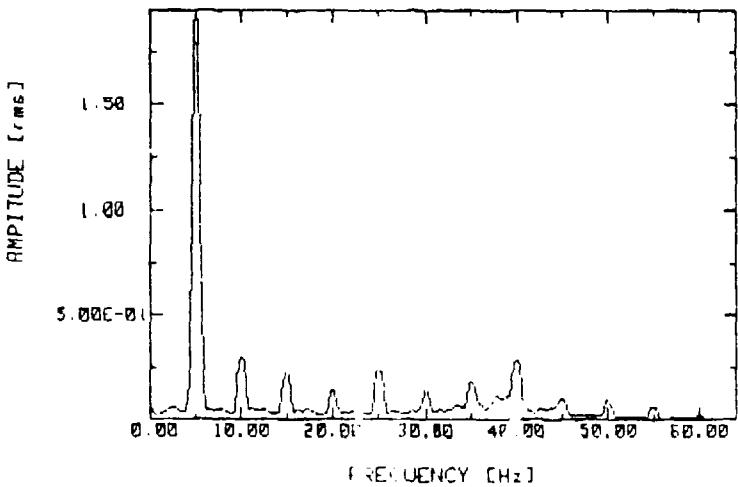
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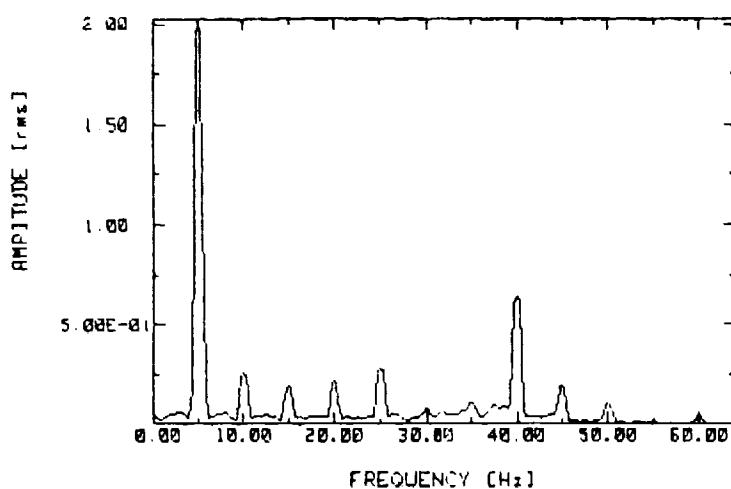


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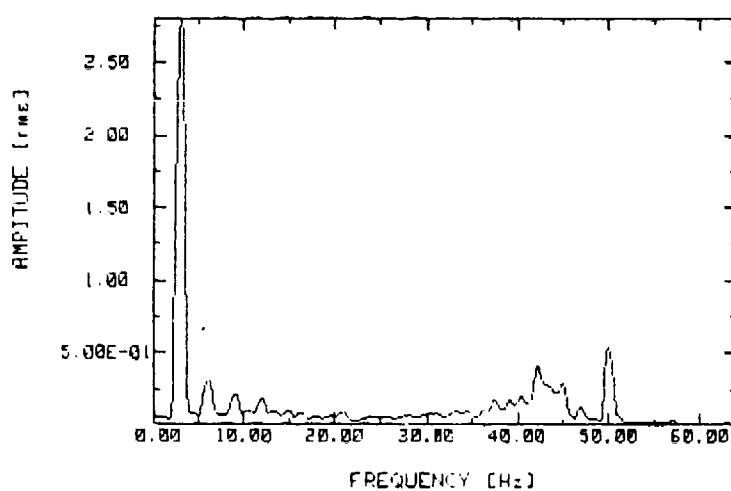
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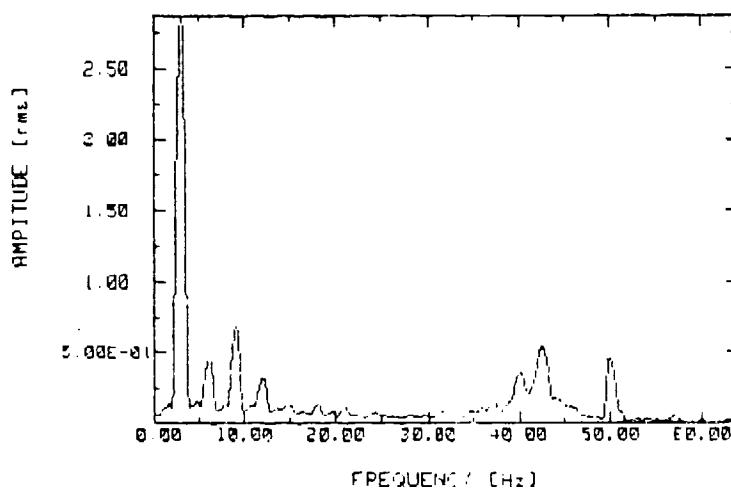
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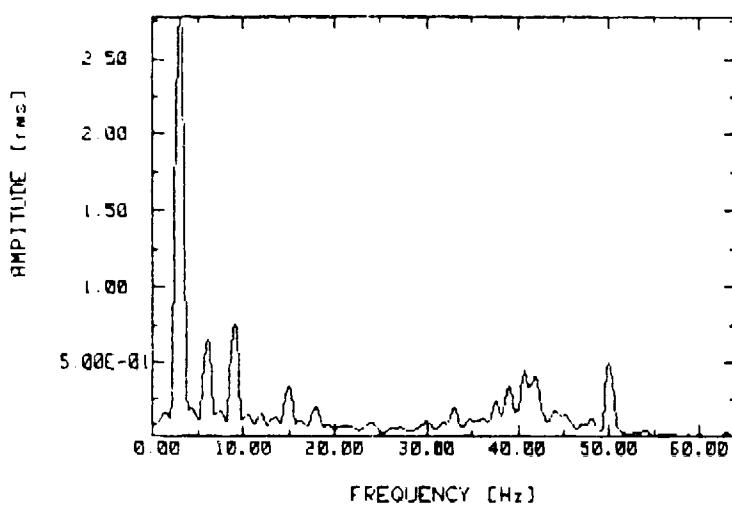


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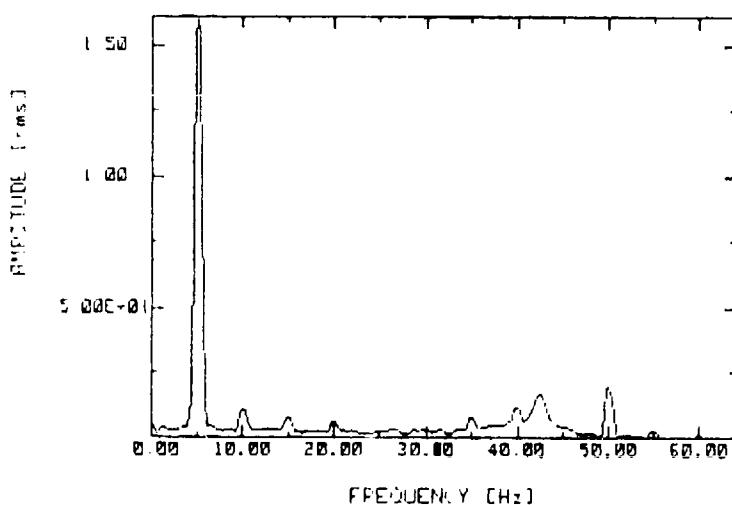
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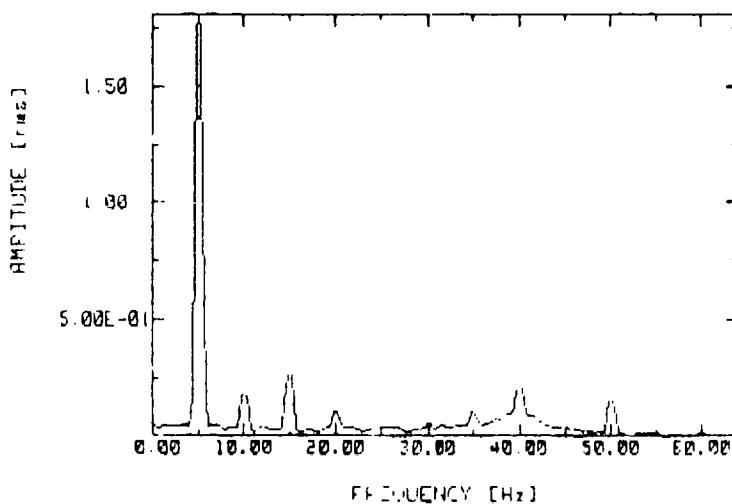
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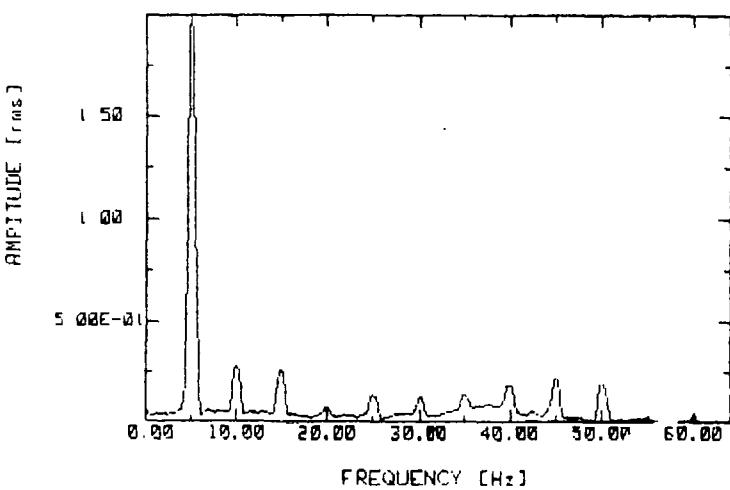
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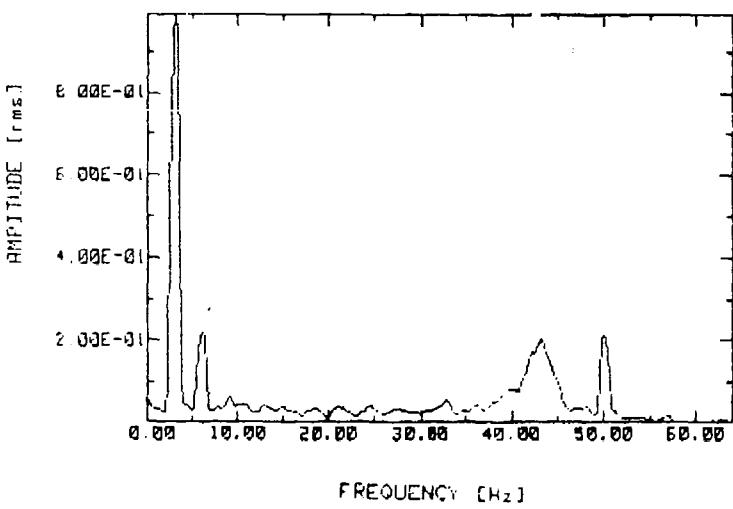
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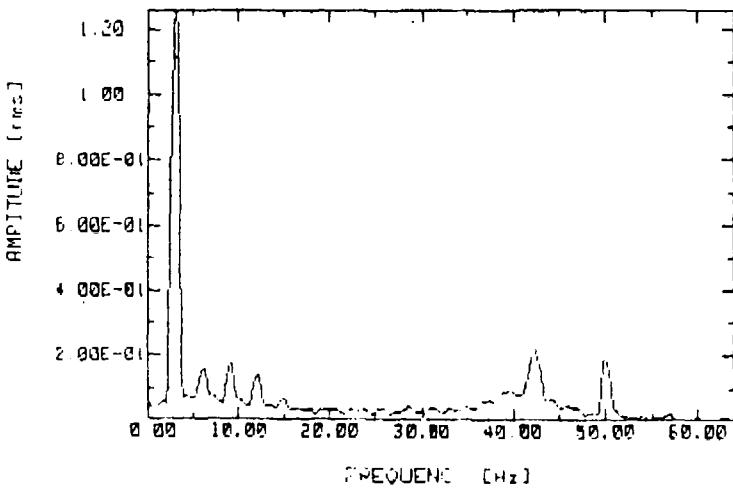
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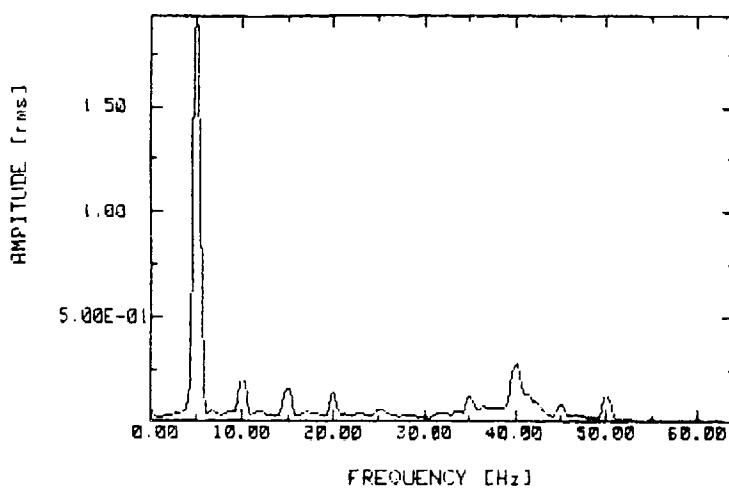
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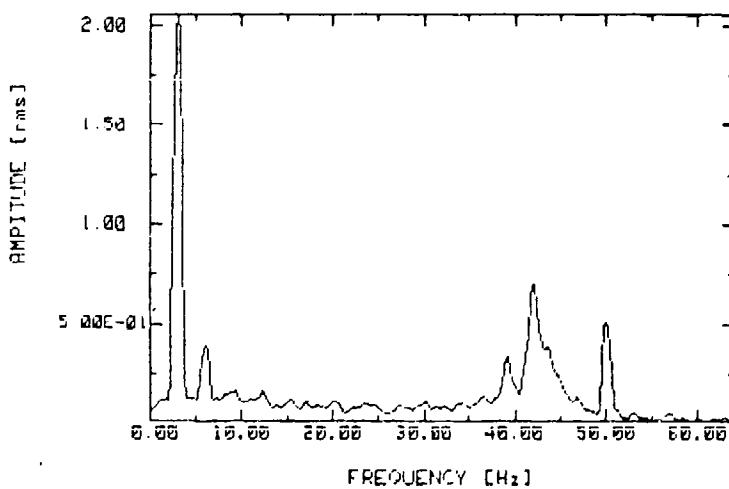
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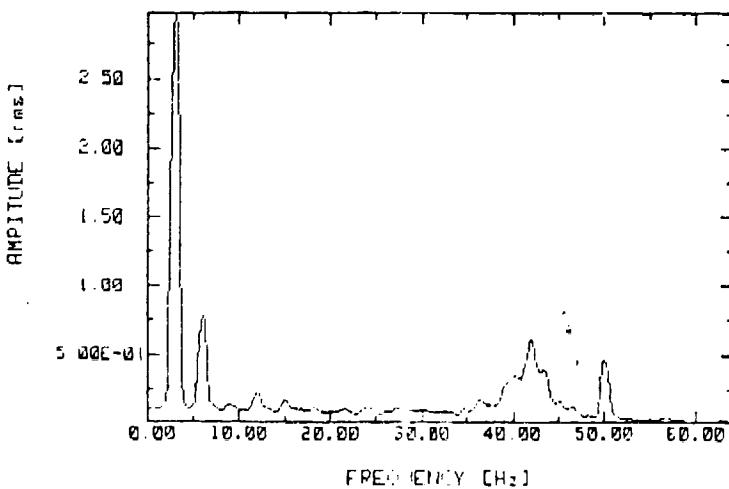
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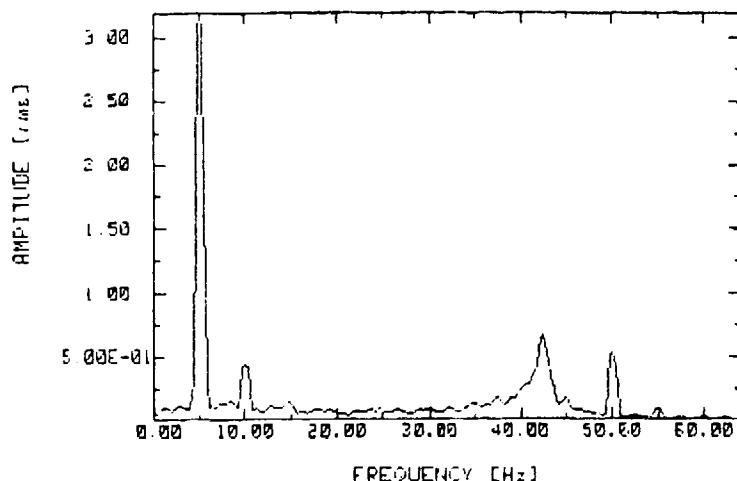


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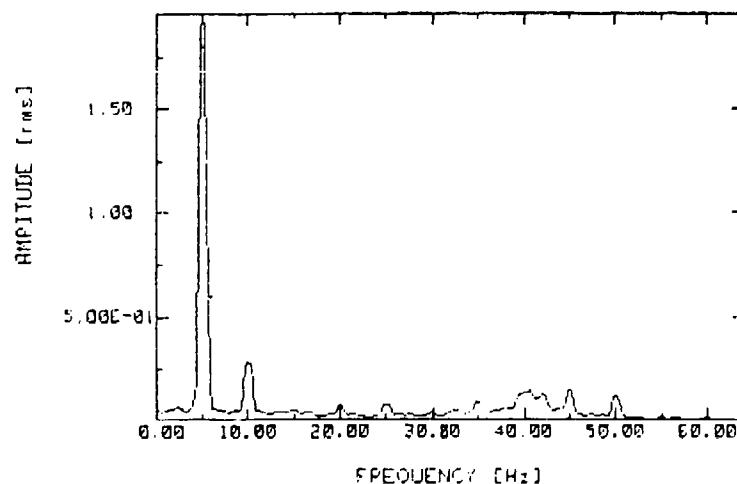
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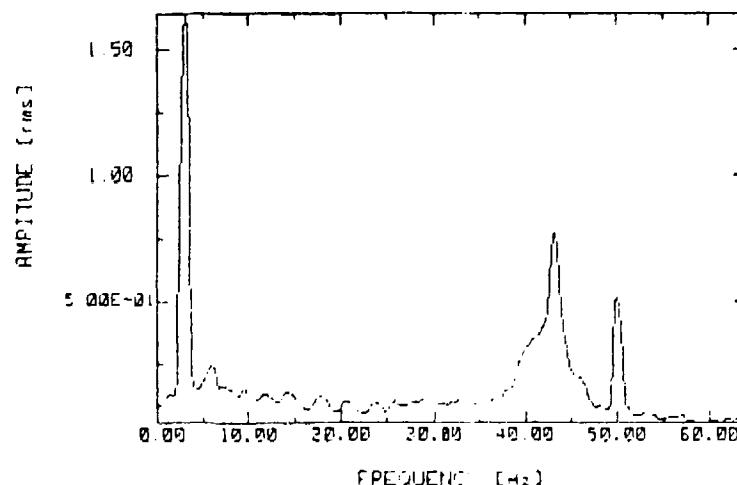
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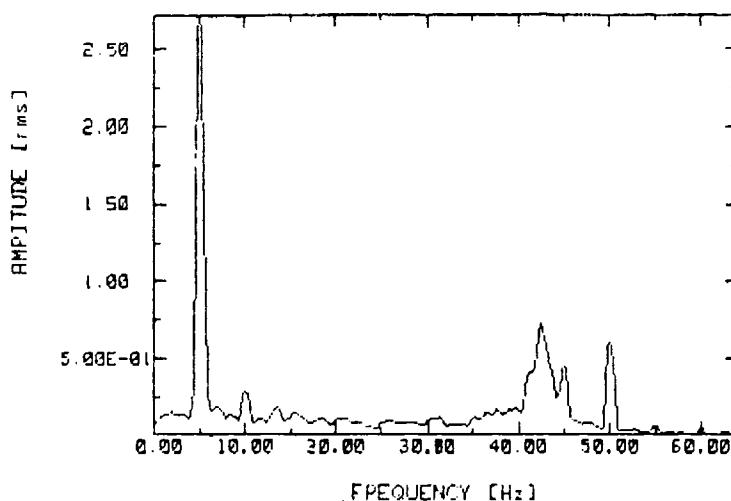


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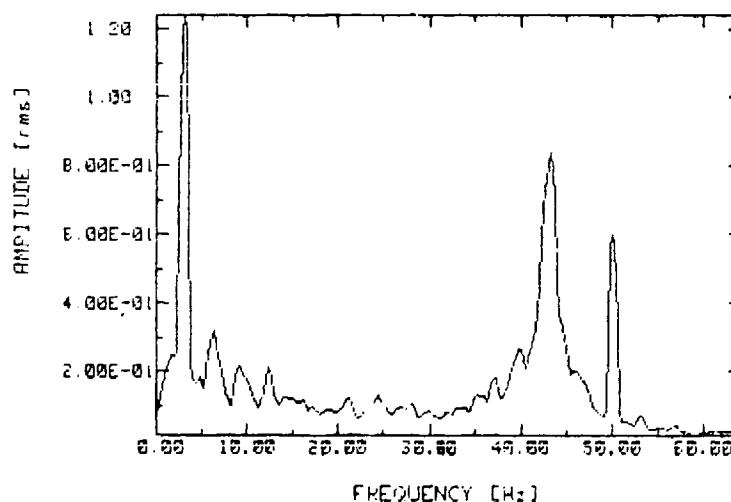
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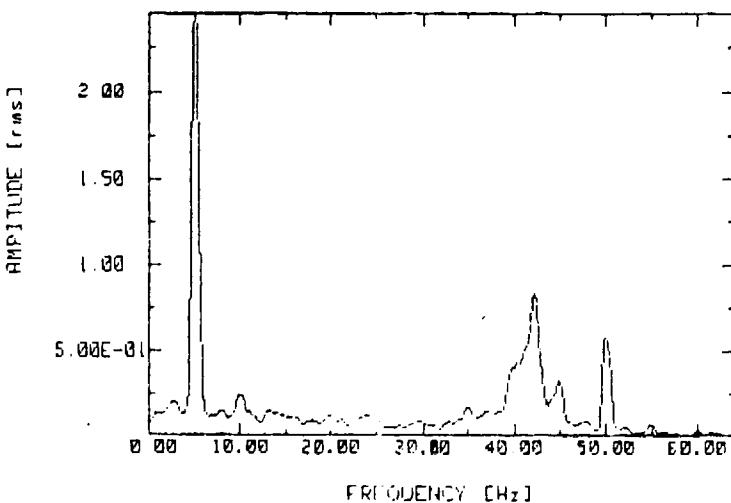
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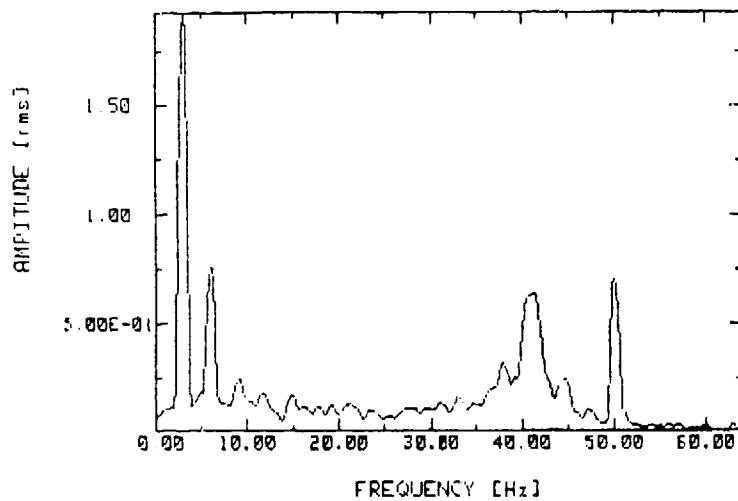
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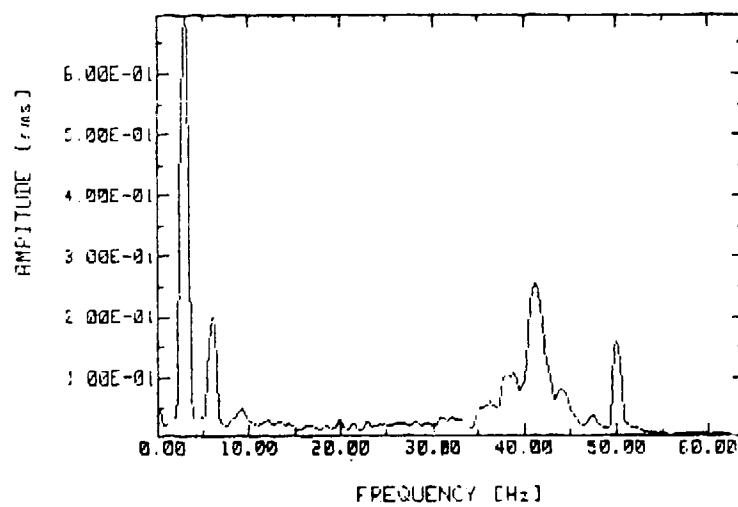
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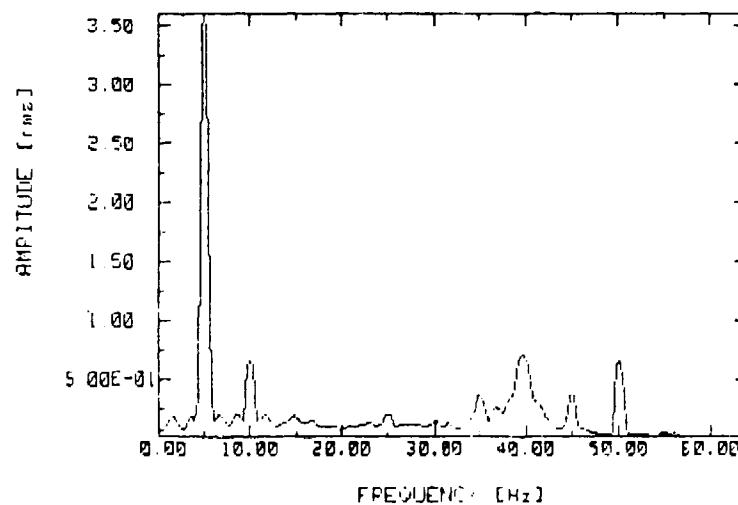
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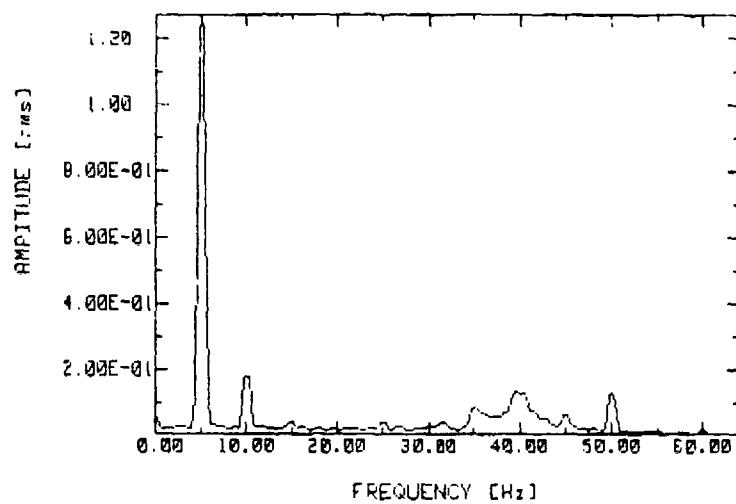
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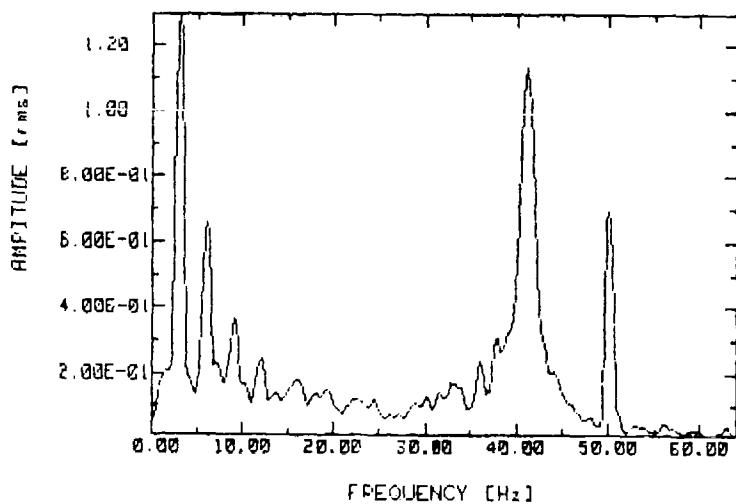
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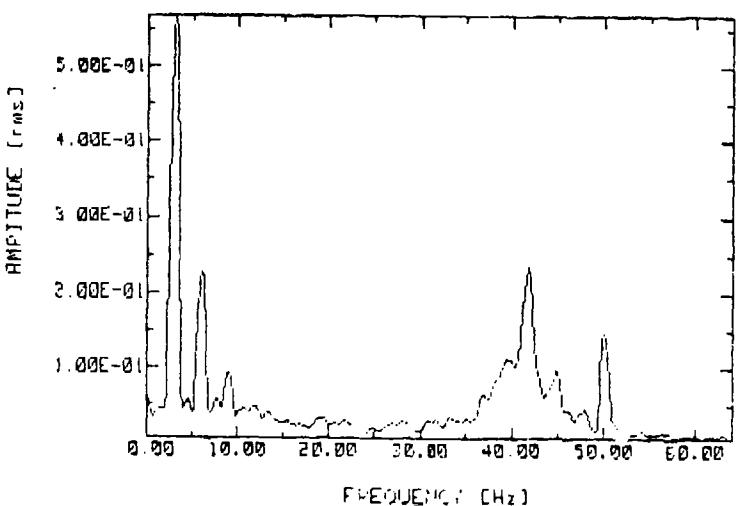
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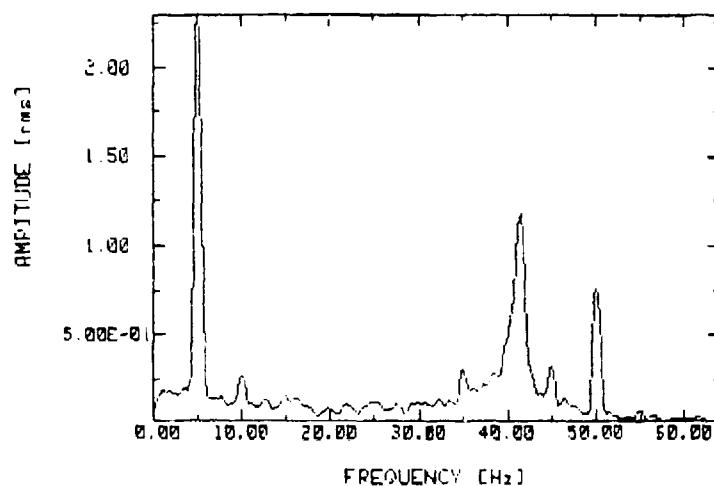
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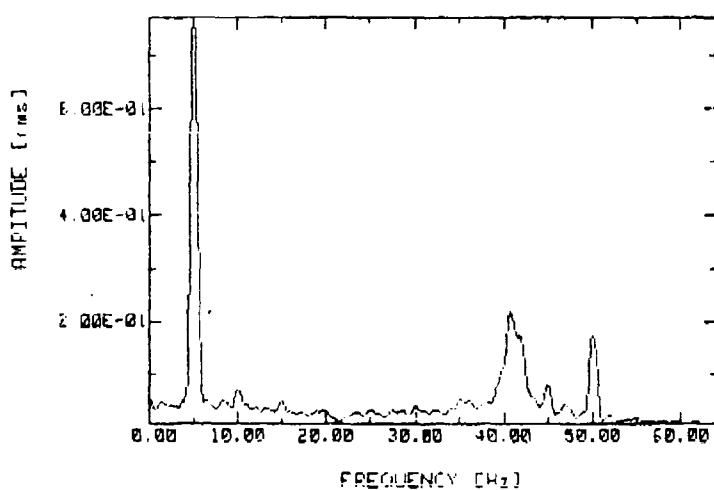
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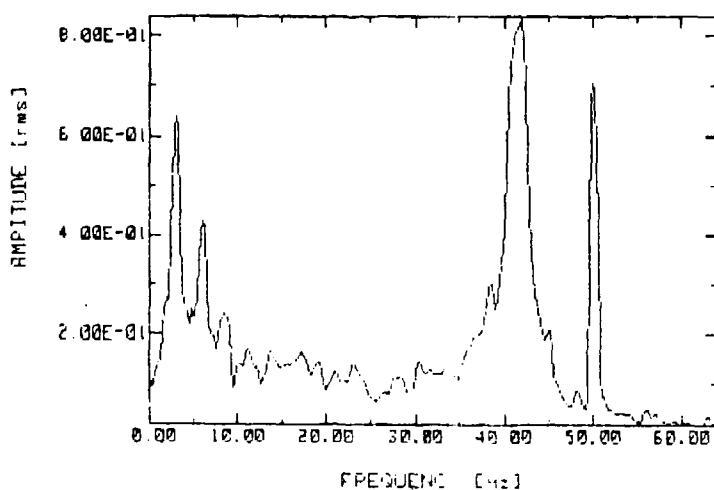
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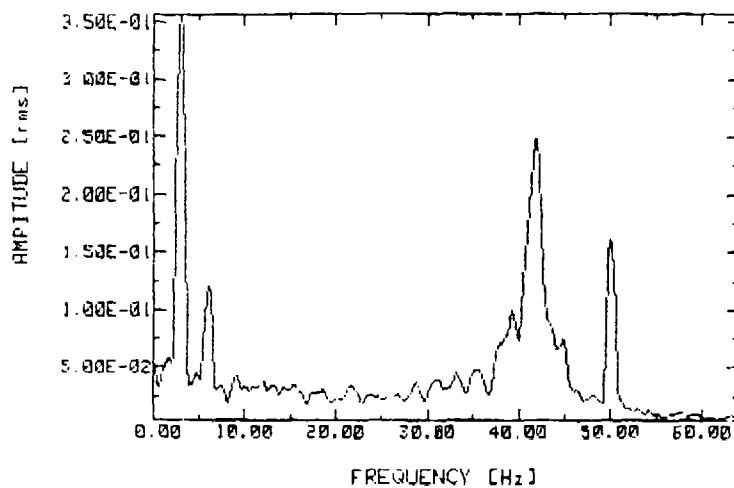
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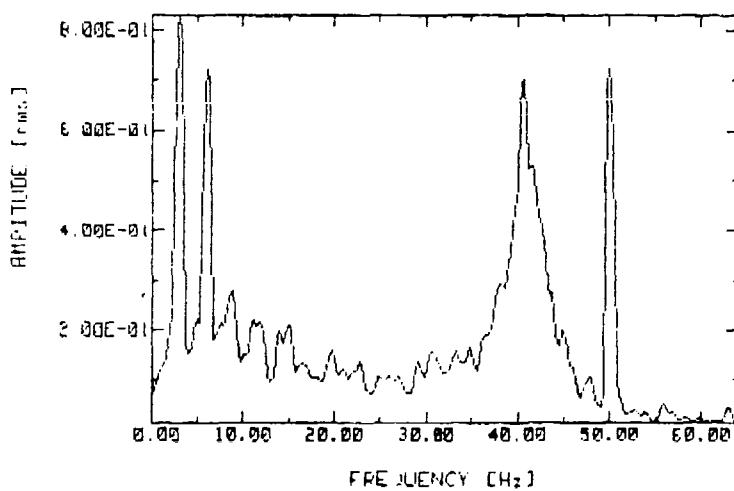
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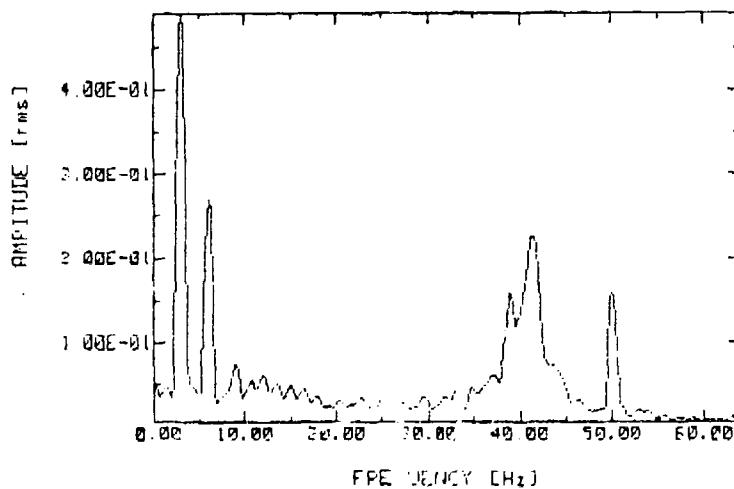
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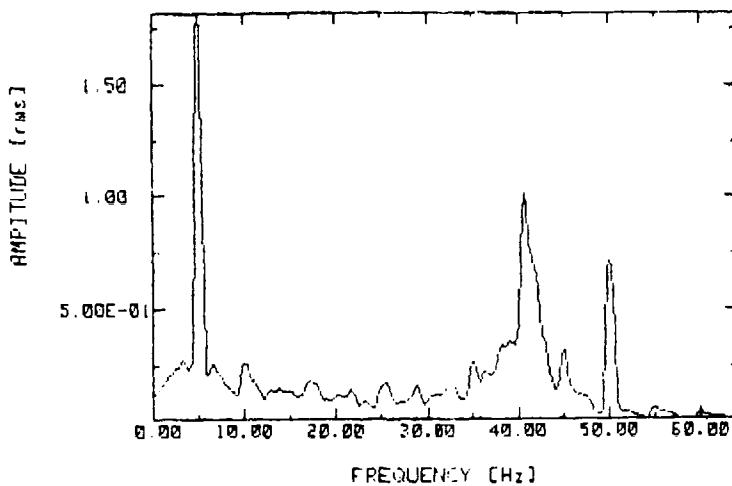
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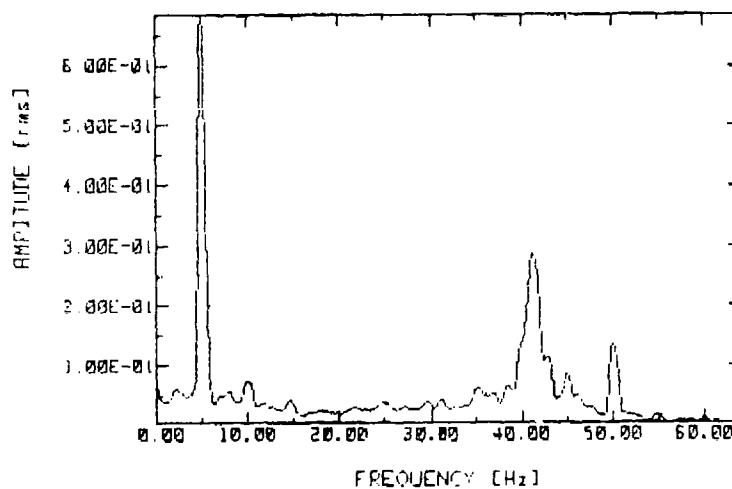
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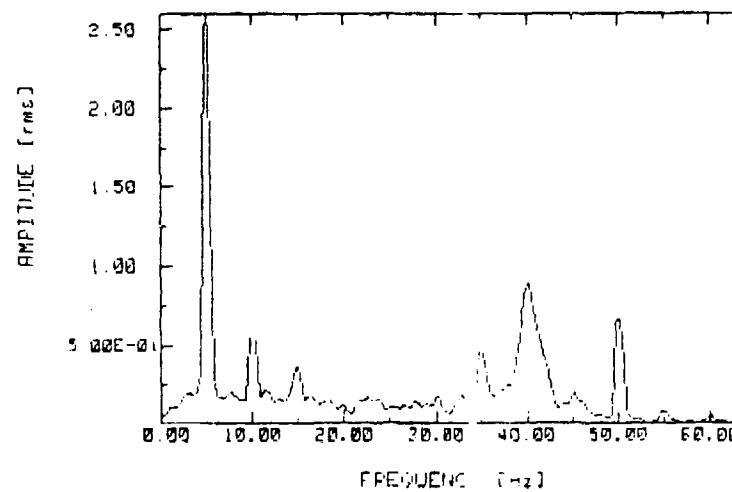
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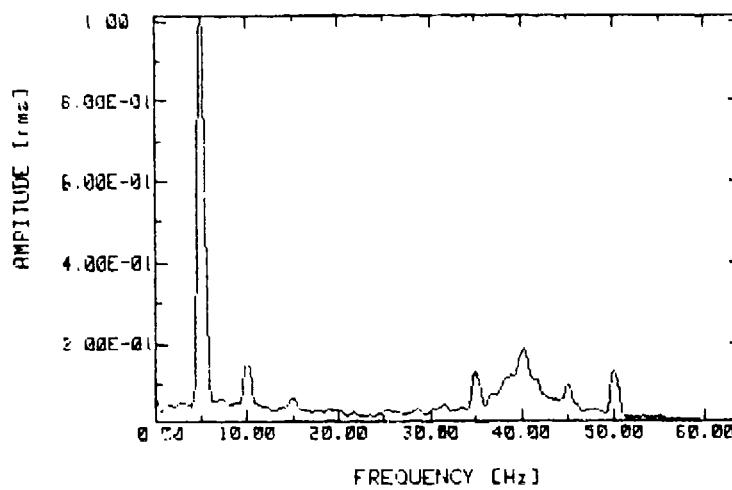
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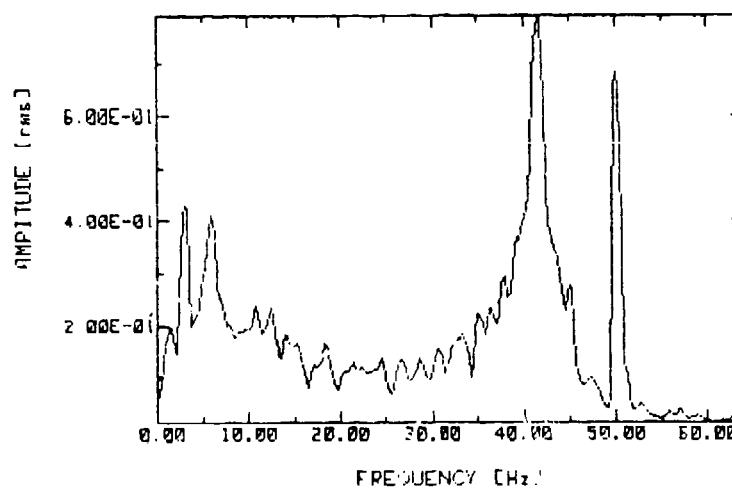
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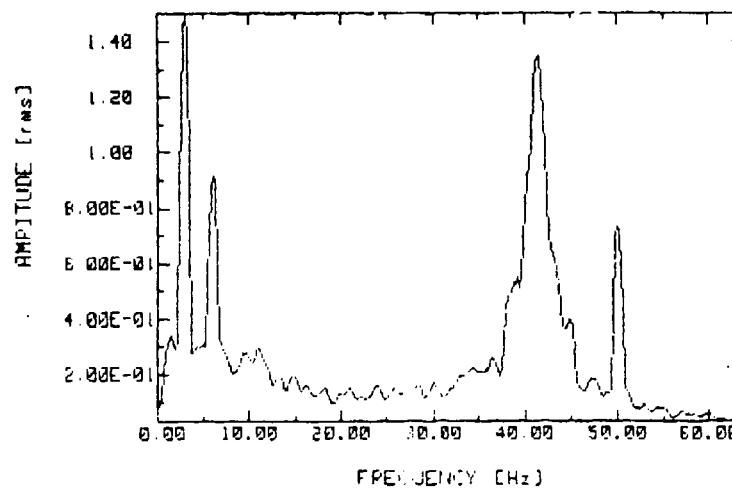
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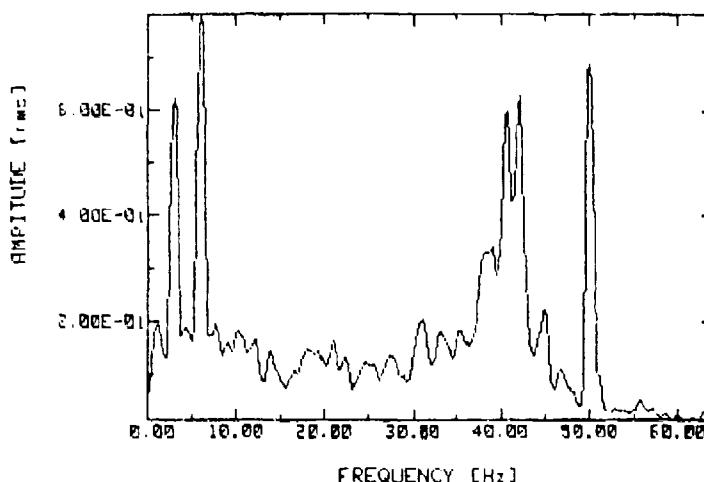
A SPEC 1 DELT_2164 #RV: 10



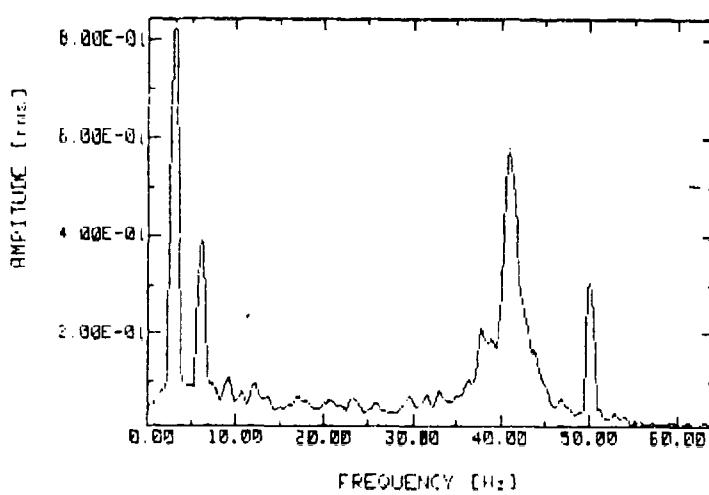
A SPEC 1 DELT_2165 #RV: 10



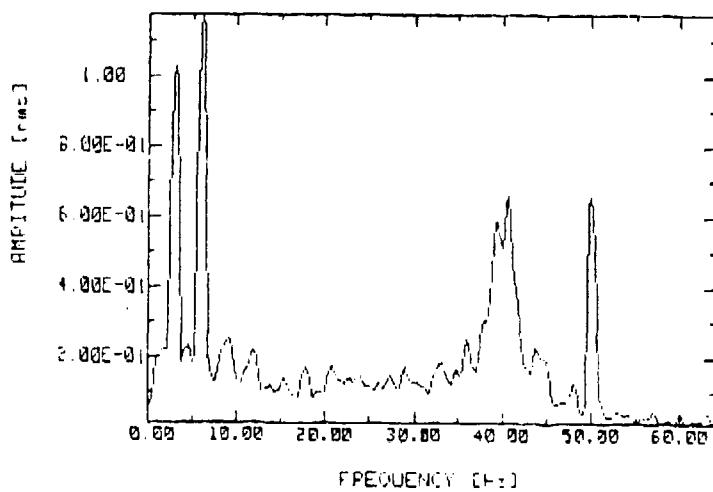
A SPEC 1 DELT_2160 #AV: 10



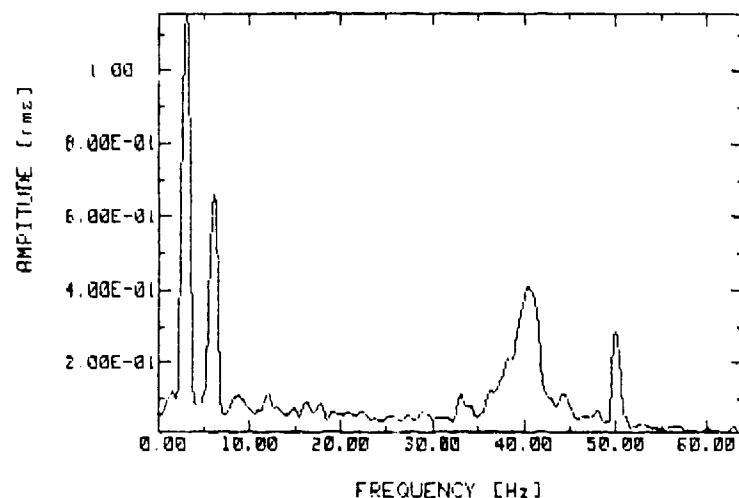
A SPEC 1 DELT_2169 #AV: 10



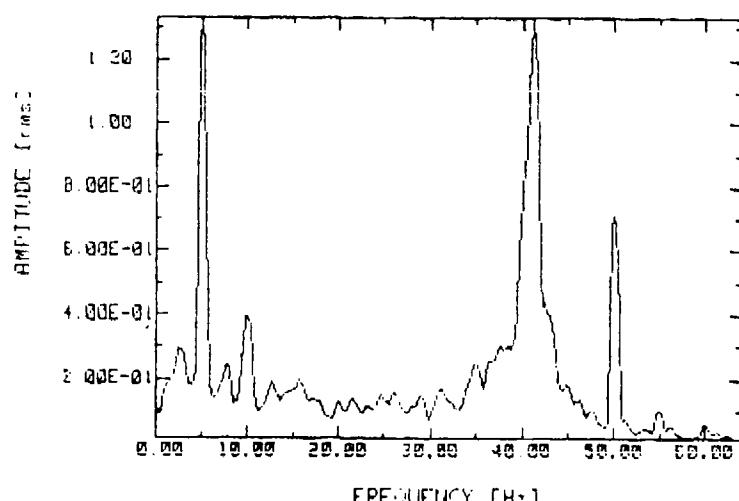
A SPEC 1 DELT_2172 #AV: 10



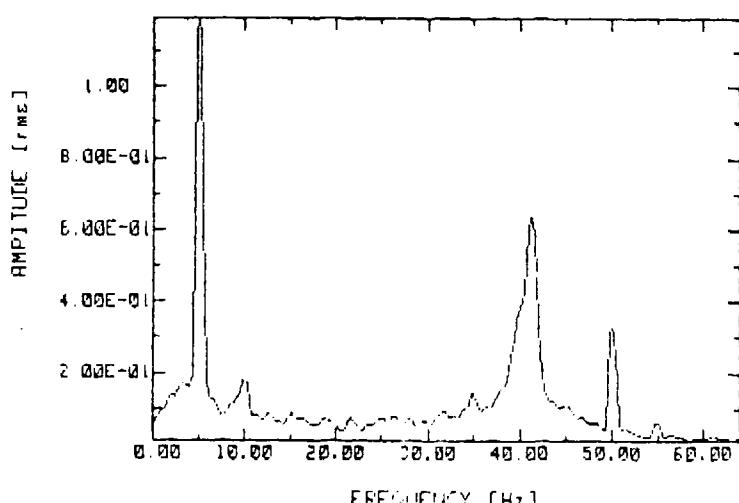
A SPEC 1 DELT_2179 #RV: 10



A SPEC 1 DELT_2221 #RV: 10

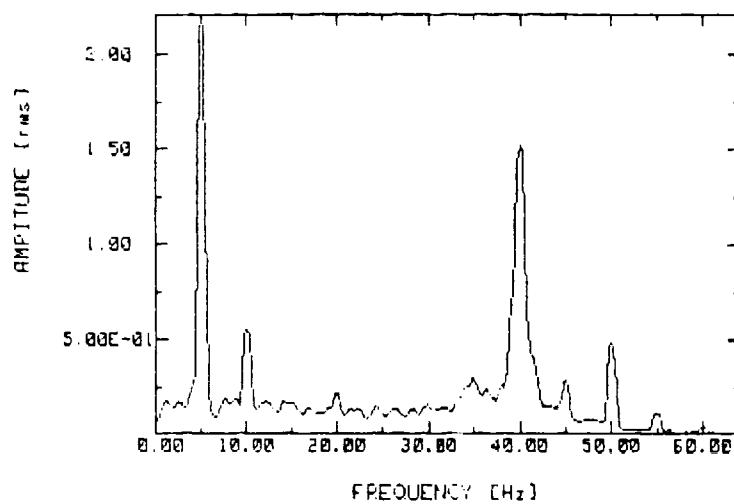


A SPEC 1 DELT_2222 #RV: 10



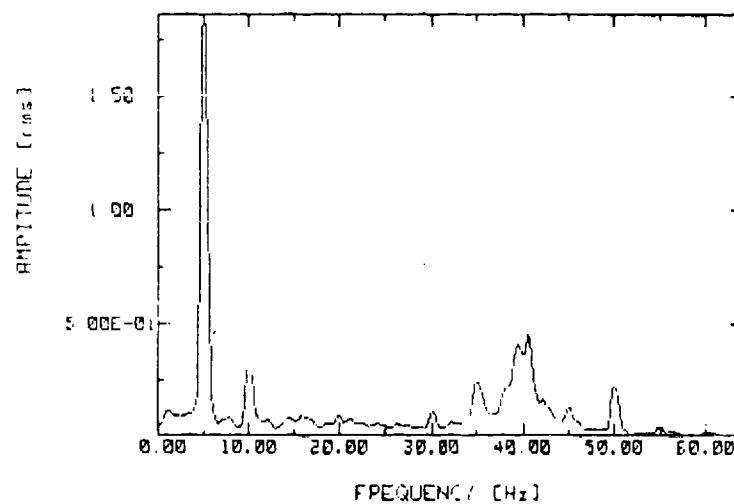
A SPEC 1 DELT_2225

#AV: 10



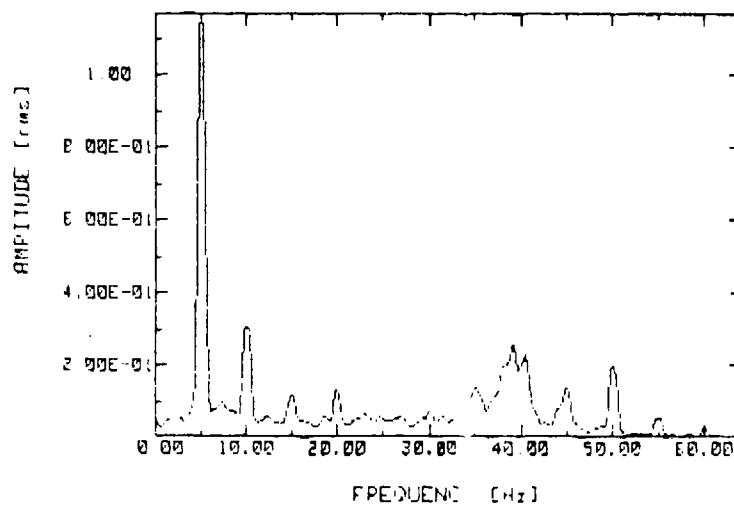
R SPEC 1 DELT_2226

#AV: 10

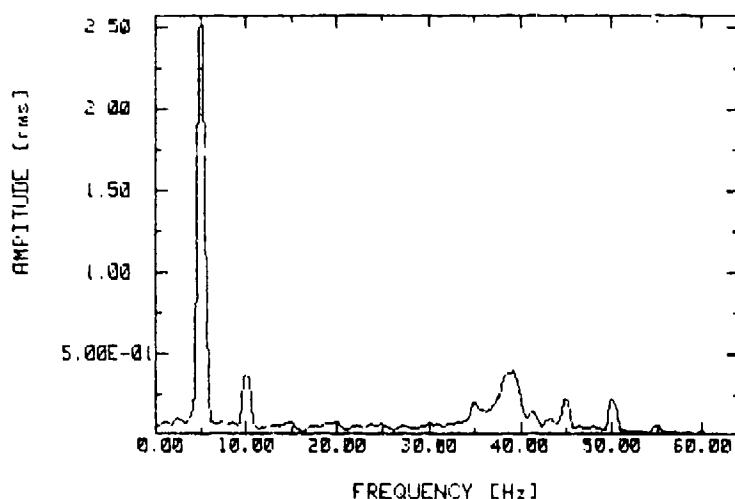


A SPEC 1 DELT_2291

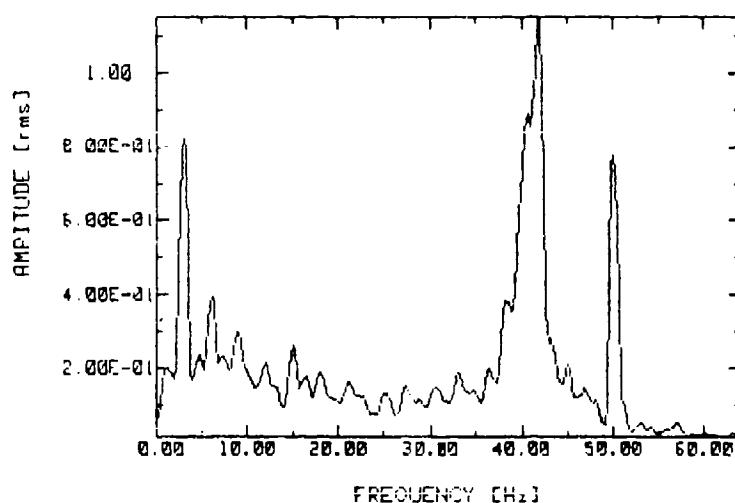
#AV: 10



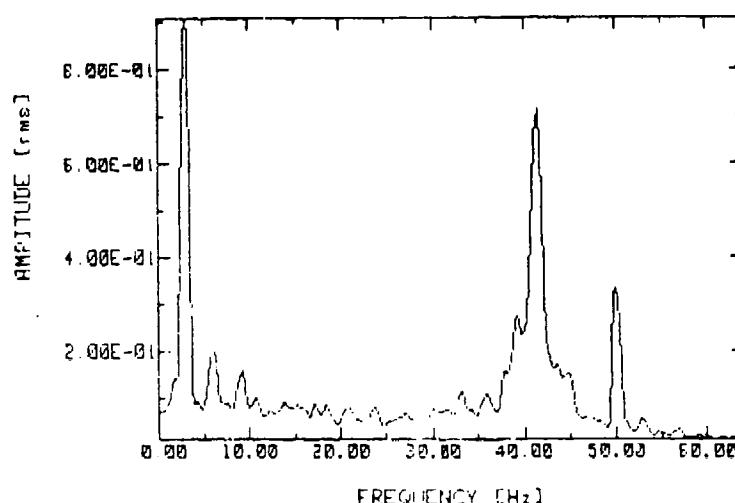
A SPEC 1 DELT_2232 #AV: 10



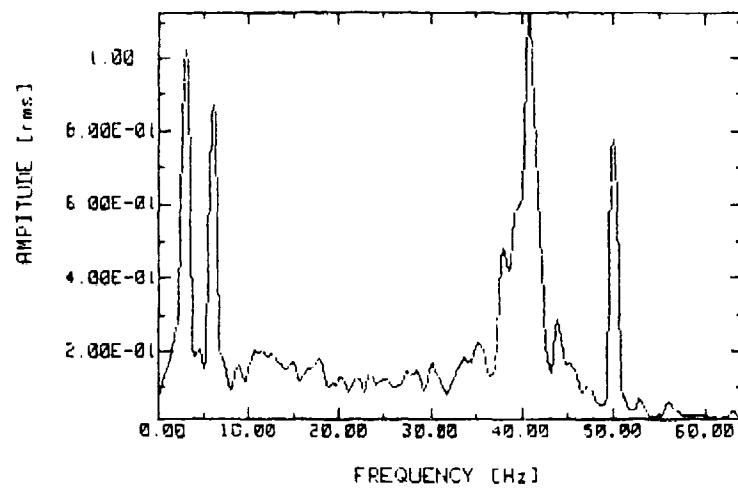
A SPEC 1 DELT_2267 #AV: 10



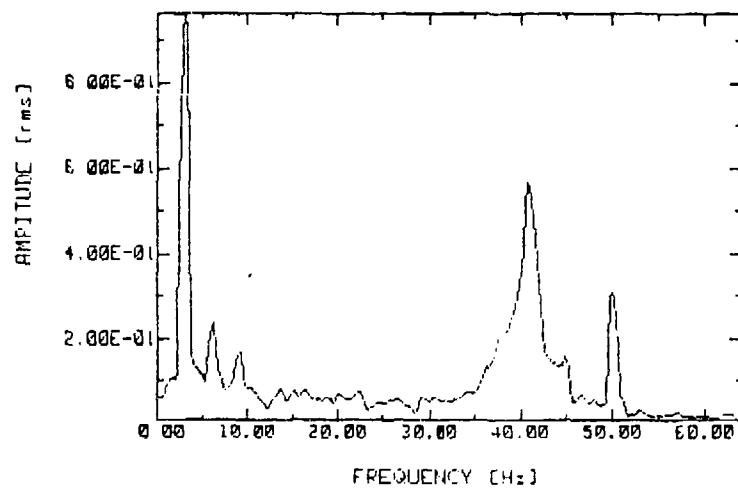
A SPEC 1 DELT_2269 #AV: 10



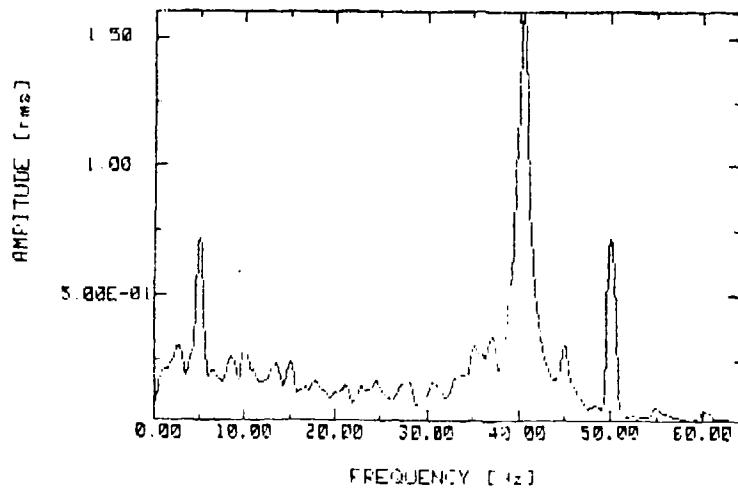
A SPEC 1 DELT_2271 #AV: 10



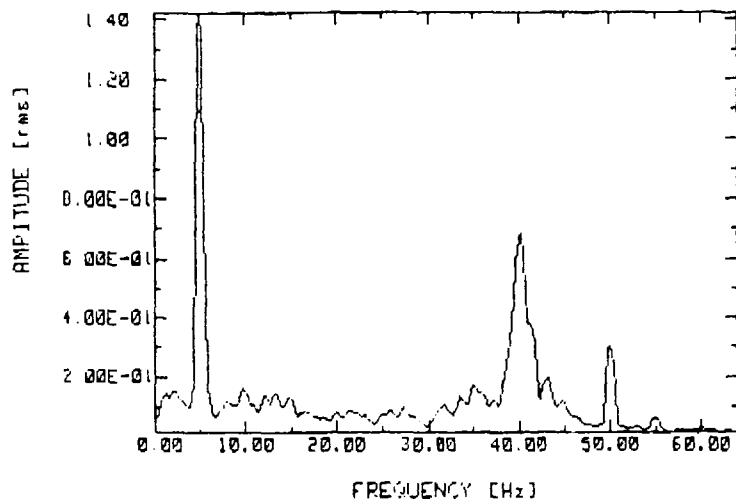
A SPEC 1 DELT_2272 #AV: 10



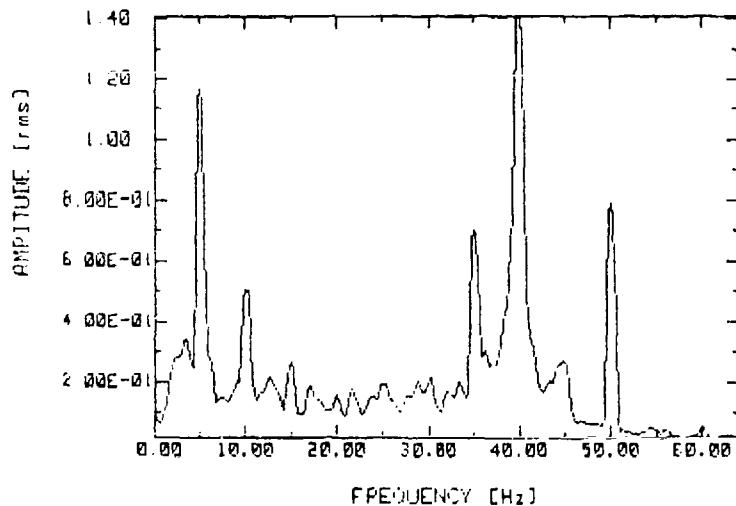
A SPEC 1 DELT_3105 #AV: 10



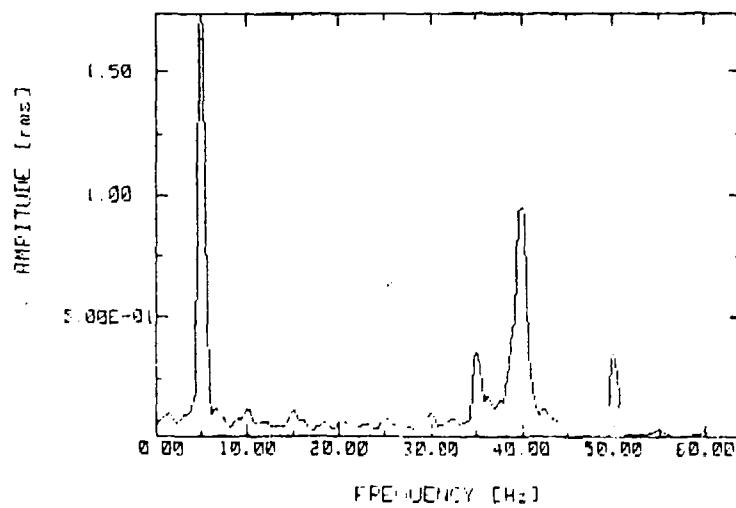
A SPEC I DELT_3105 #AV: 10



A SPEC I DELT_3109 #AV: 10

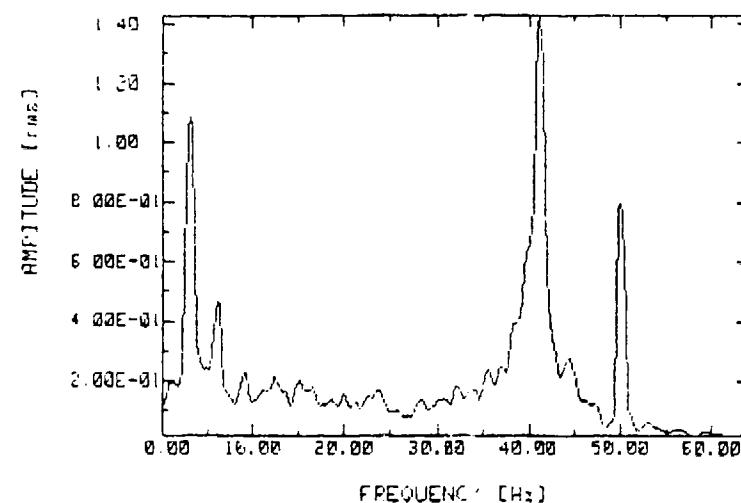


A SPEC I DELT_3110 #AV: 10



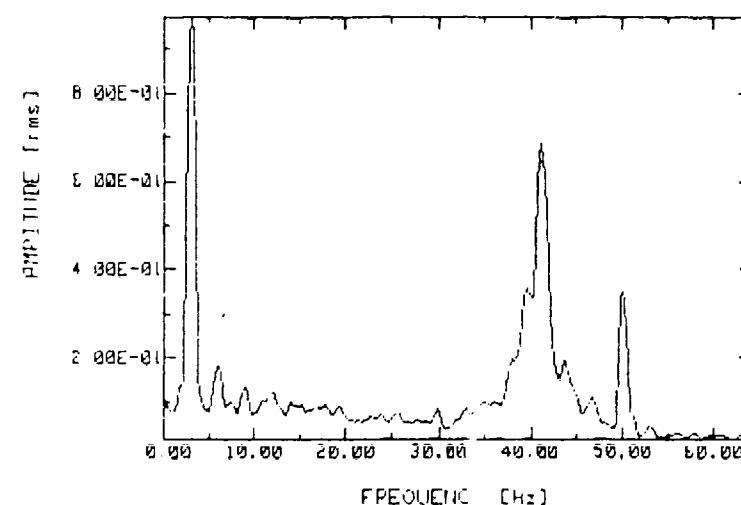
A SPEC 1 DELT_311?

#AV: 10



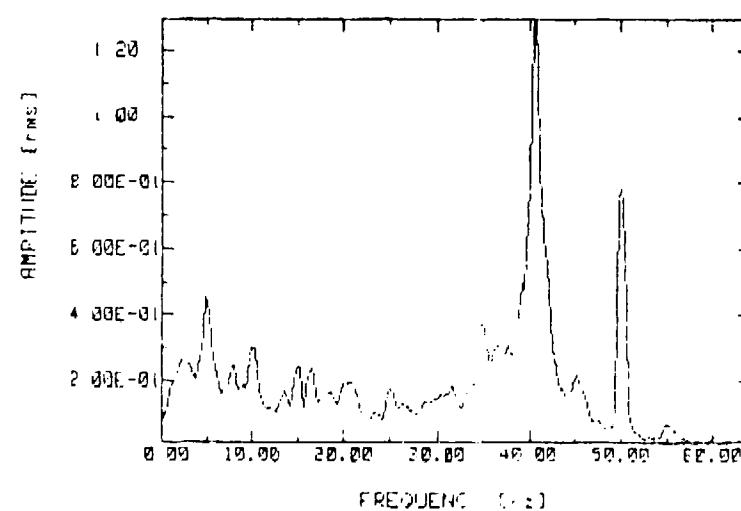
A SPEC 1 DELT_311B

#AV: 10



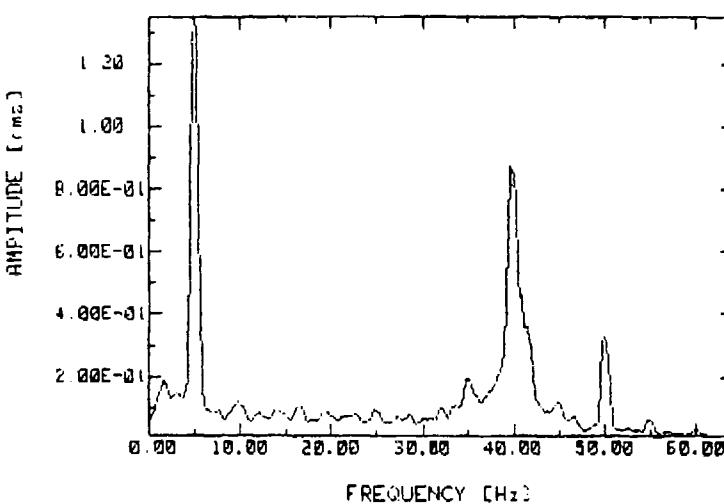
A SPEC 1 DELT_312?

#AV: 10



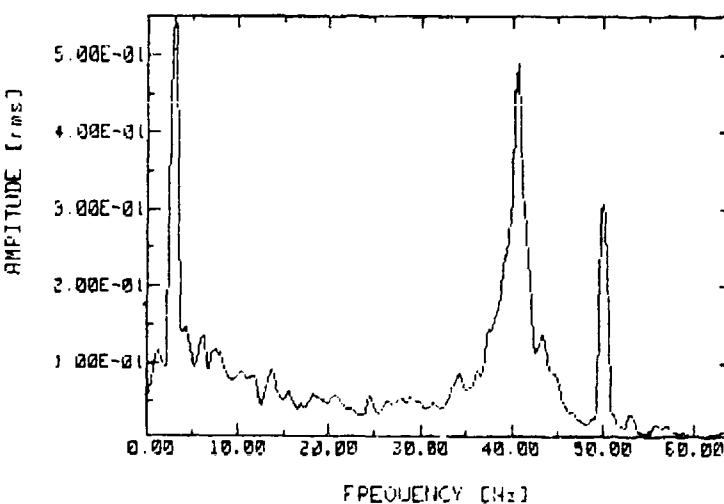
R SPEC 1 DELT_312B

#AV: 10



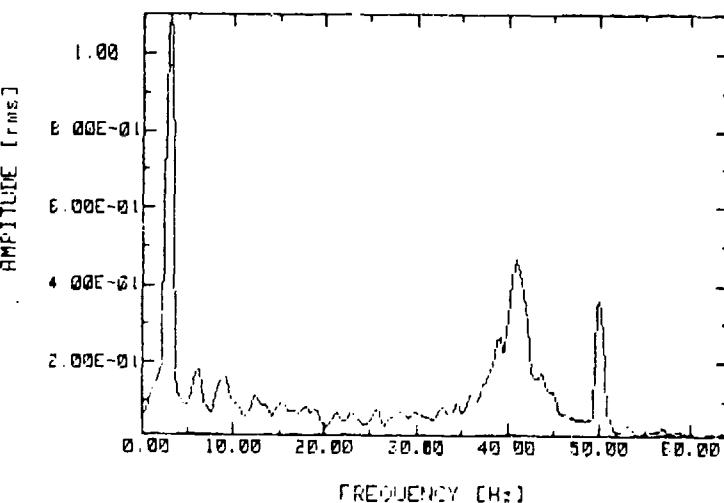
R SPEC 1 DELT_3137

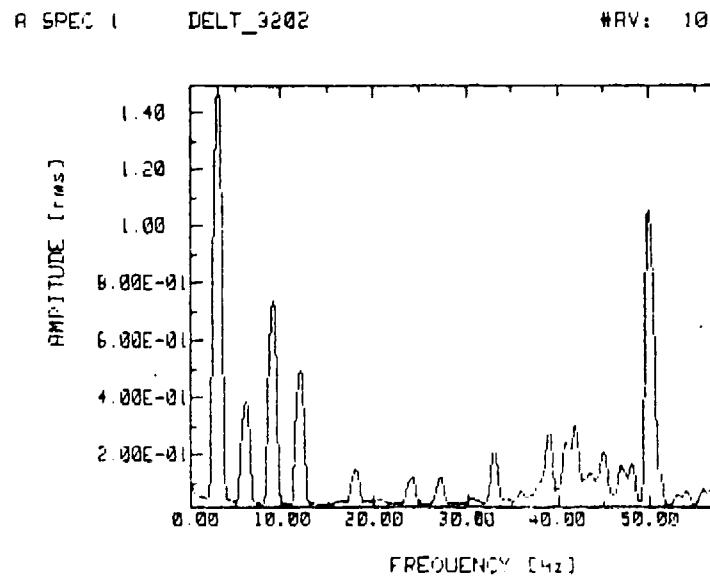
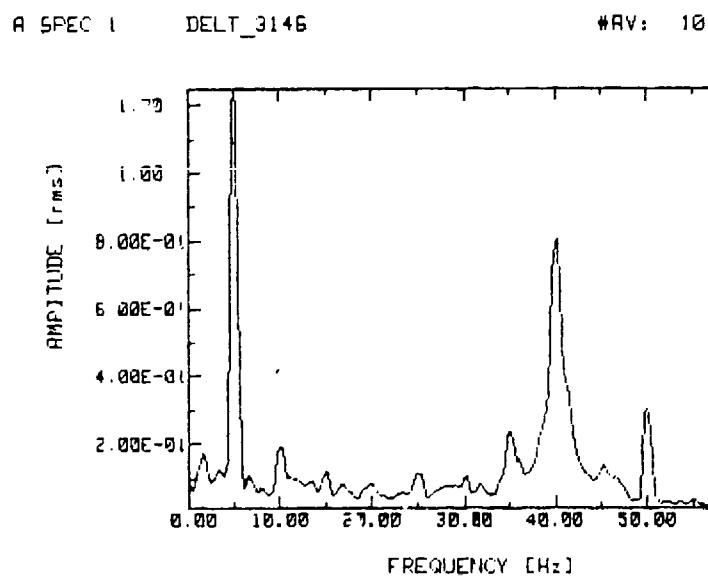
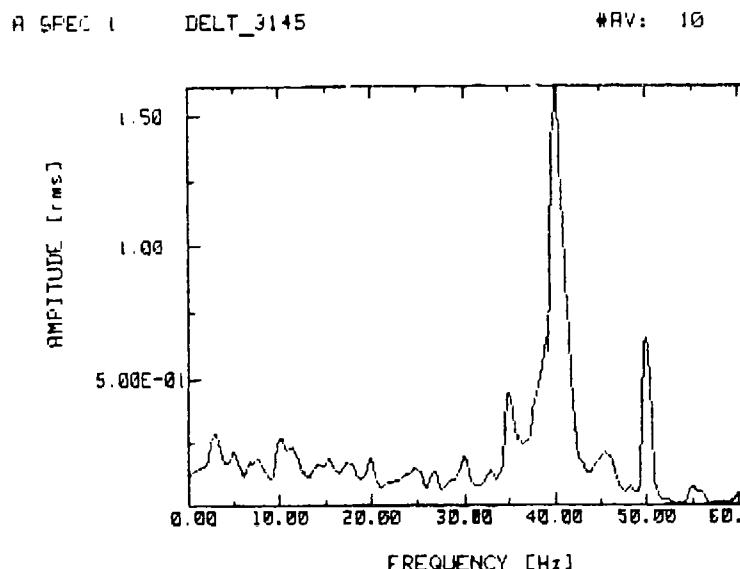
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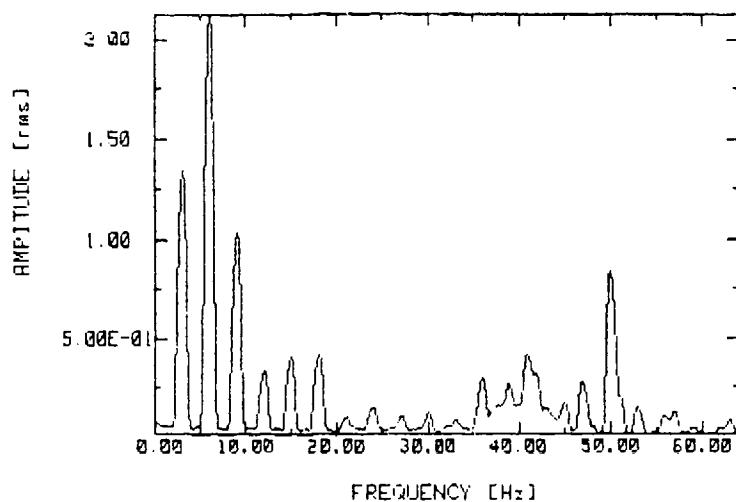
R SPEC 1 DELT_3138

#AV: 10

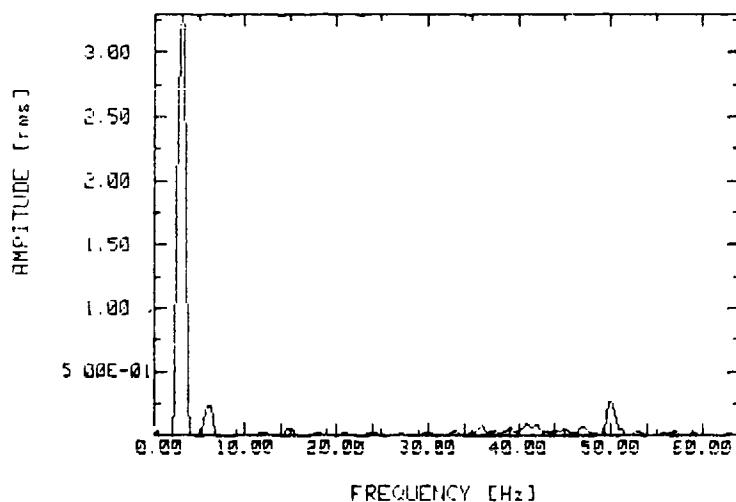




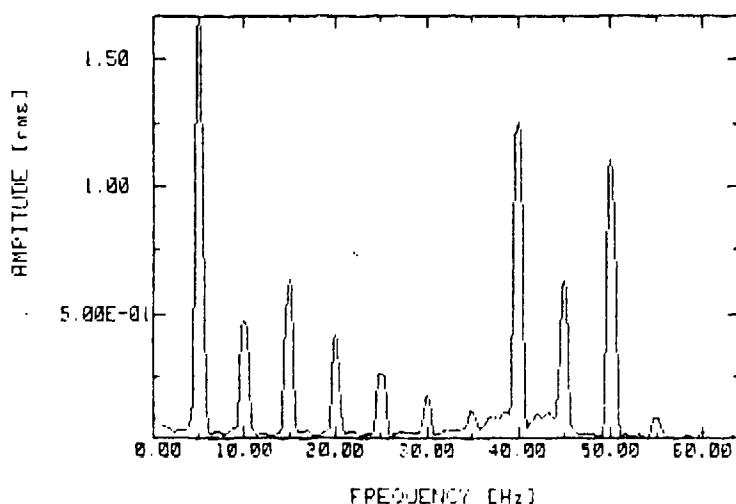
A SPEC 1 DELT_3203 #AV: 10



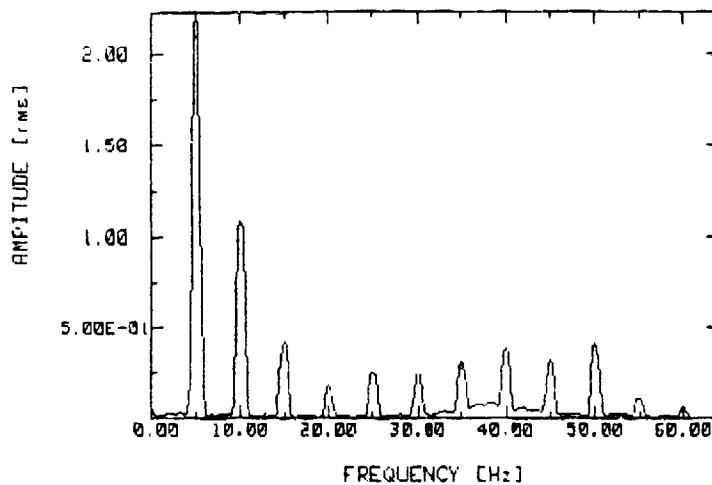
A SPEC 1 DELT_3204 #AV: 10



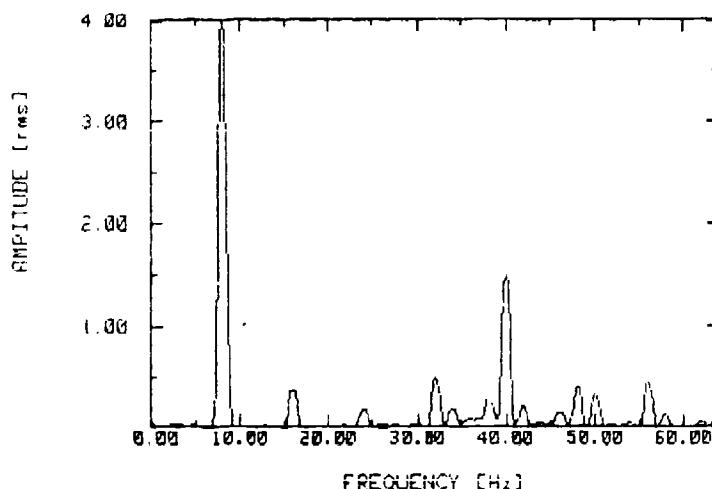
A SPEC 1 DELT_3207 #AV: 10



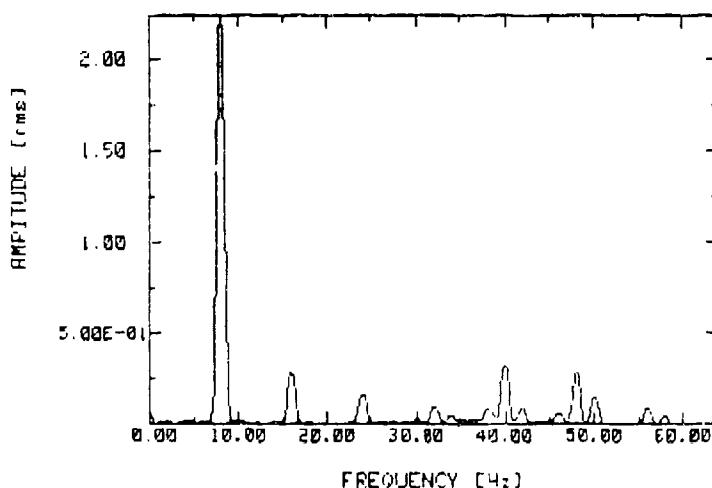
R SPEC 1 DELT_3208 #AV: 10



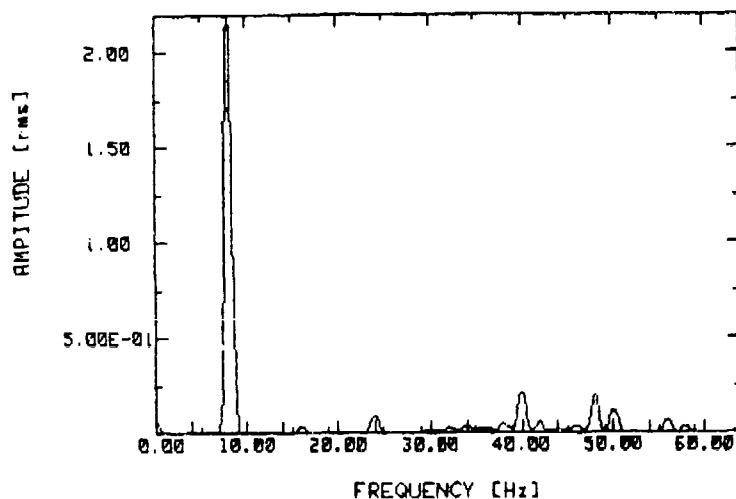
R SPEC 1 DELT_3211 #AV: 10



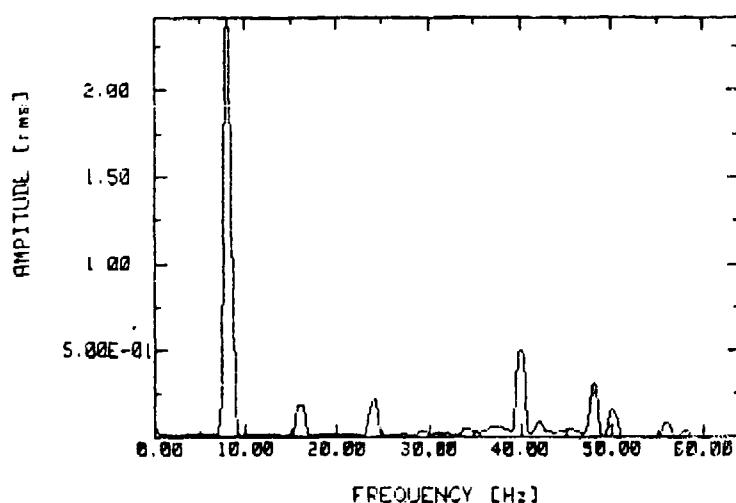
R SPEC 1 DELT_3243 #AV: 10



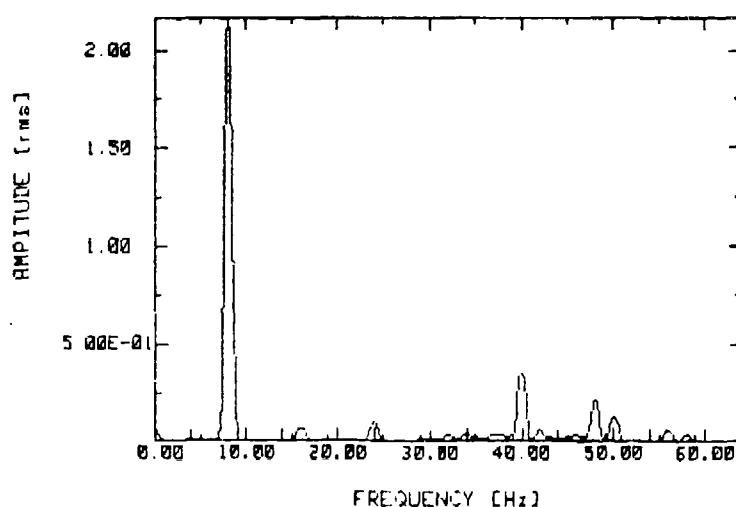
A SPEC 1 DELT_3244 #AV: 10



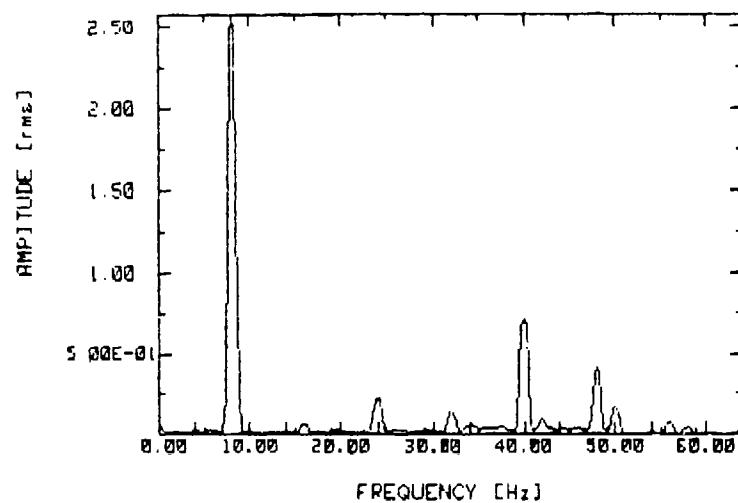
A SPEC 1 DELT_3255 #AV: 10



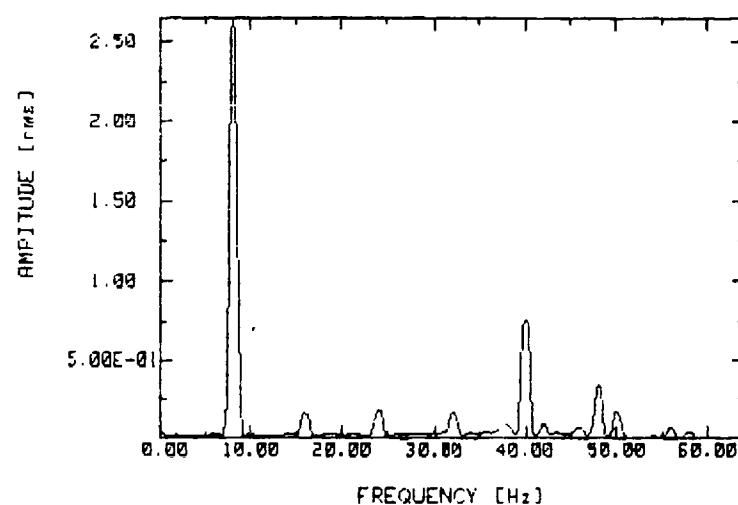
A SPEC 1 DELT_3256 #AV: 10



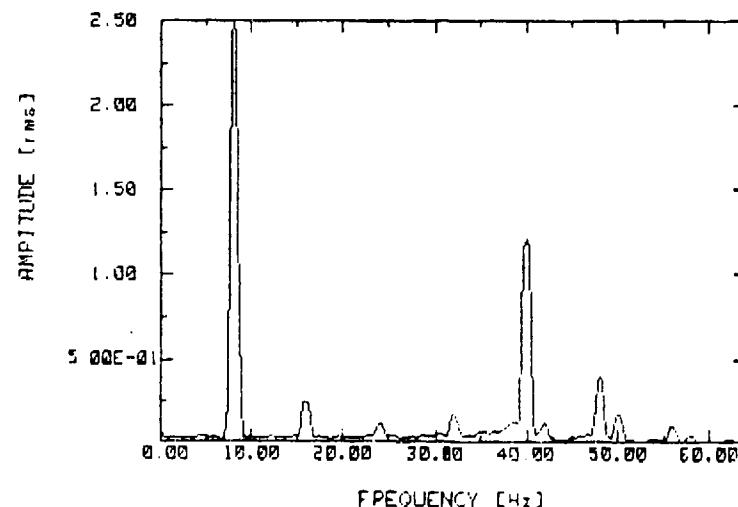
A SPEC 1 DELT_3270 #AV: 10



A SPEC 1 DELT_4104 #AV: 10

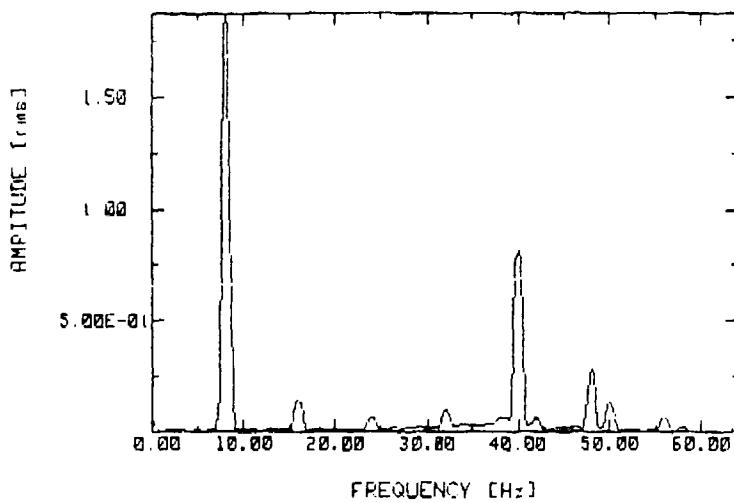


A SPEC 1 DELT_4110 #AV: 10



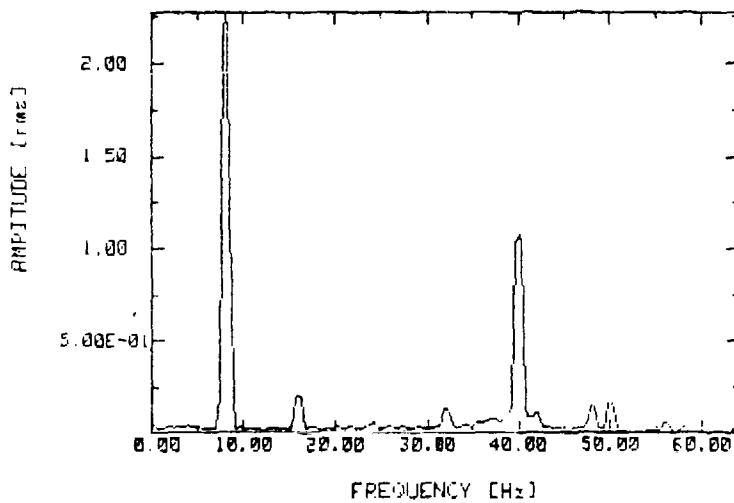
A SPEC 1 DELT_4111

#AV: 10



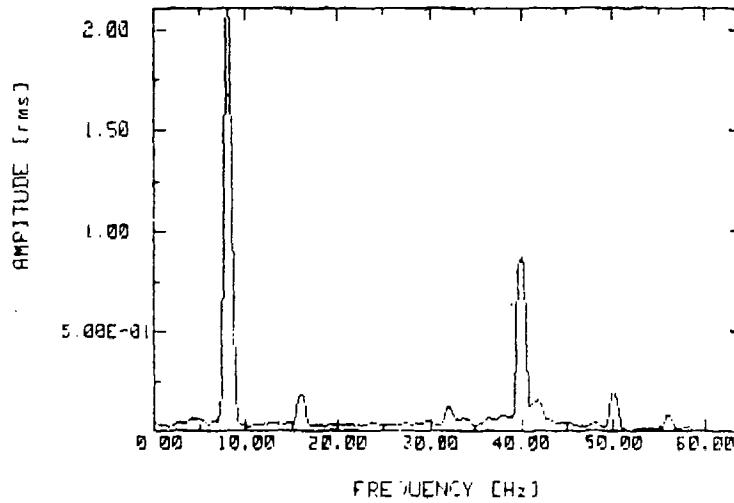
A SPEC 1 DELT_4117

#AV: 10

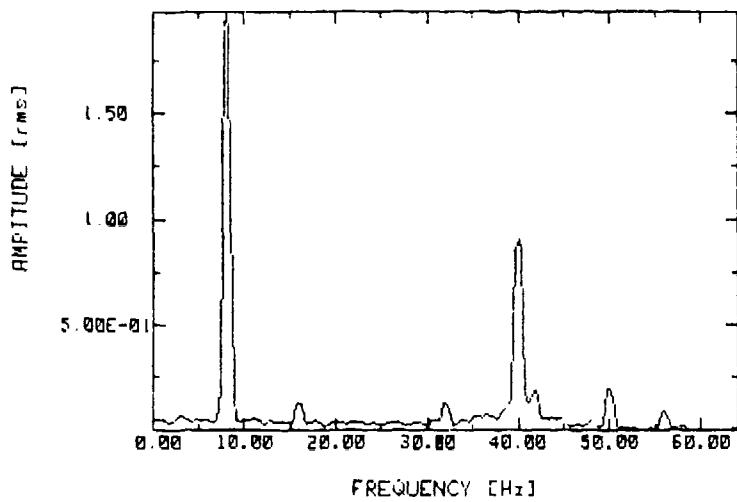


A SPEC 1 DELT_4123

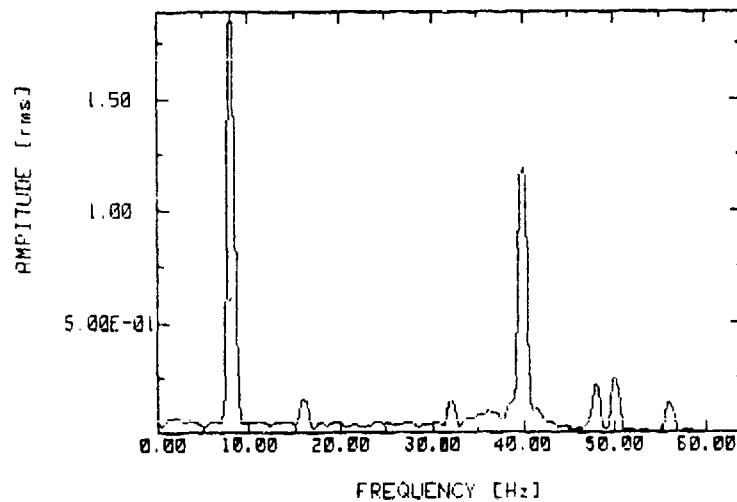
#AV: 10



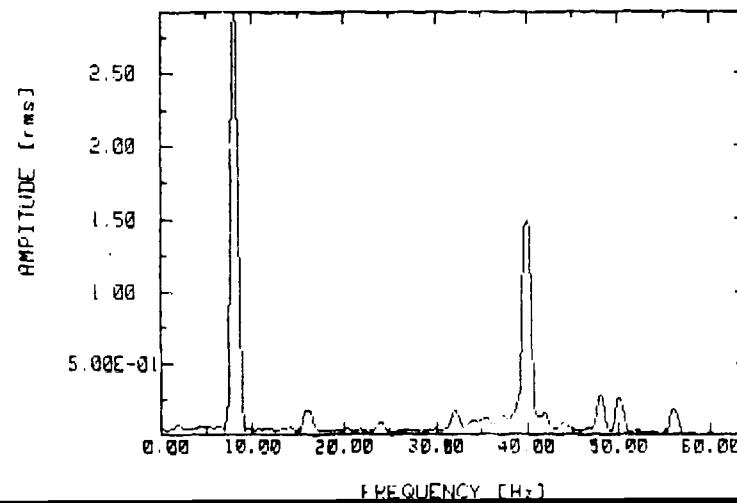
R SPEC 1 DELT_4129 #AV: 10



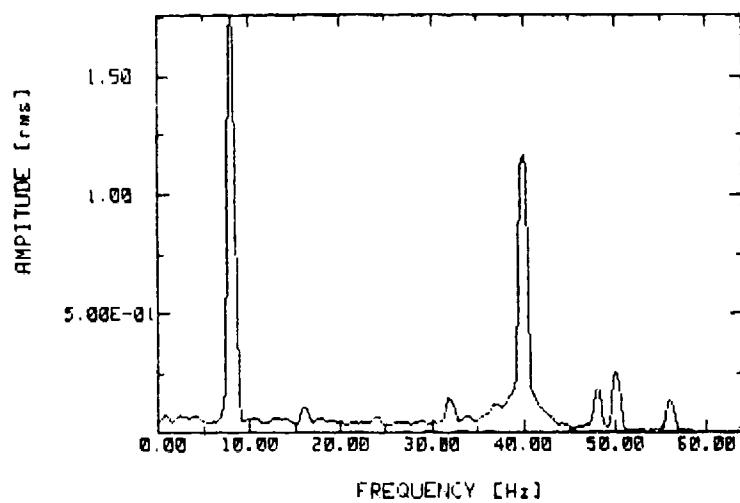
R SPEC 1 DELT_4149 #AV: 10



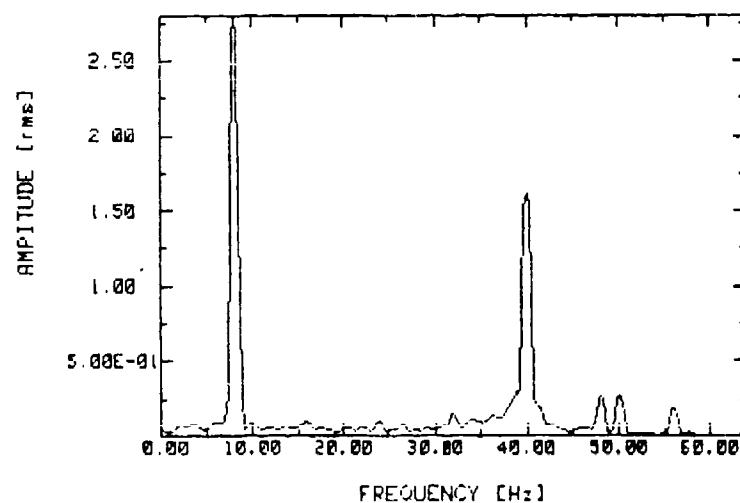
R SPEC 1 DELT_4150 #AV: 10



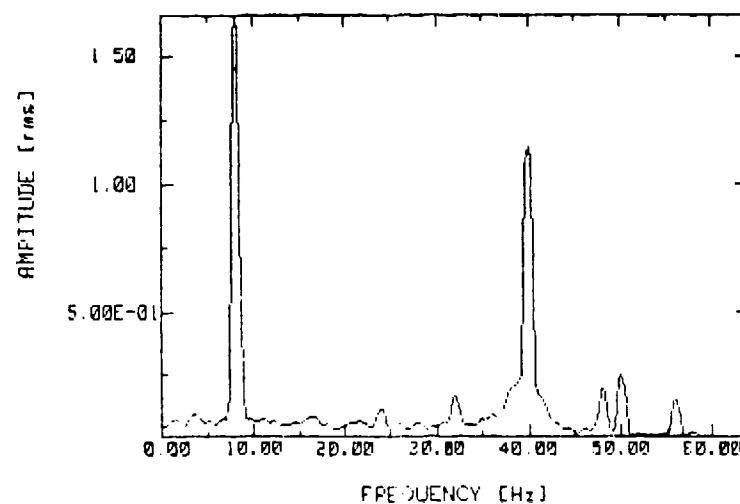
A SPEC 1 DELT_4161 #AV: 10



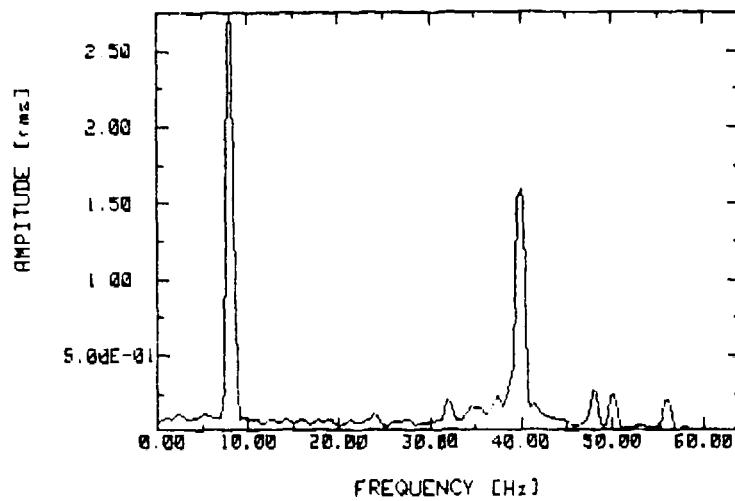
A SPEC 1 DELT_4162 #AV: 10



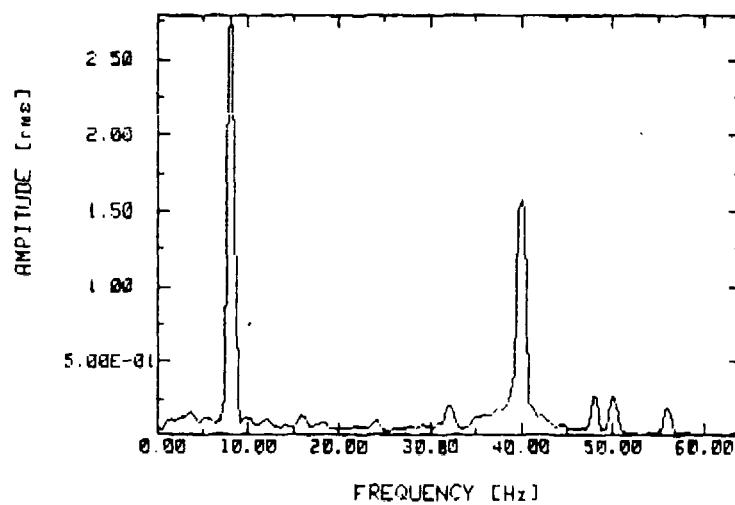
A SPEC 1 DELT_5115 #AV: 10



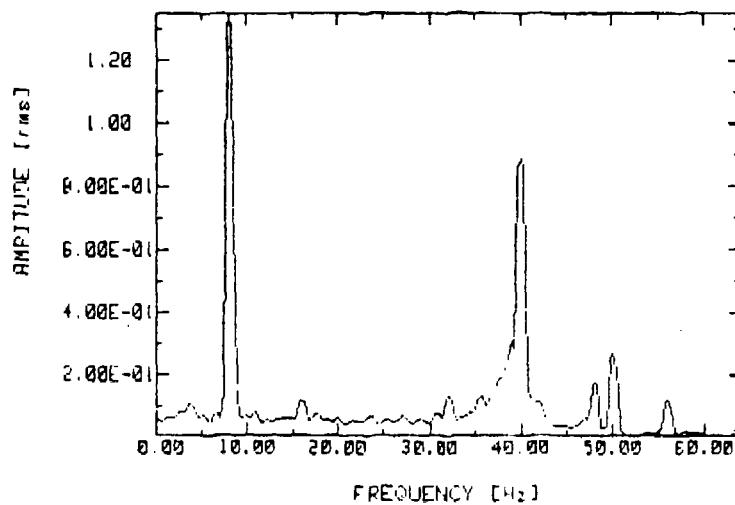
A SPEC 1 DELT_5116 #AV: 10



A SPEC 1 DELT_5132 #AV: 10

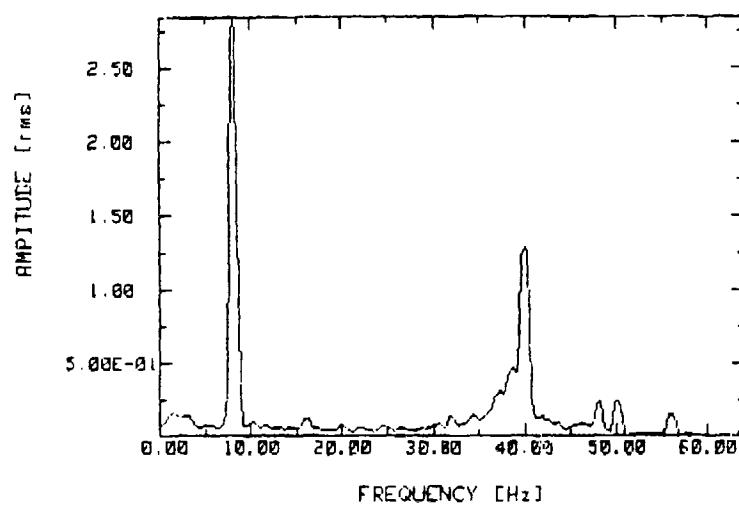


A SPEC 1 DELT_5155 #AV: 10



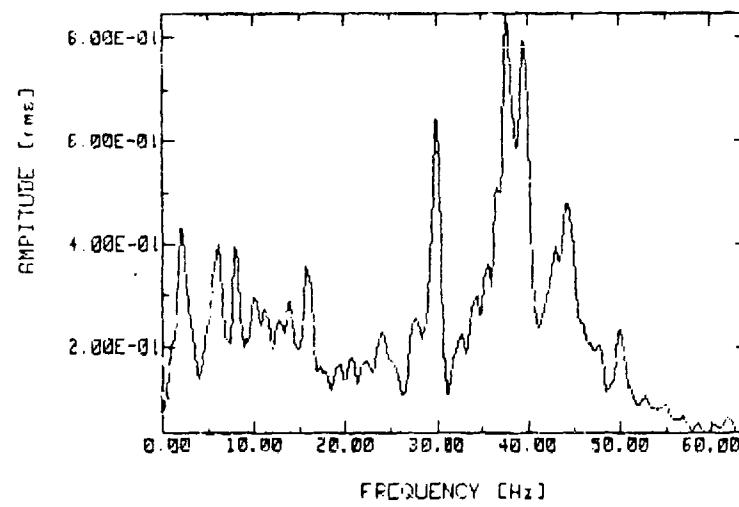
A SPEC 1 DELT_5156

#AV: 10



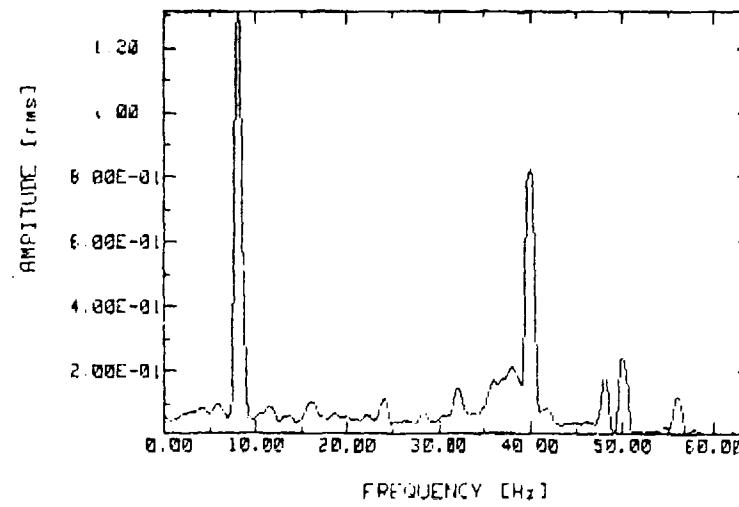
A SPEC 1 DELT_5157

#AV: 10



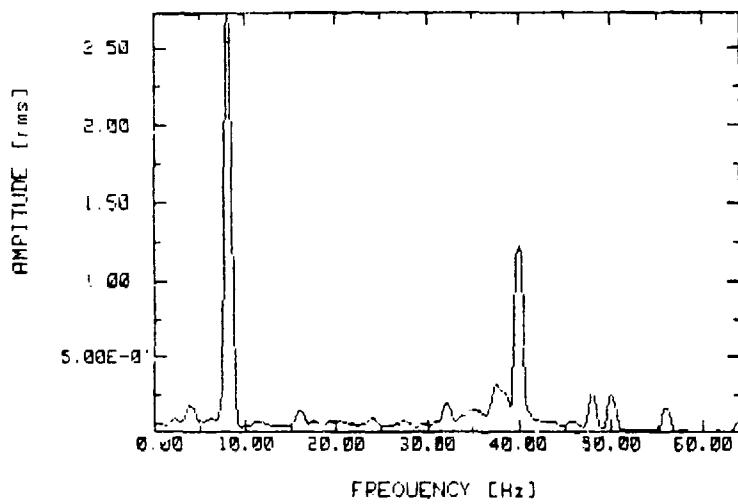
A SPEC 1 DELT_5169

#AV: 10

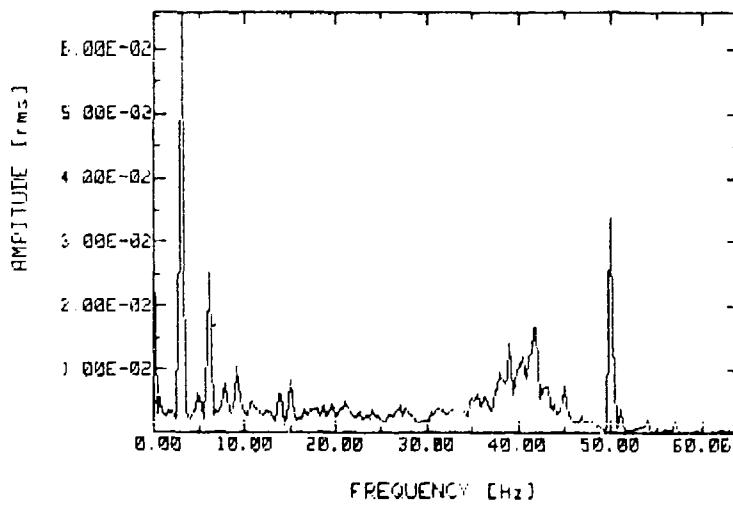


-40-

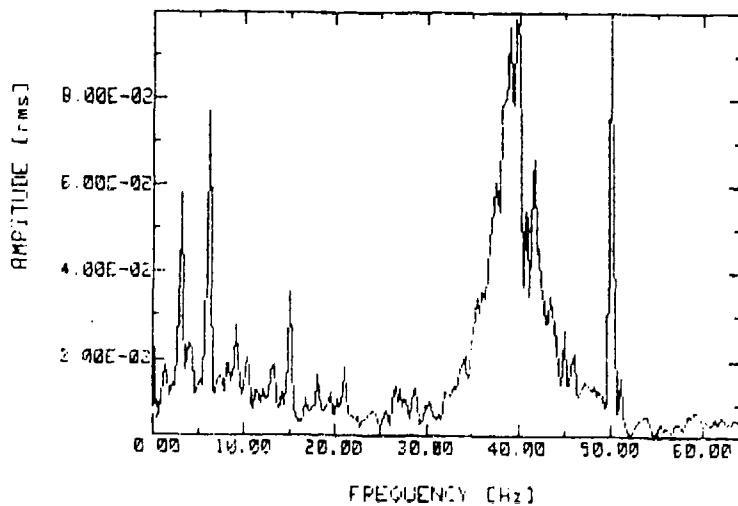
A SPEC 1 DELT_5169 #RV: 10



A SPEC 2 DELT_5240 #RV: 10

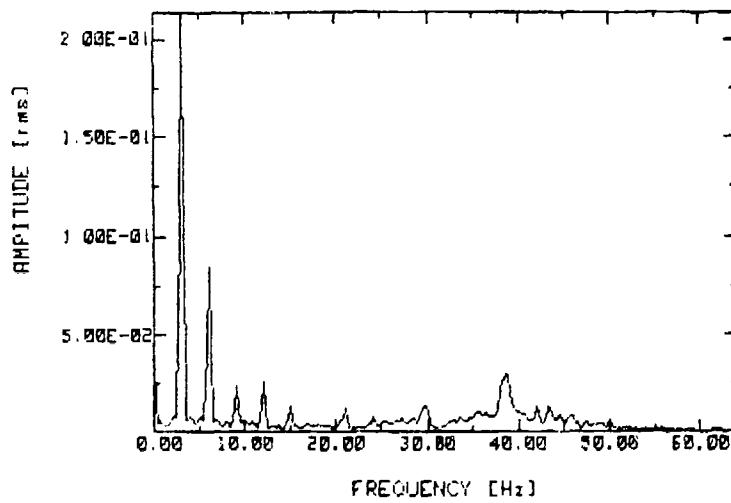


A SPEC 2 DELT_5241 #RV: 10



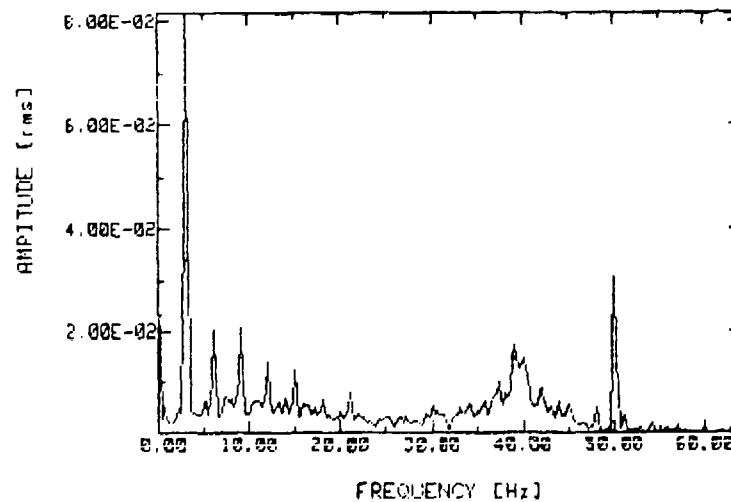
A SPEC 2 DELT_5242

#AV: 10



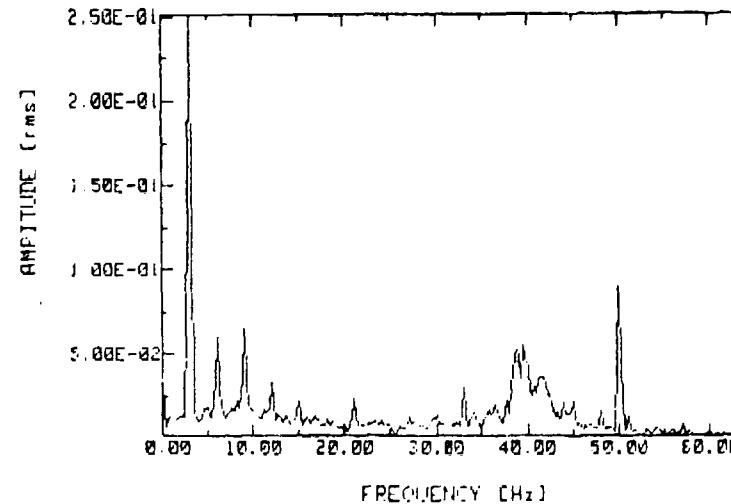
A SPEC 2 DELT_5243

#AV: 10

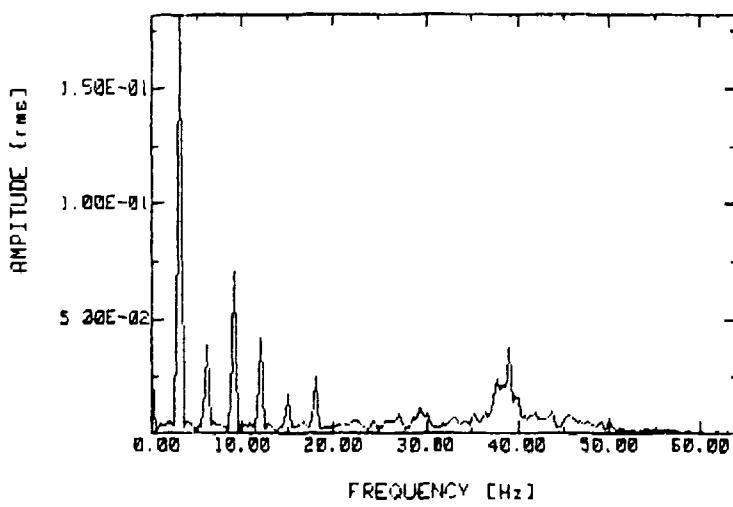


A SPEC 3 DELT_5244

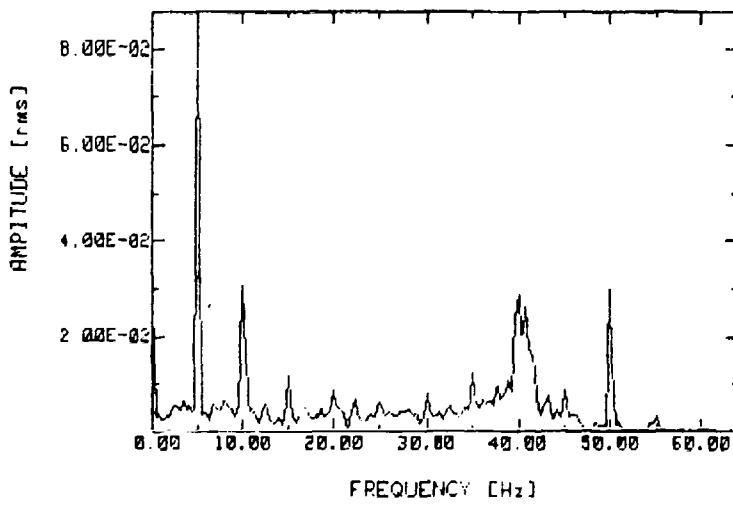
#AV: 10



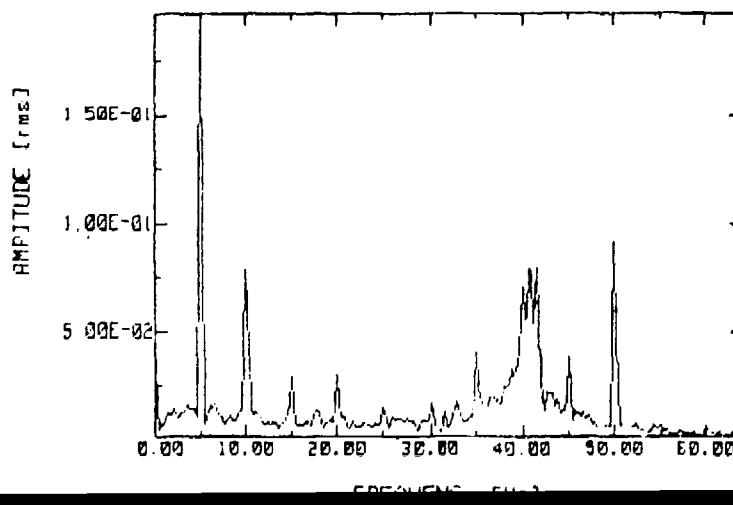
A SPEC 2 DELT_5245 #RV: 10



A SPEC 2 DELT_5249 #RV: 10



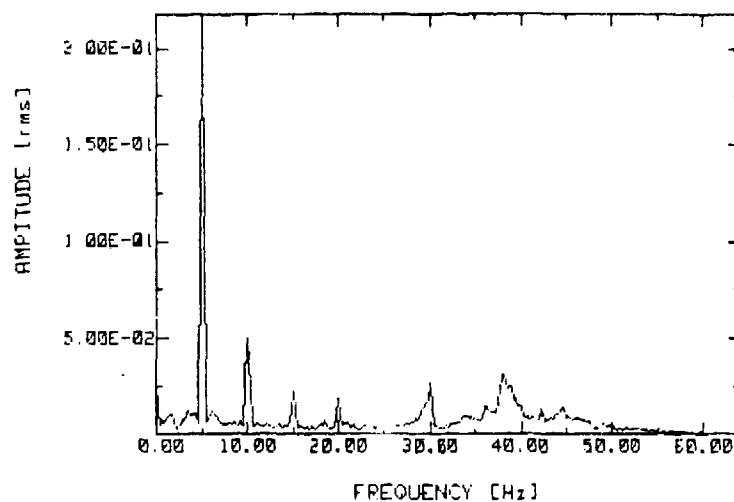
A SPEC 2 DELT_5250 #RV: 10



A SPEC 2

DELT_5251

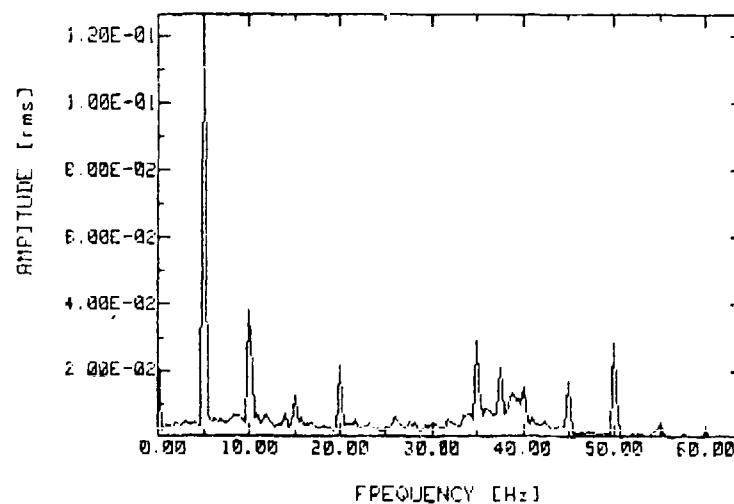
#AV: 10



A SPEC 2

DELT_5252

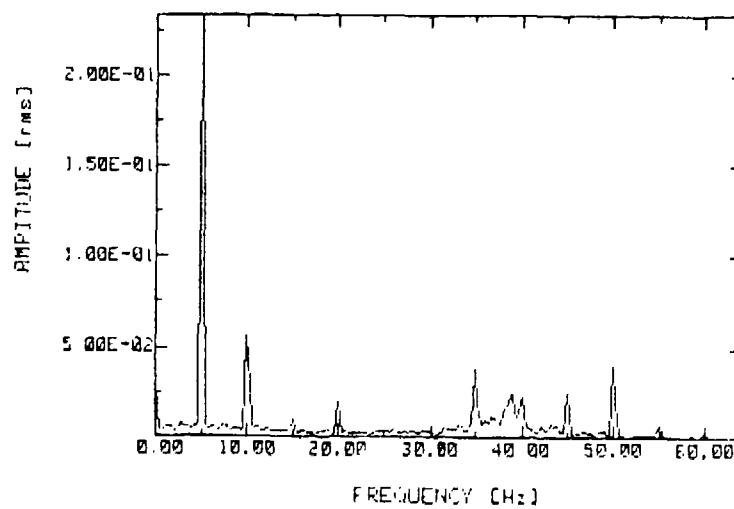
#AV: 10



A SPEC 2

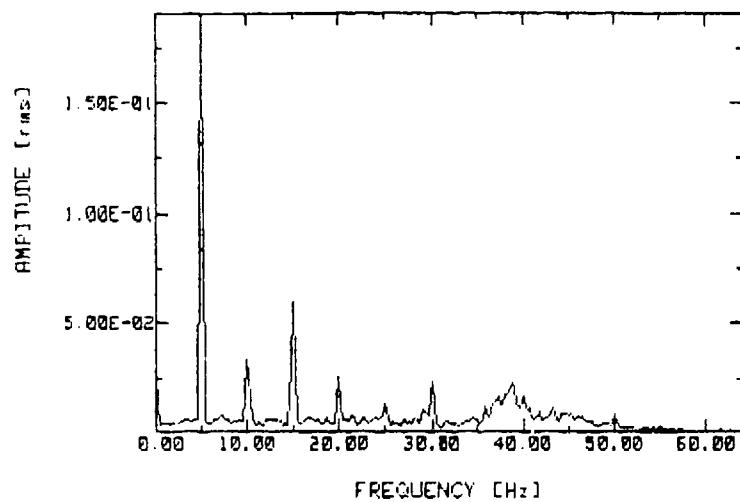
DELT_5253

#AV: 10



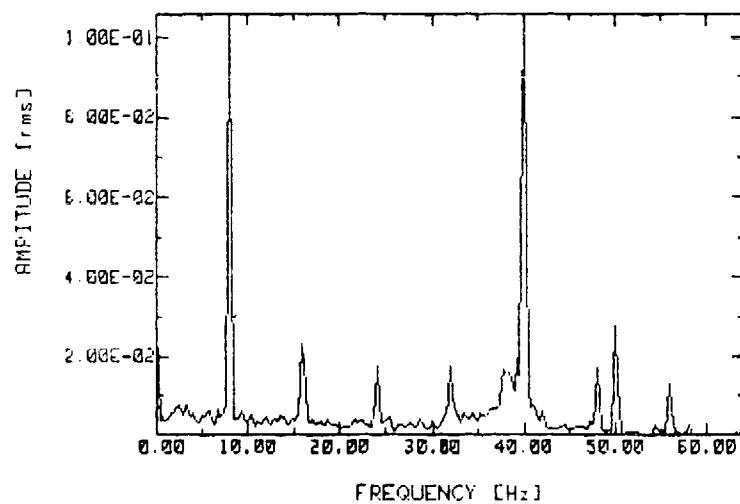
R SPEC 2 DELT_5254

#AV: 10



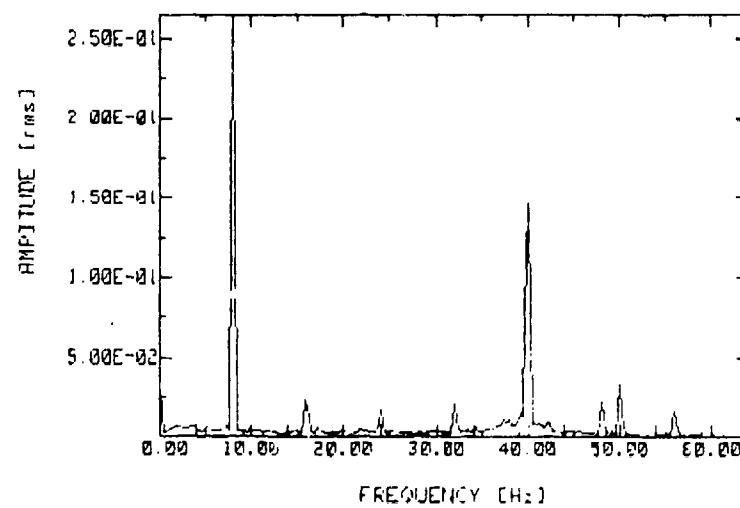
R SPEC 2 DELT_5261

#AV: 10

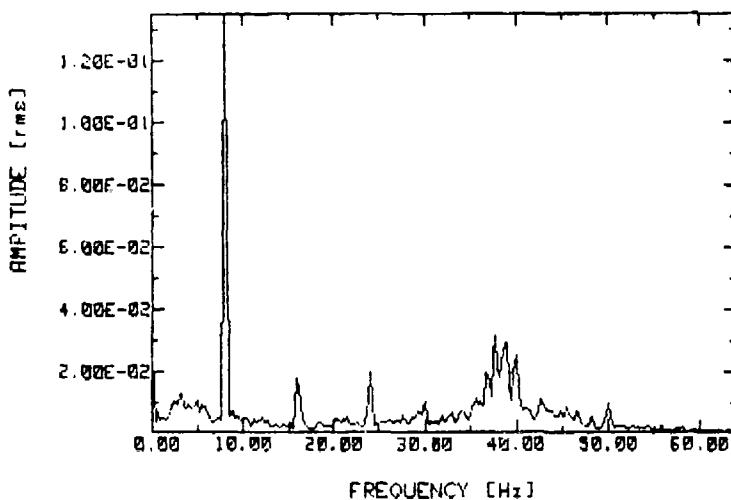


R SPEC 2 DELT_5262

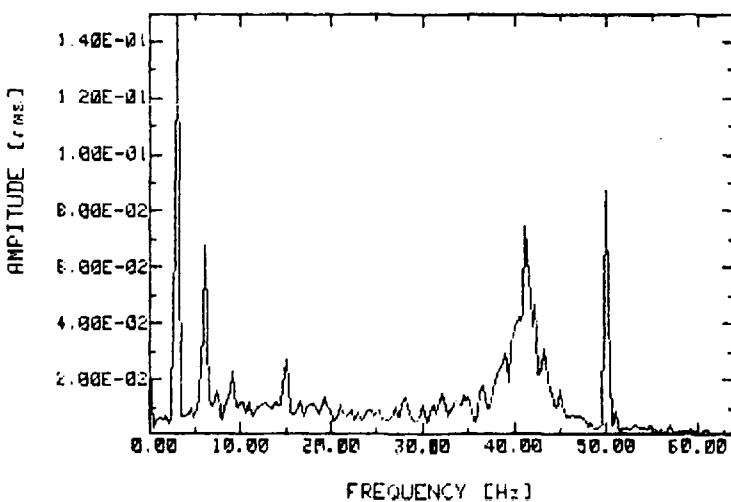
#AV: 10



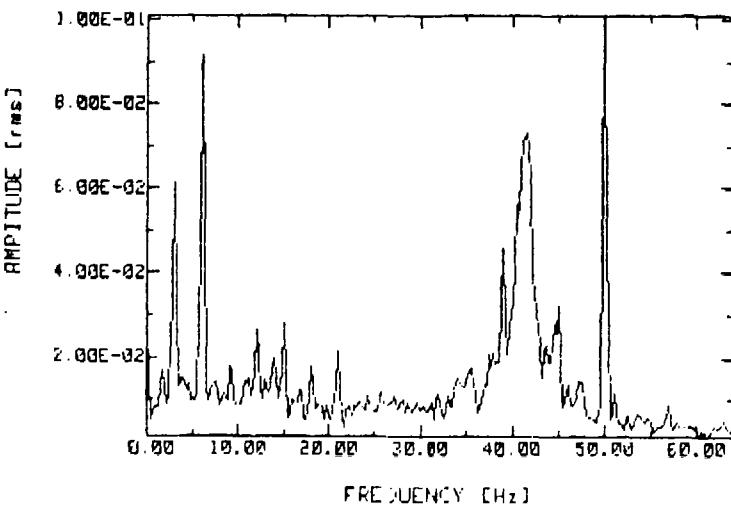
A SPEC 2 DELT_5263 #AV: 10



A SPEC 2 DELT_5270 #AV: 10



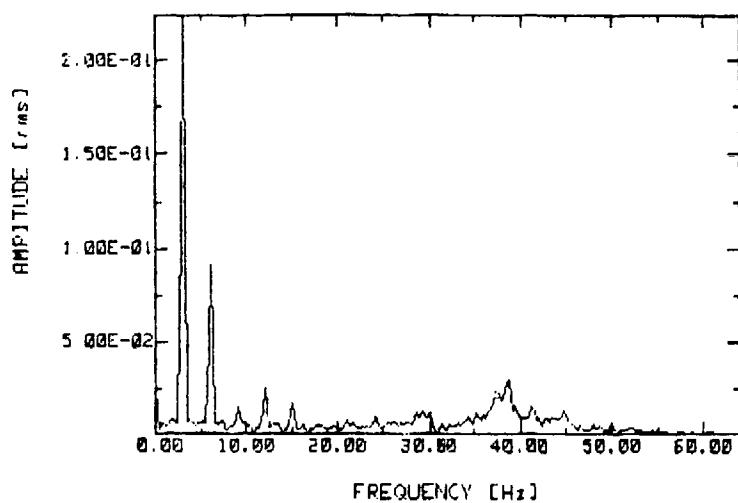
A SPEC 2 DELT_5271 #AV: 10



A SPEC 2

DELT_5272

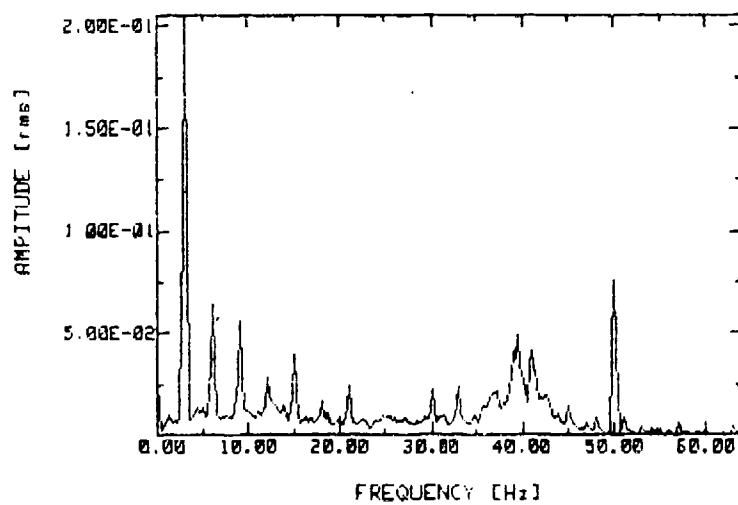
#AV: 10



A SPEC 2

DELT_5273

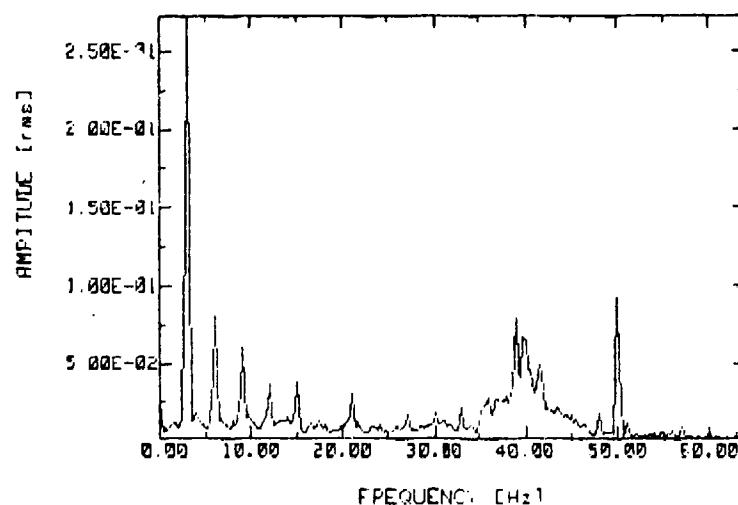
#AV: 10



A SPEC 2

DELT_5274

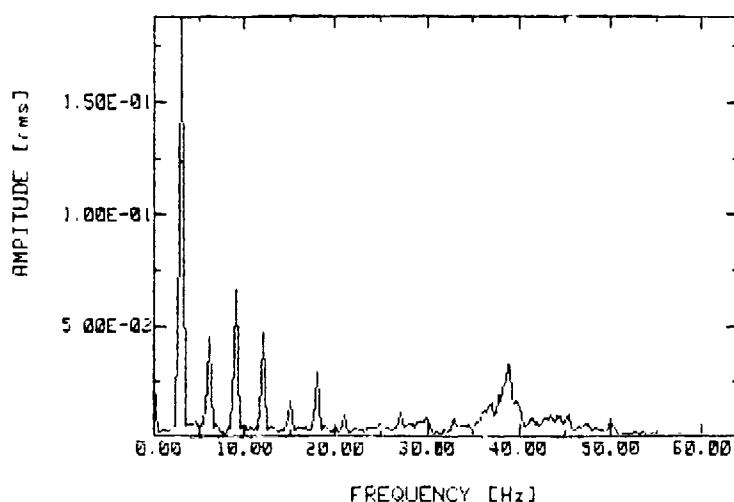
#AV: 10



A SPEC 2

DELT_6201

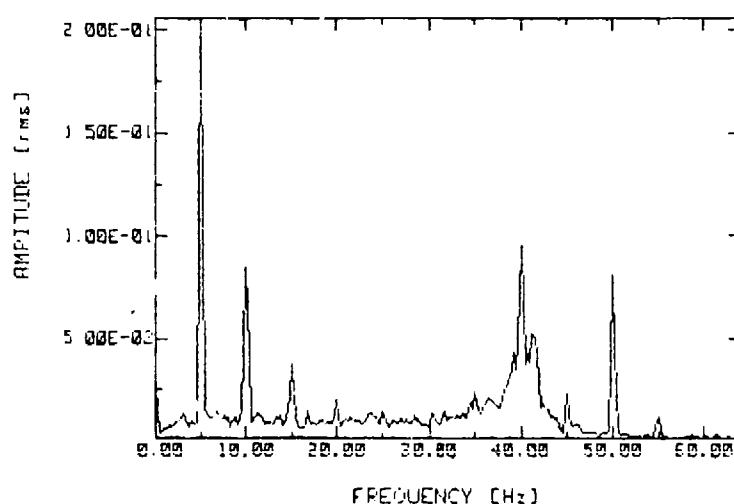
#AV: 10



A SPEC 2

DELT_6205

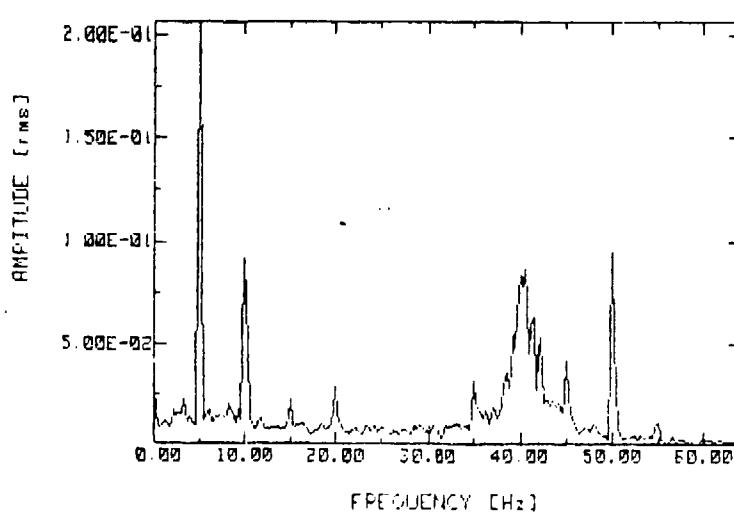
#AV: 10



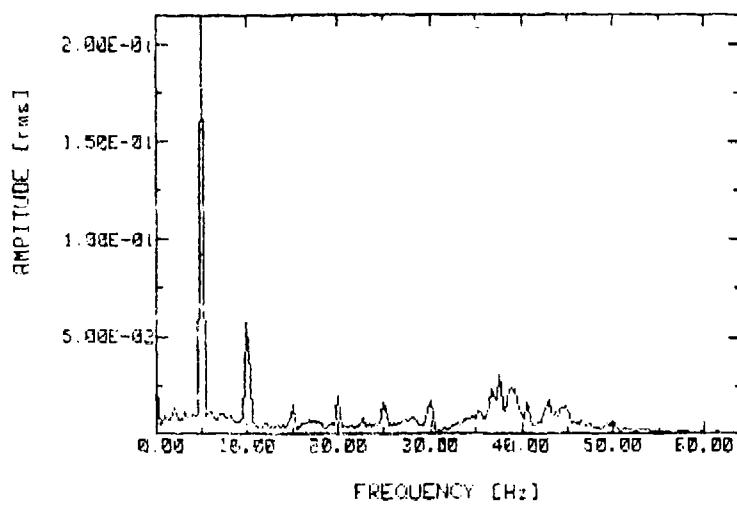
A SPEC 2

DELT_6206

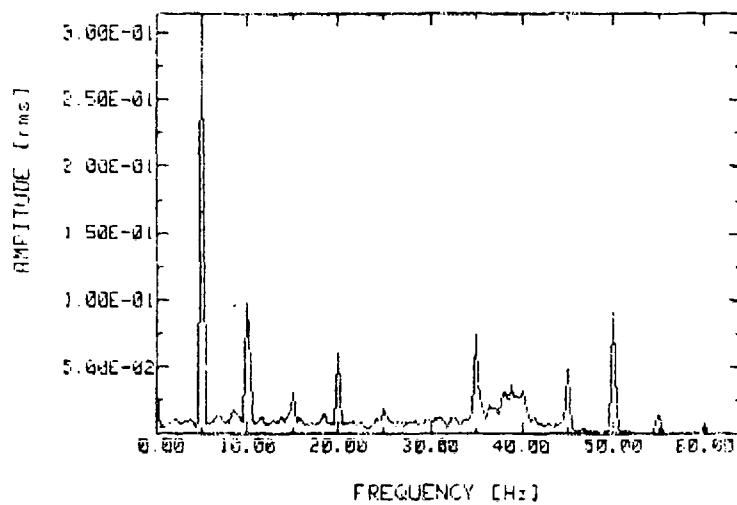
#AV: 10



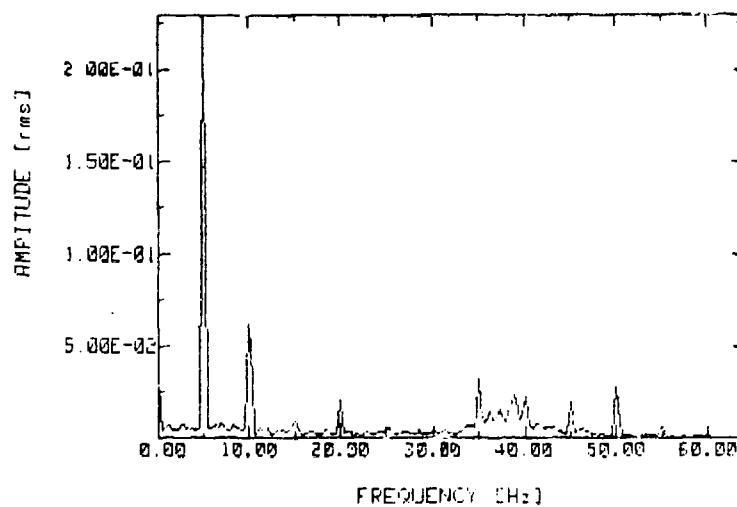
A SPEC 2 DELT_6207 #AV: 10



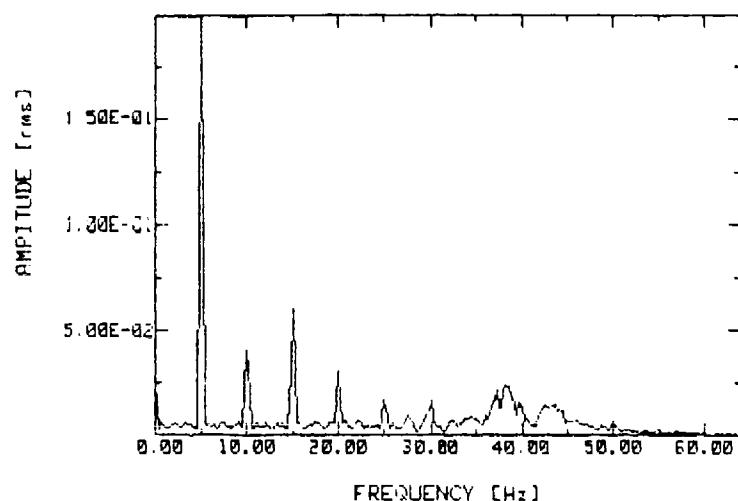
A SPEC 2 DELT_6200 #AV: 10



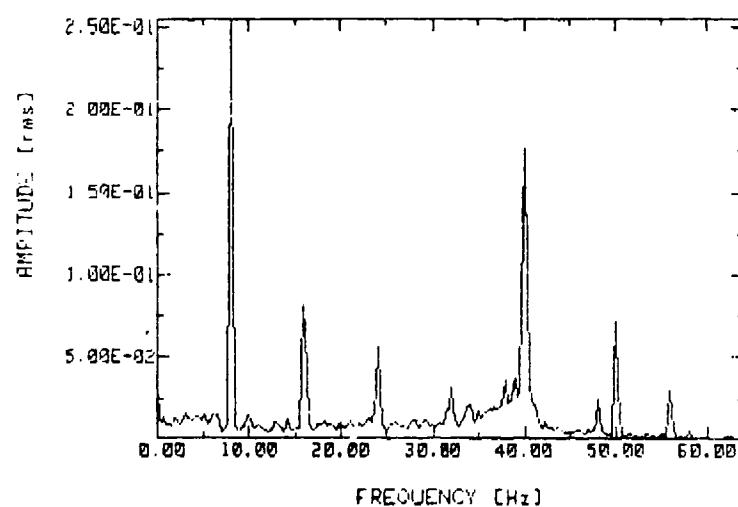
A SPEC 2 DELT_6209 #AV: 10



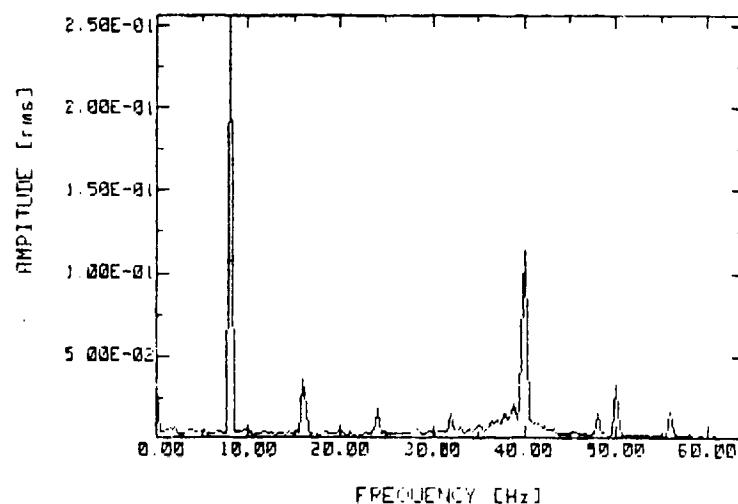
A SPEC 2 DELT_6210 #AV: 10



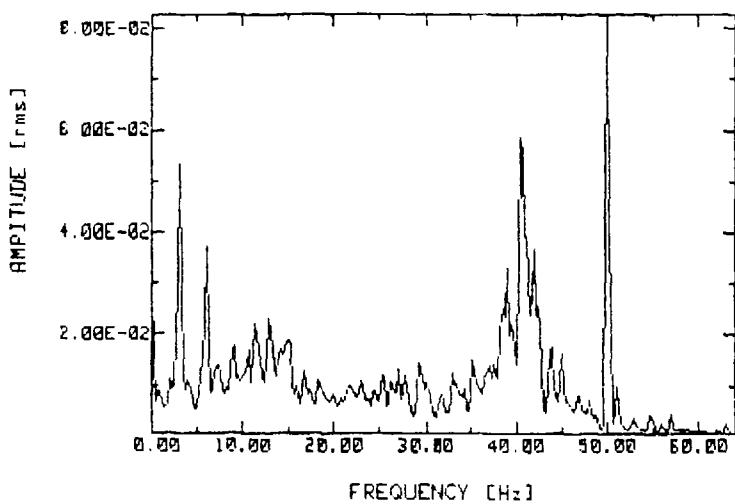
A SPEC 2 DELT_6217 #AV: 10



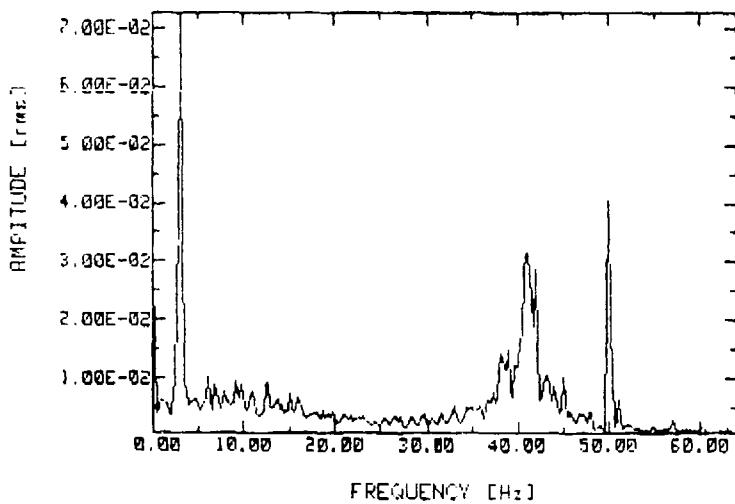
A SPEC 2 DELT_6218 #AV: 10



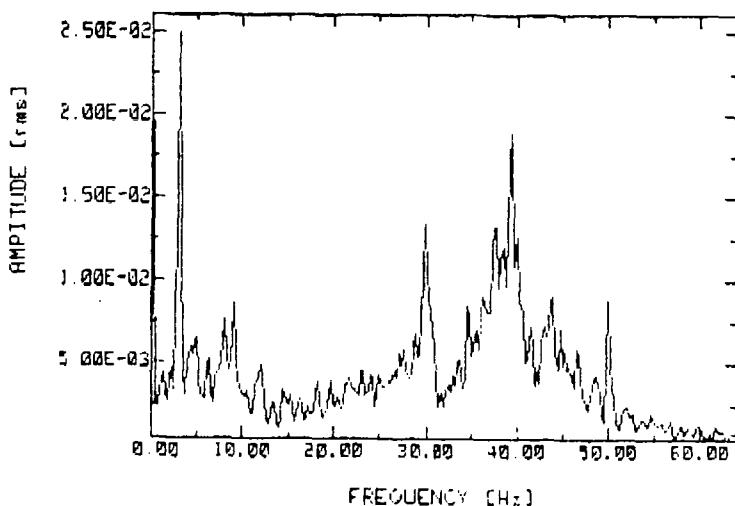
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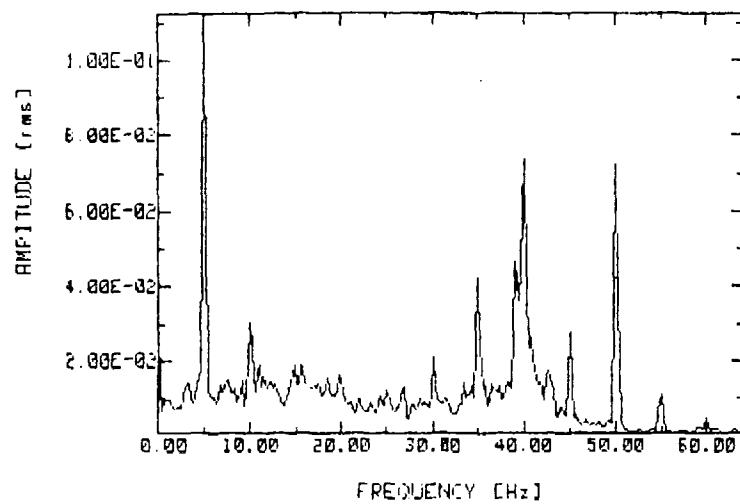
R SPEC 2 DELT_6226 #AV: 10



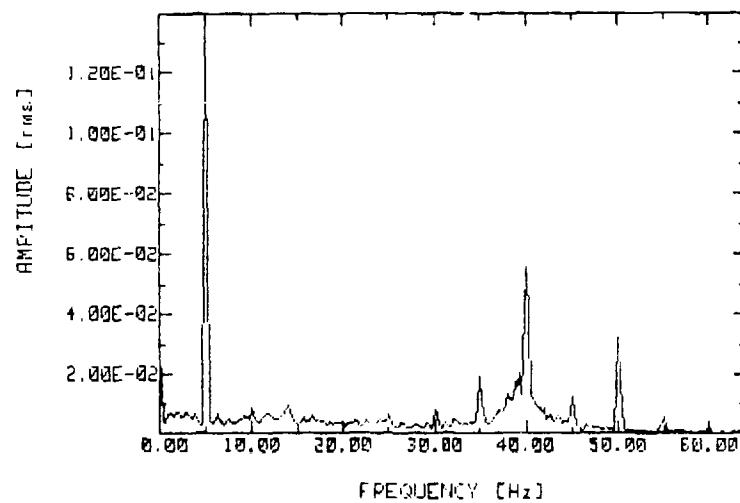
R SPEC 2 DELT_6227 #AV: 10



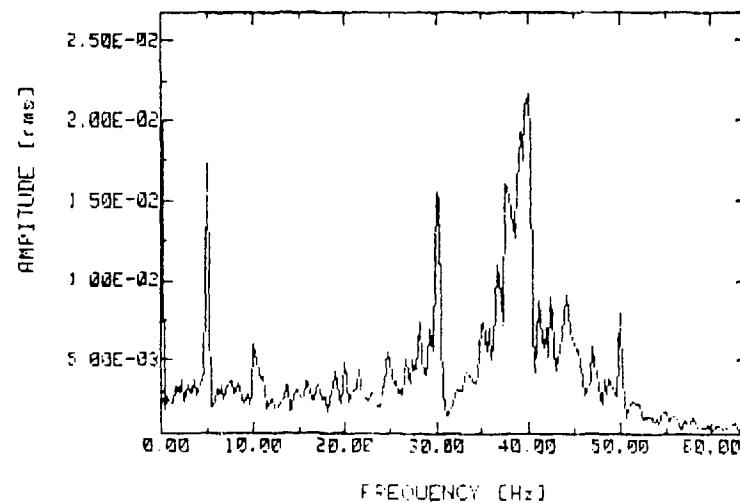
A SPEC 2 DELT_6233 #RV: 10



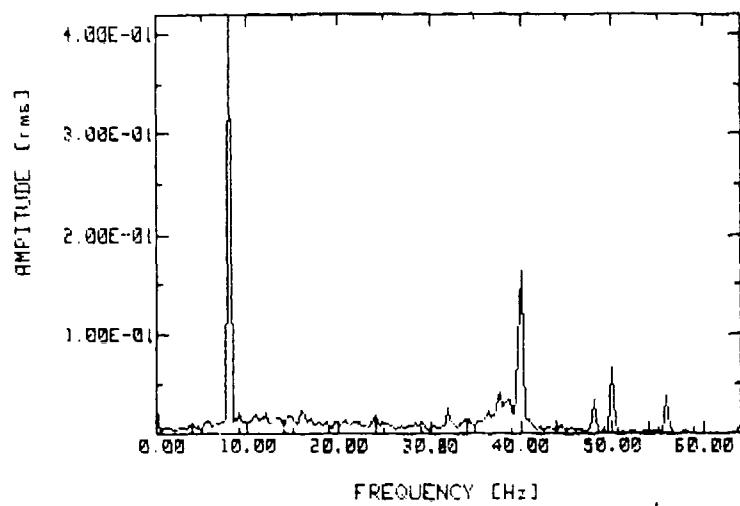
A SPEC 2 DELT_6234 #RV: 10



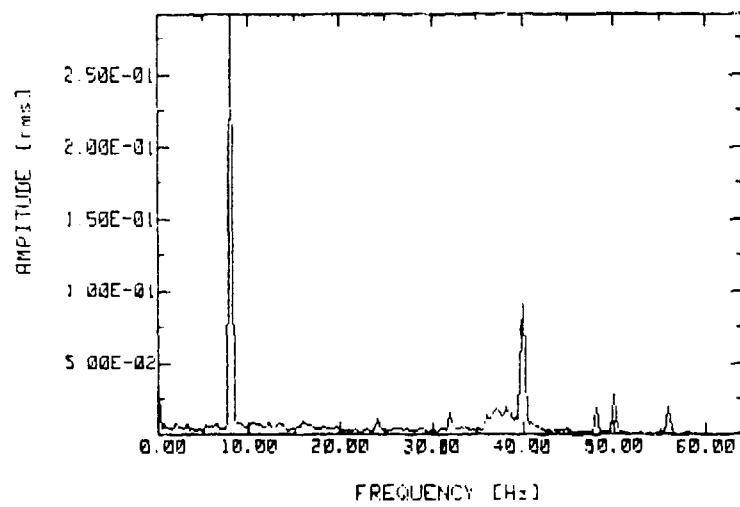
A SPEC 2 DELT_6235 #RV: 10



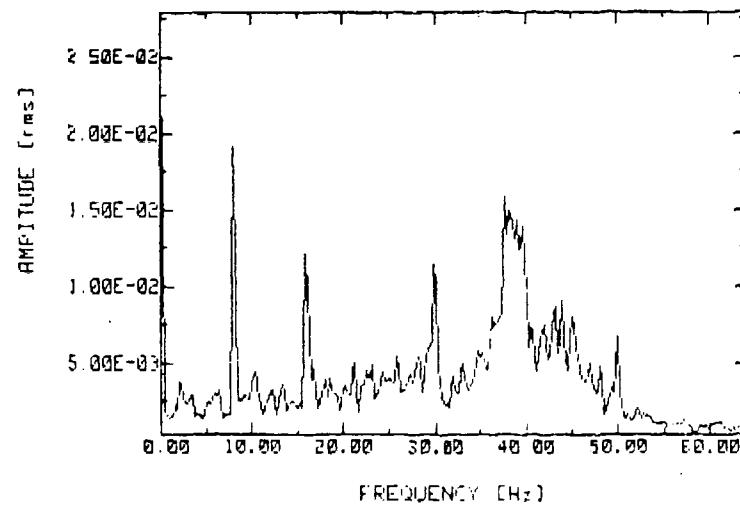
A SPEC 2 DELT_6242 #AV: 10



A SPEC 2 DELT_6243 #AV: 10

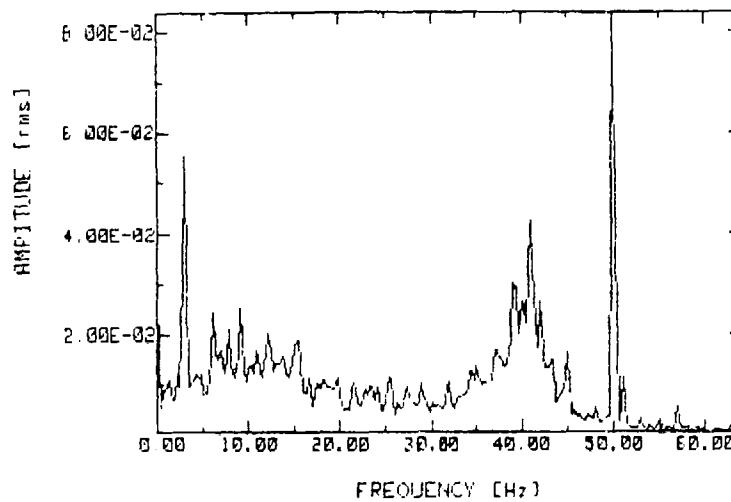


A SPEC 2 DELT_6244 #AV: 10



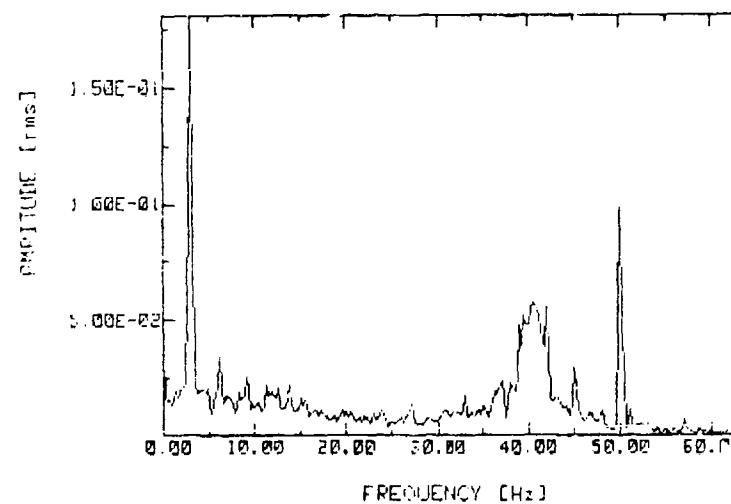
R SPEC 2 DELT_6251

#RV: 10



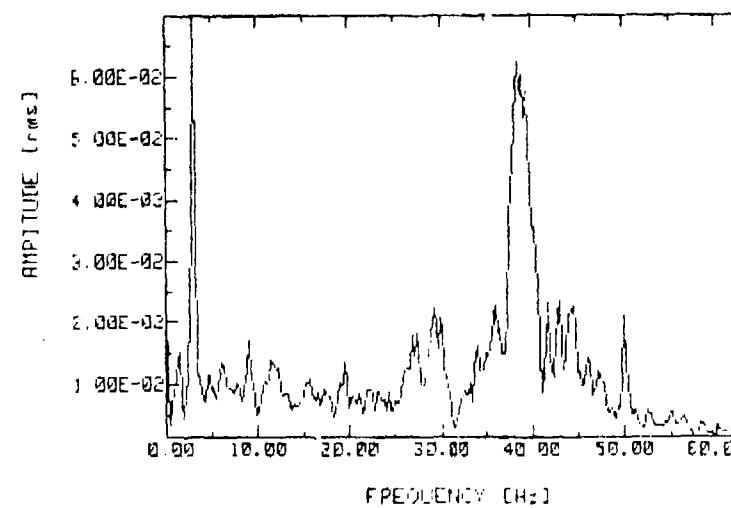
R SPEC 2 DELT_6252

#RV: 10



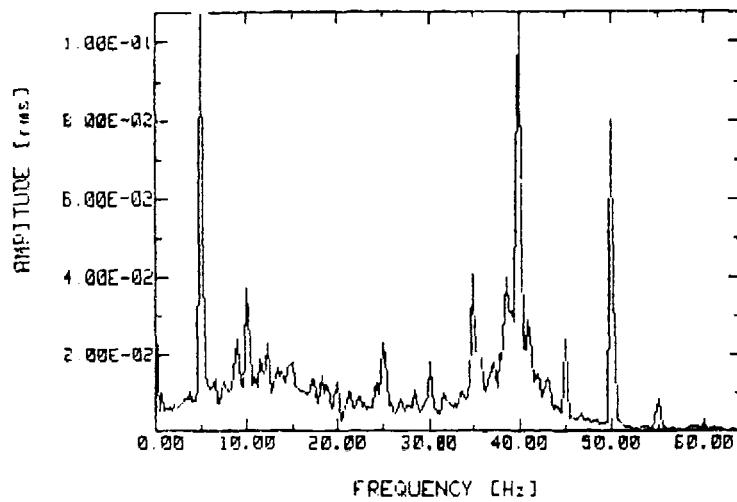
R SPEC 2 DELT_6253

#RV: 10



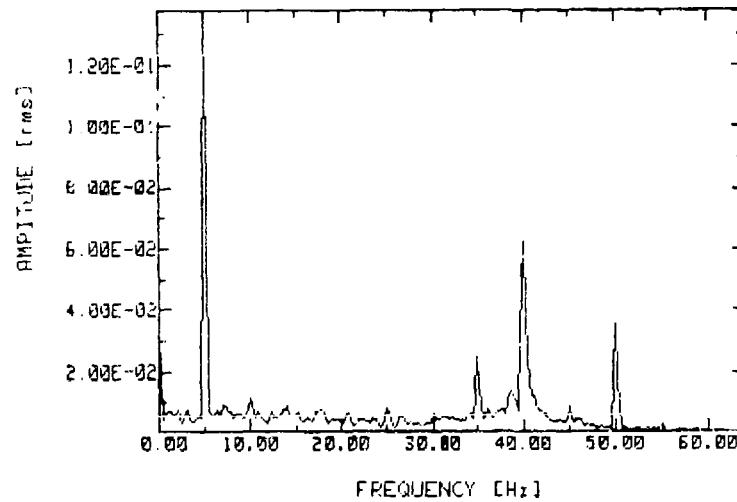
A SPEC 2 DELT_6257

#AV: 10



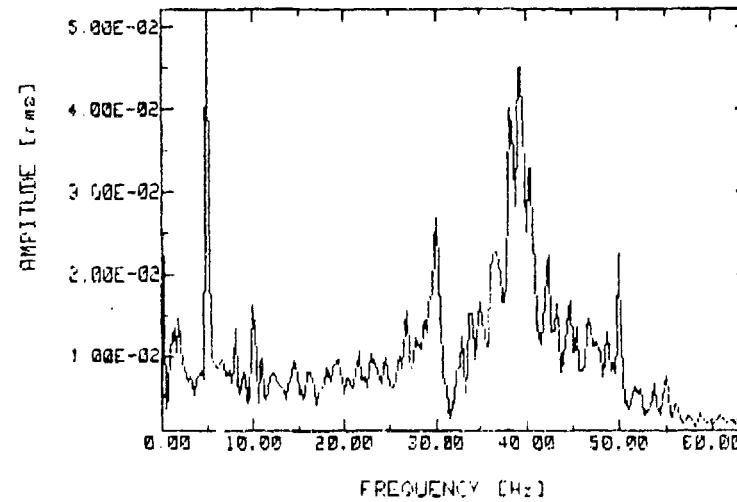
A SPEC 2 DELT_6258

#AV: 10



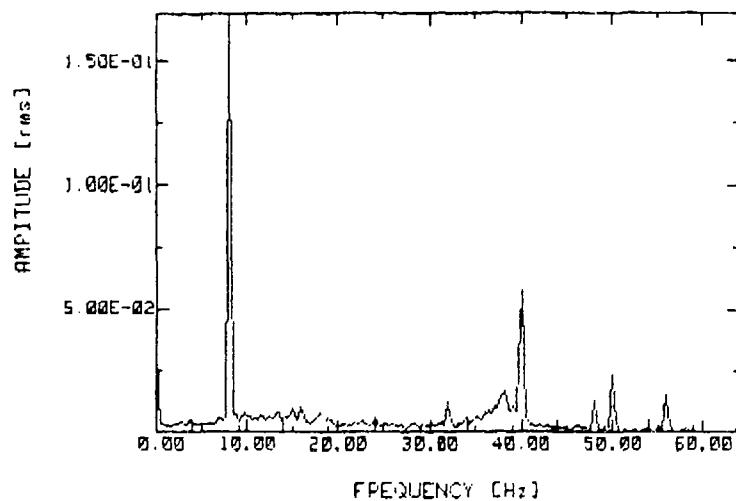
A SPEC 2 DELT_6259

#AV: 10

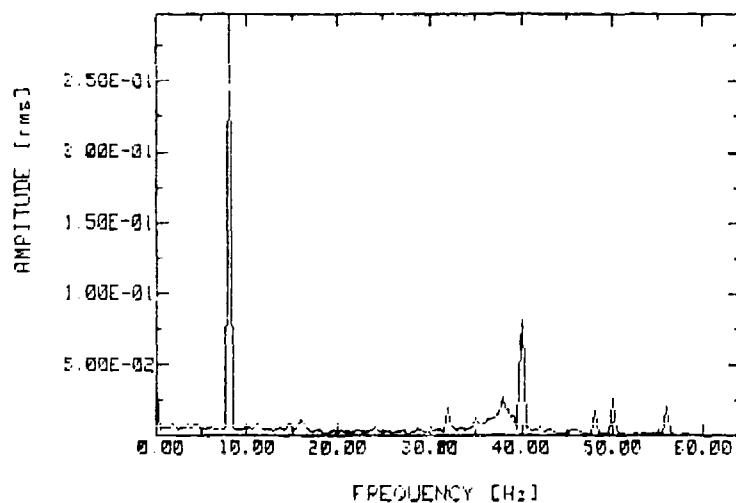


-55--

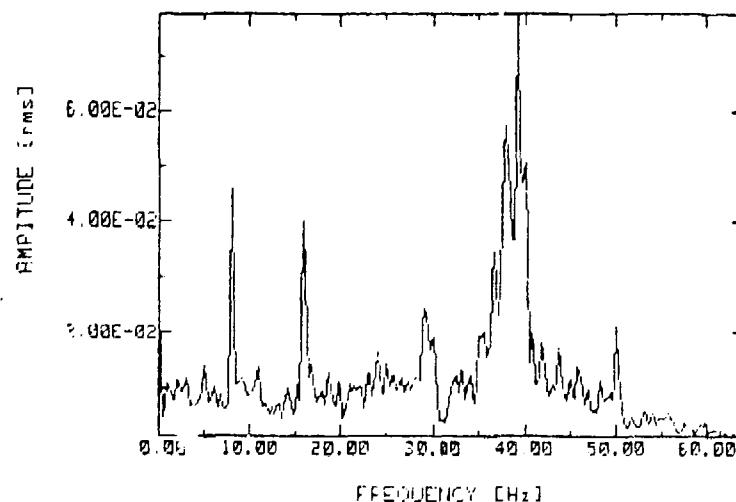
A SPEC 2 DELT_6266 #RV: 10



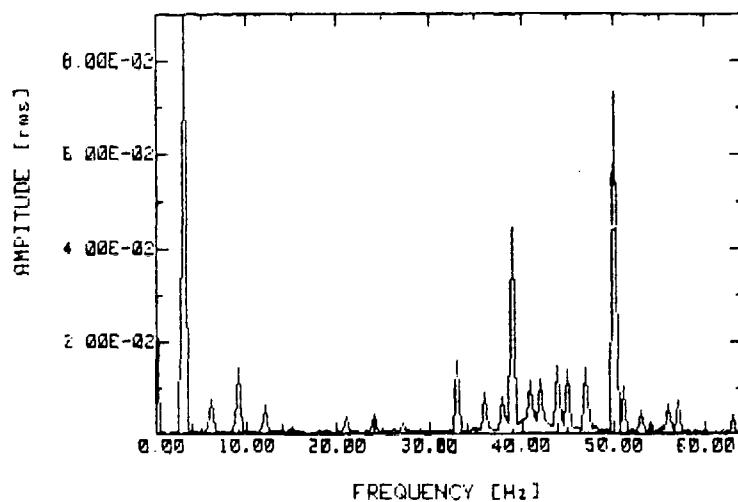
A SPEC 2 DELT_6267 #RV: 10



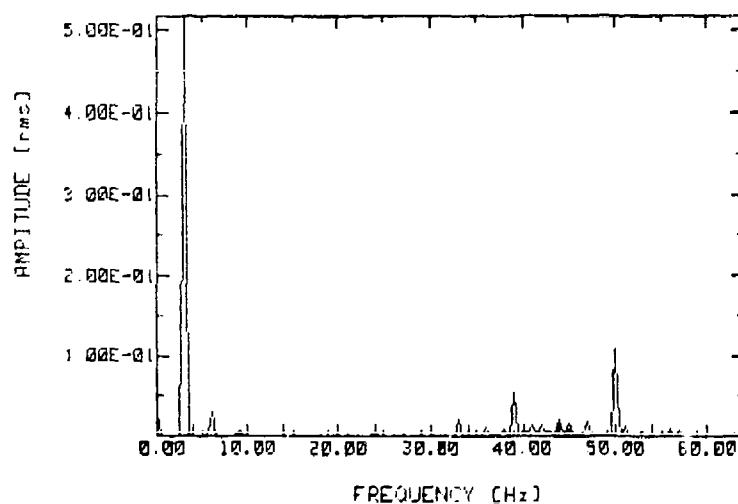
A SPEC 2 DELT_6268 #RV: 10



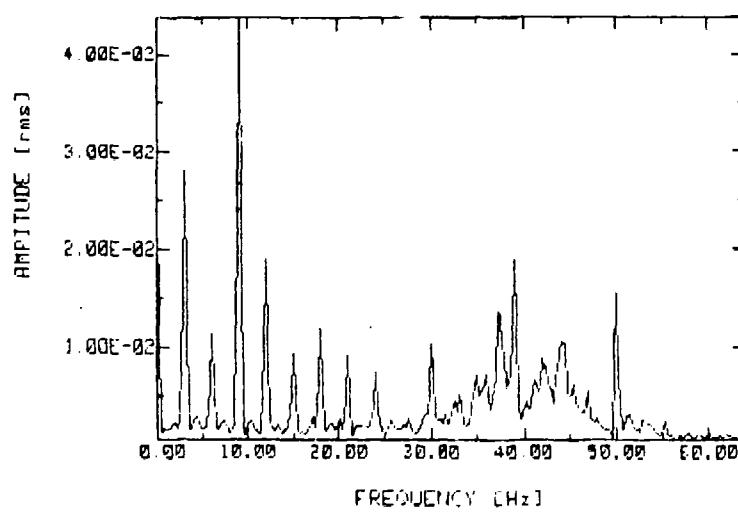
A SPEC 2 DELT_7104 #RV: 10



A SPEC 2 DELT_7105 #RV: 10

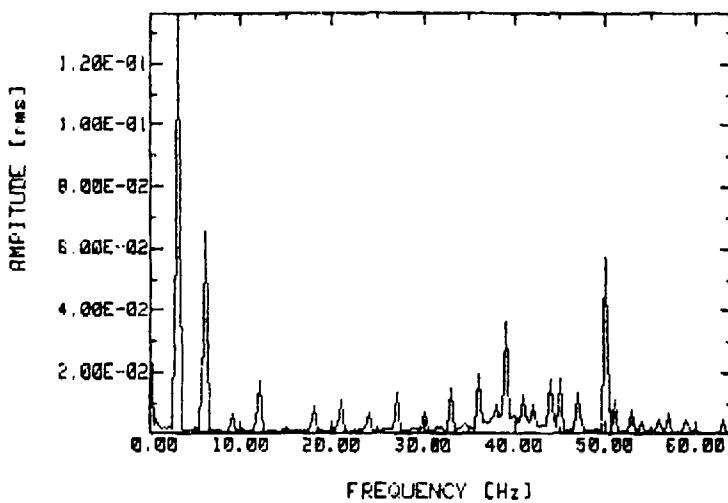


A SPEC 2 DELT_7106 #RV: 10



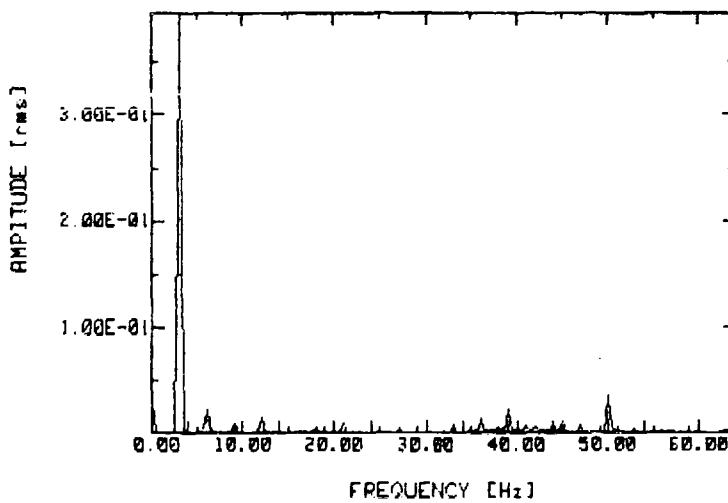
A SPEC 2 DELT_7107

#AV: 10



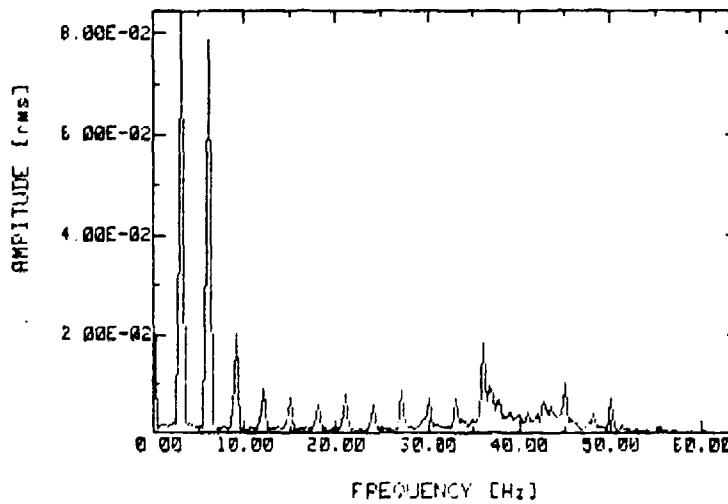
A SPEC 2 DELT_7108

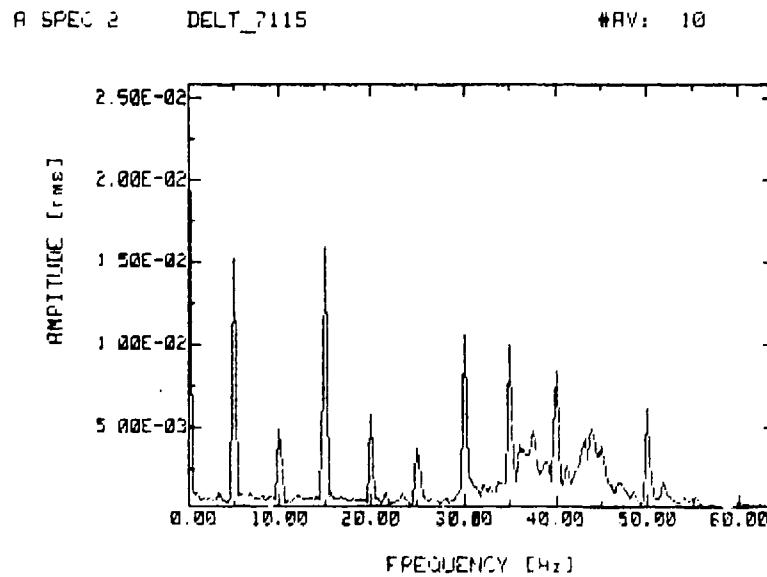
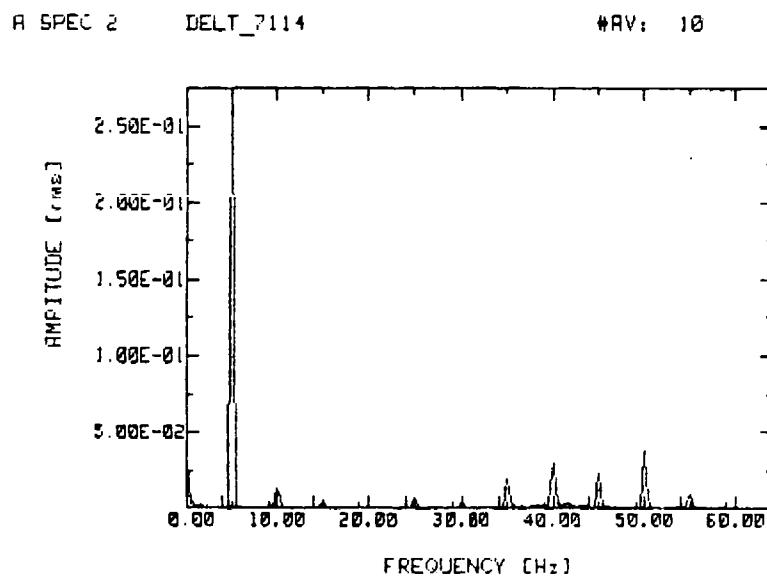
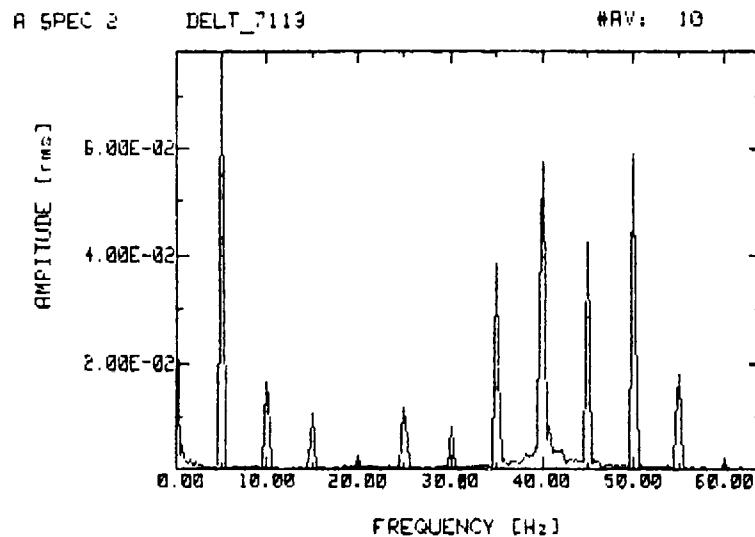
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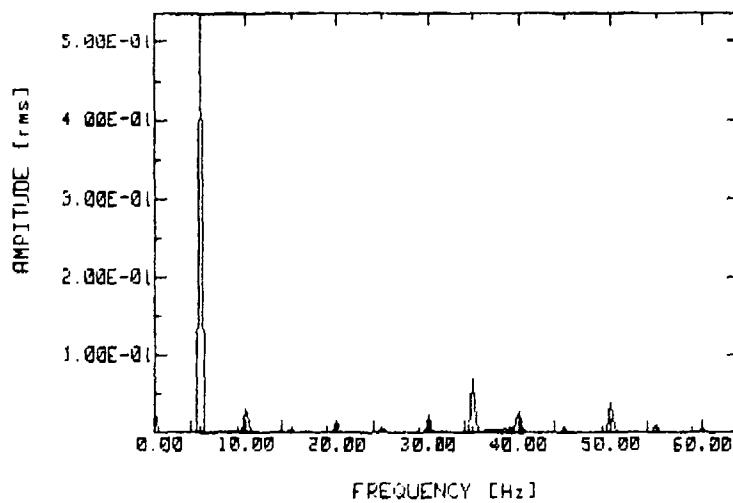
A SPEC 2 DELT_7109

#AV: 10

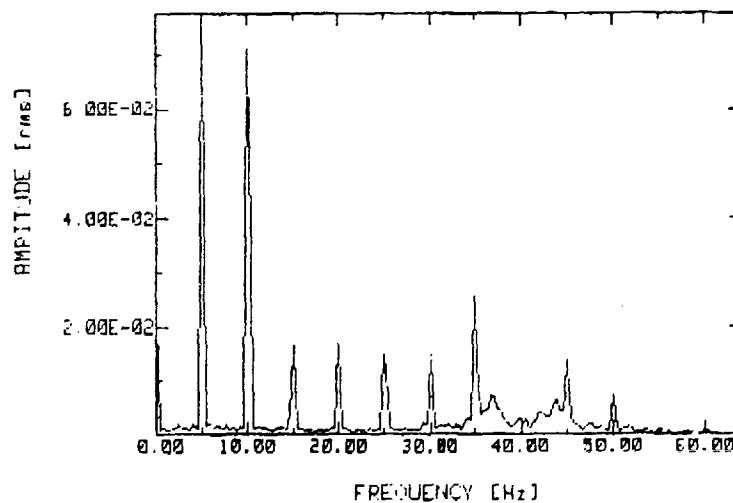




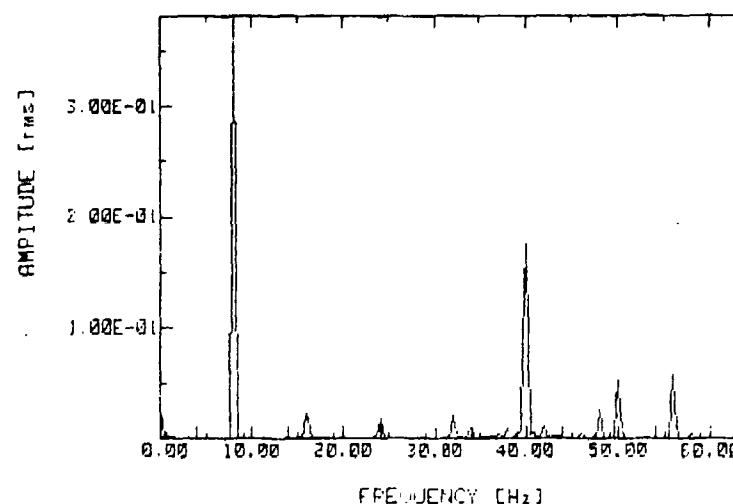
R SPEC 2 DELT_7116 #AV: 10



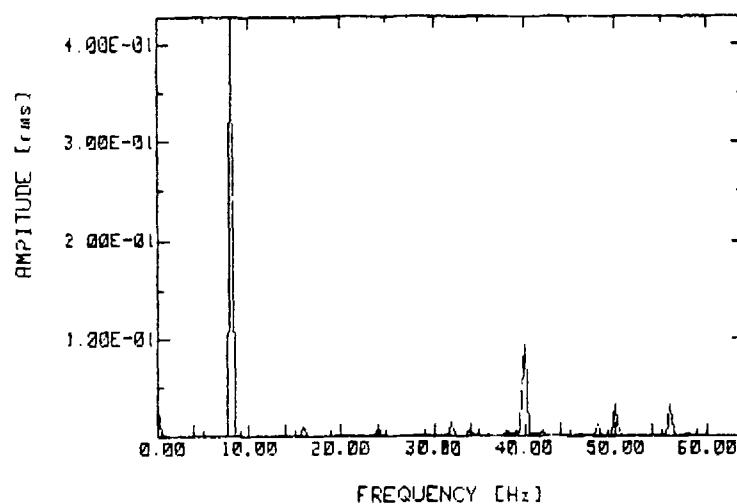
R SPEC 2 DELT_7117 #AV: 10



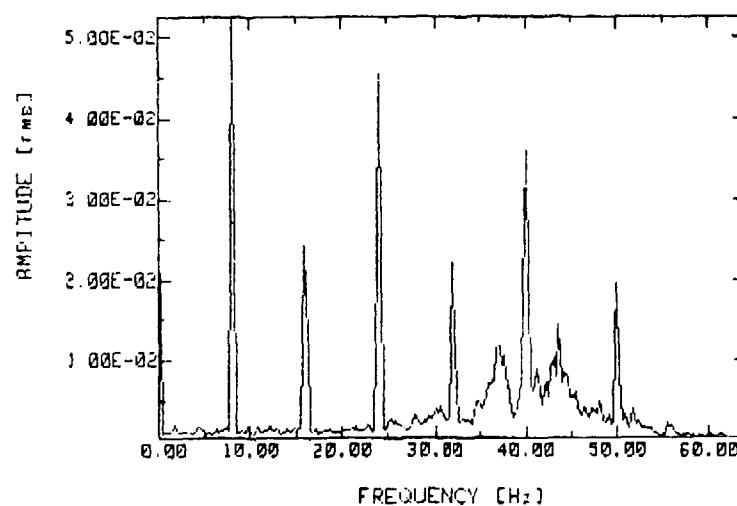
R SPEC 2 DELT_7124 #AV: 10



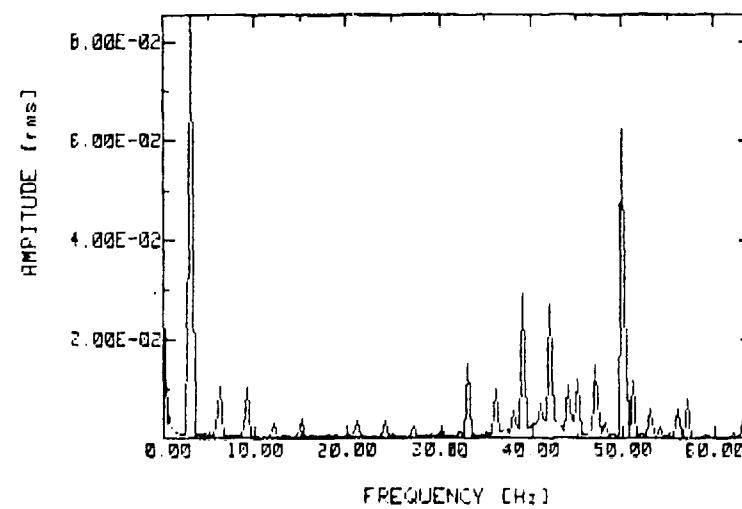
A SPEC 2 DELT_7125 #AV: 10



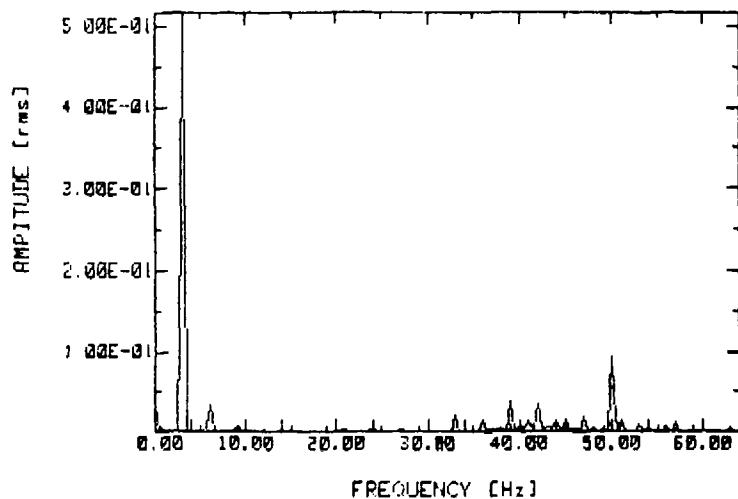
A SPEC 2 DELT_7126 #AV: 10



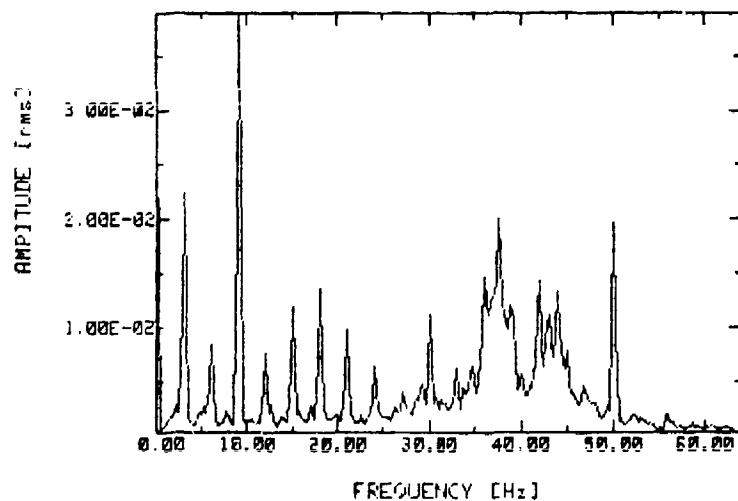
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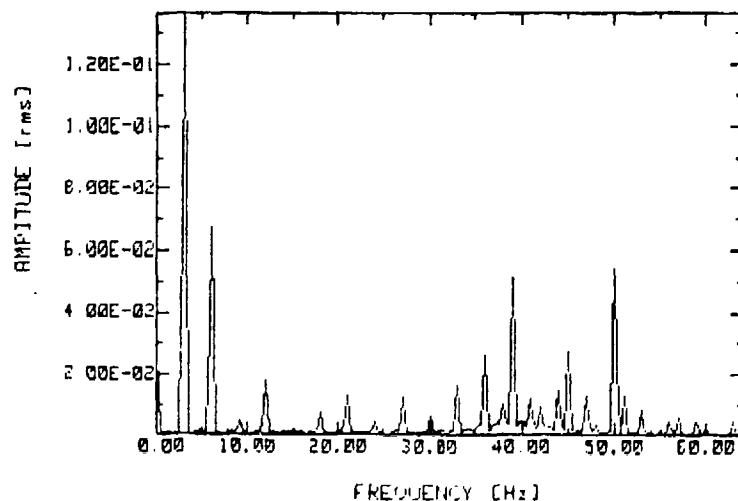
A SPEC 2 DELT_7194 #AV: 10



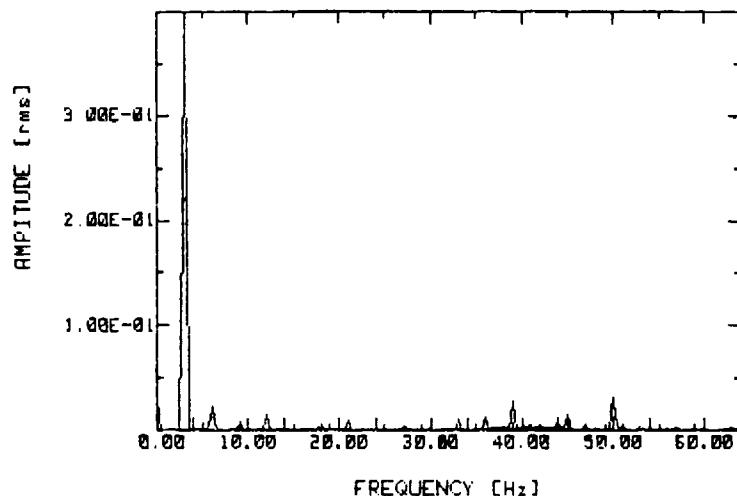
A SPEC 2 DELT_7195 #AV: 10



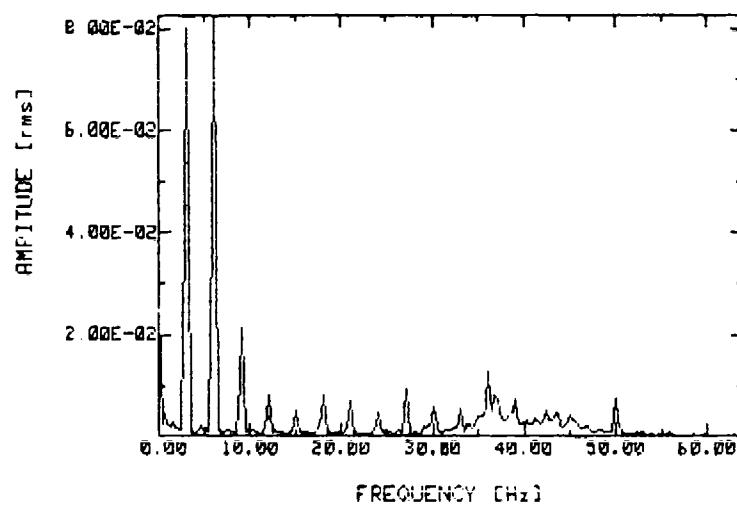
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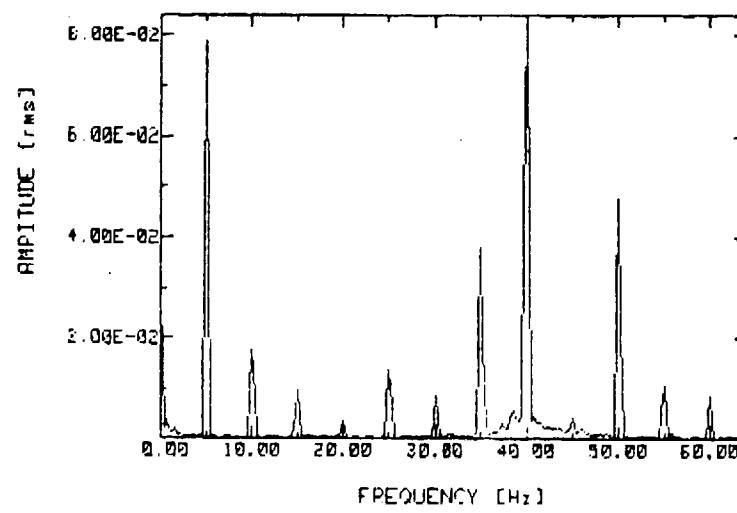
A SPEC 2 DELT_7137 #AV: 10



A SPEC 2 DELT_7138 #AV: 10

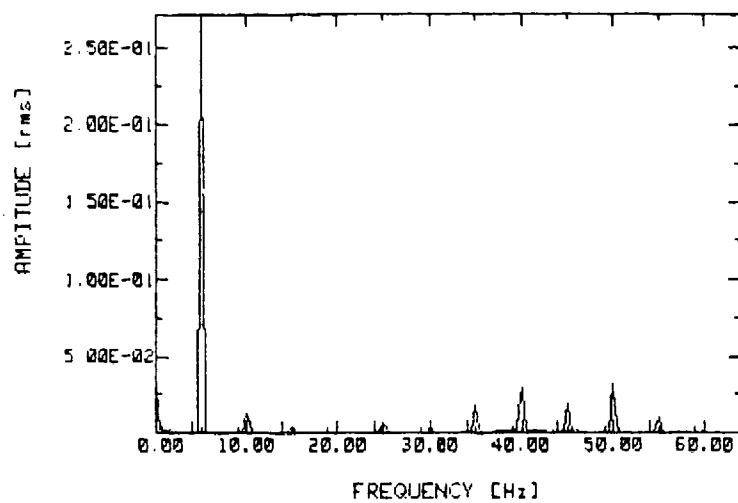


A SPEC 2 DELT_7142 #AV: 10



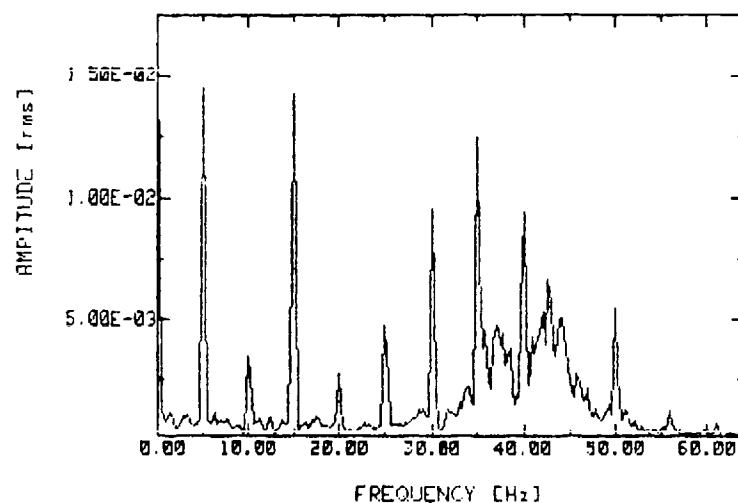
A SPEC 2 DELT_7143

#AV: 10



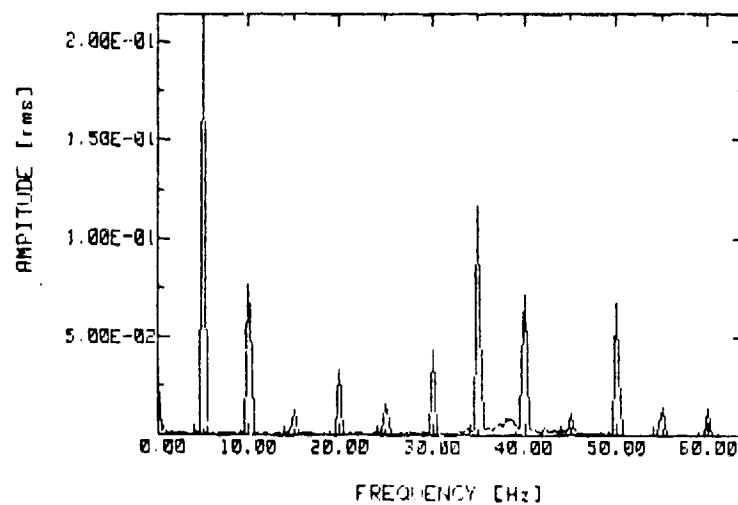
A SPEC 2 DELT_7144

#AV: 10



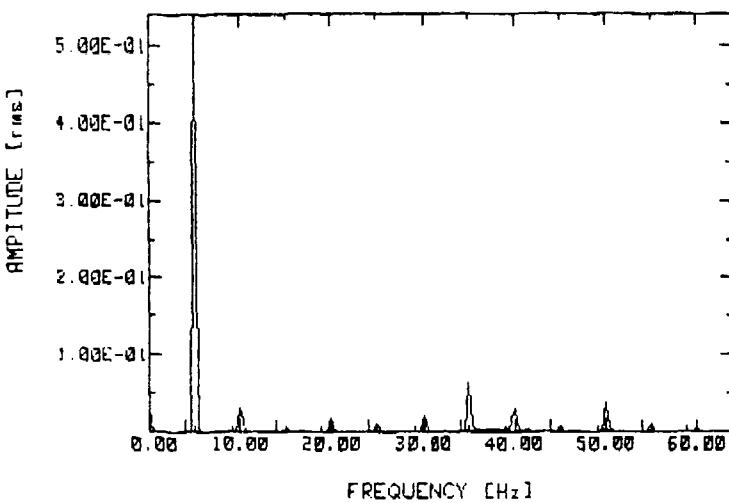
A SPEC 2 DELT_7145

#AV: 10



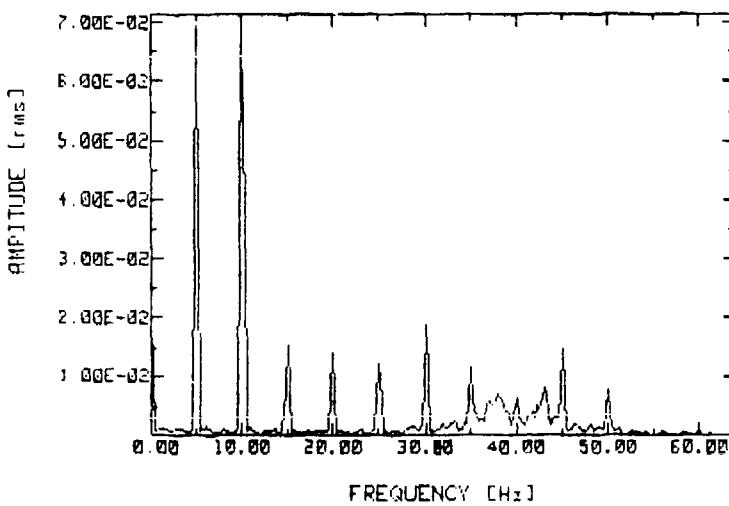
A SPEC 2 DELT_7146

#AV: 10



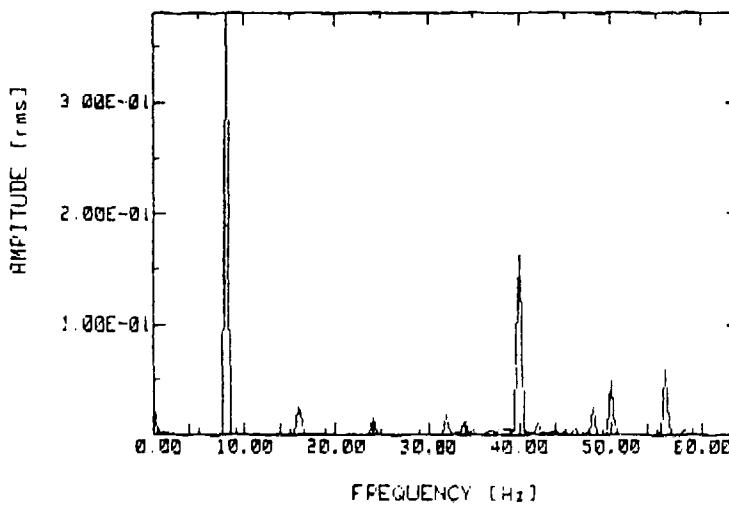
A SPEC 2 DELT_7147

#AV: 10

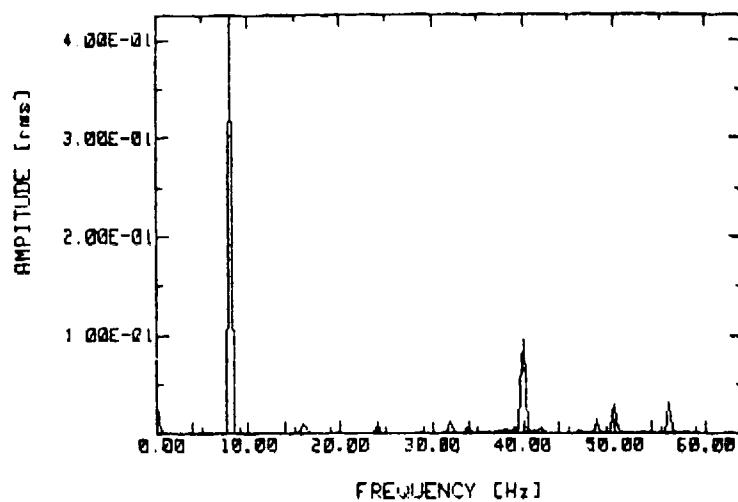


A SPEC 2 DELT_7153

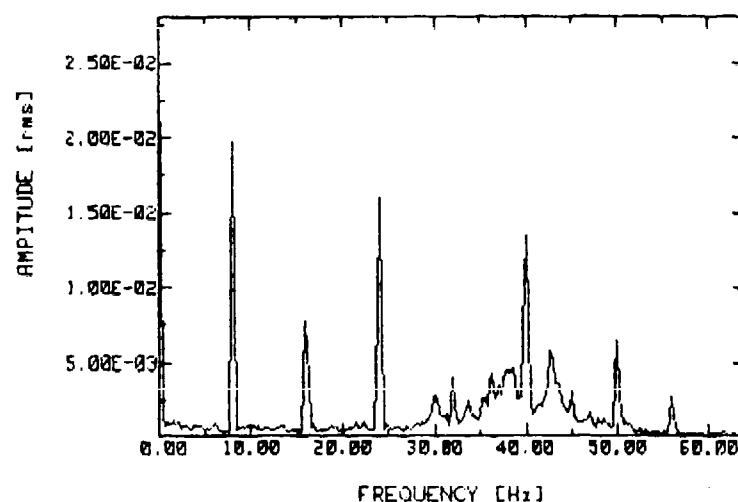
#AV: 10



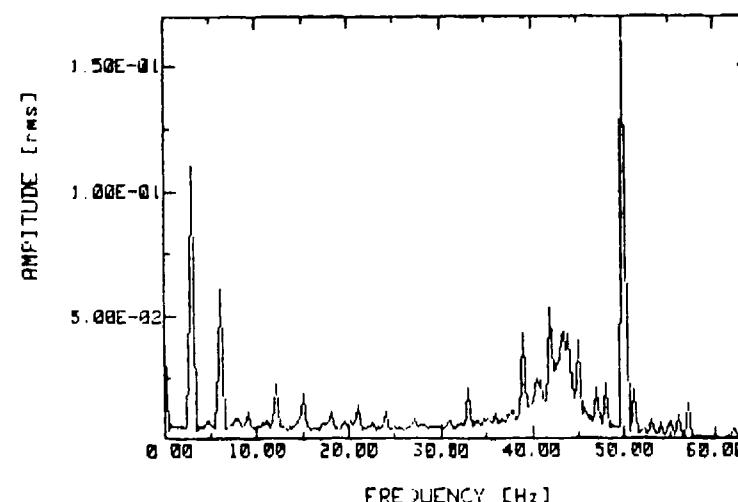
A SPEC 2 DELT_7154 #AV: 10



A SPEC 2 DELT_7155 #AV: 10

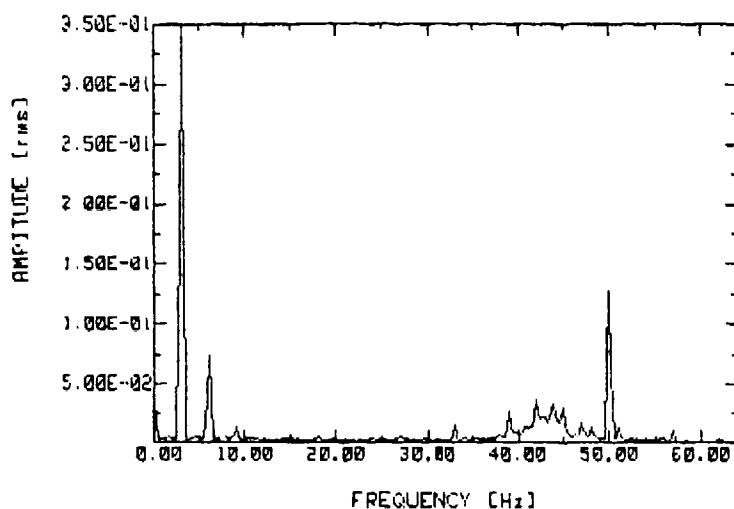


A SPEC 2 DELT_7162 #AV: 20



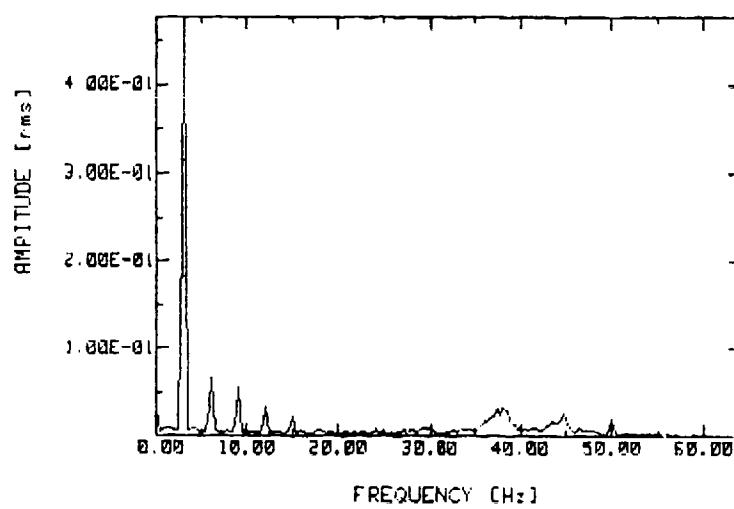
R SPEC 3 DELT_7163

#AV: 20



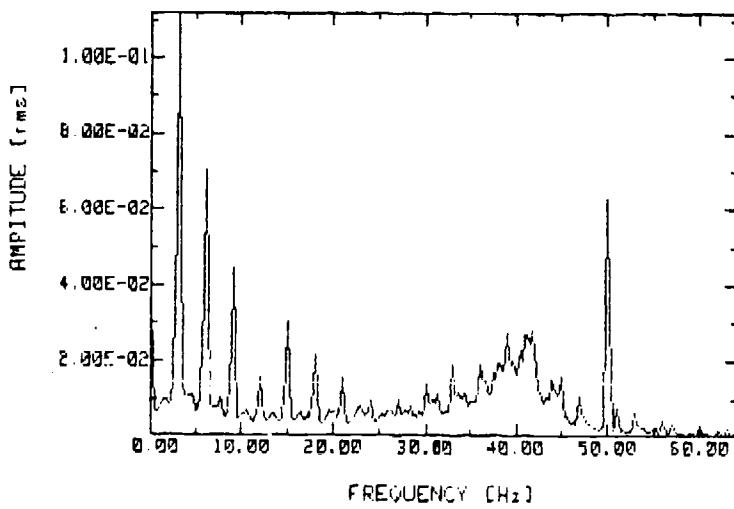
R SPEC 2 DELT_7164

#AV: 20

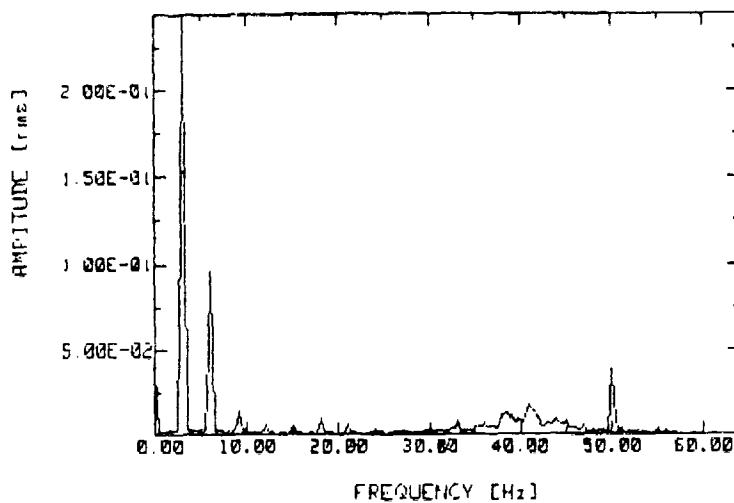


R SPEC 2 DELT_7165

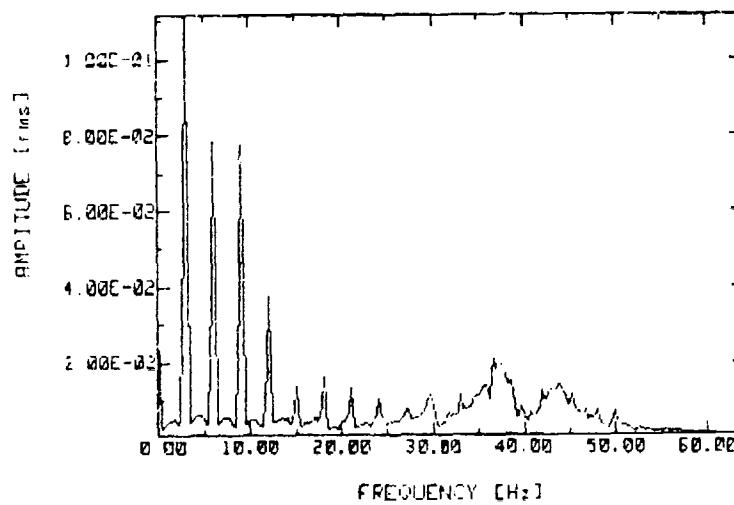
#AV: 20



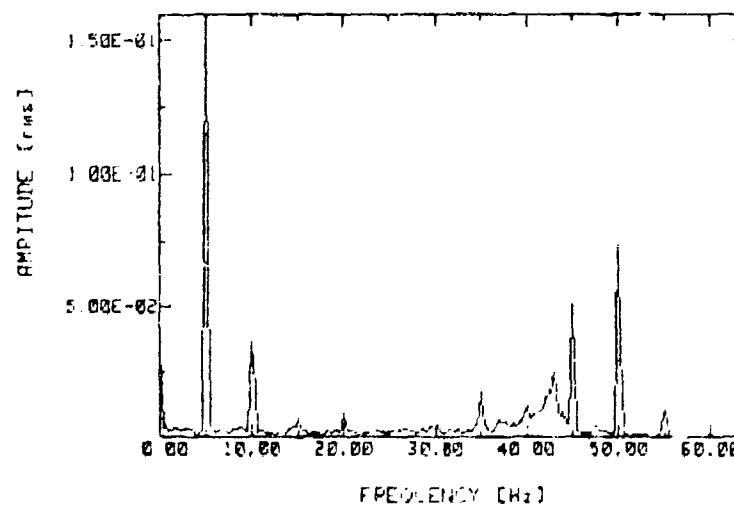
A SPEC 2 DELT_7166 #AV: 20



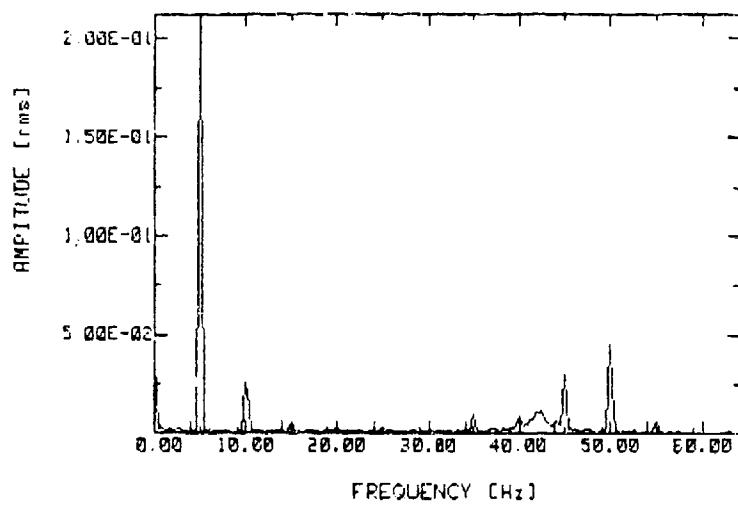
A SPEC 2 DELT_7167 #AV: 20



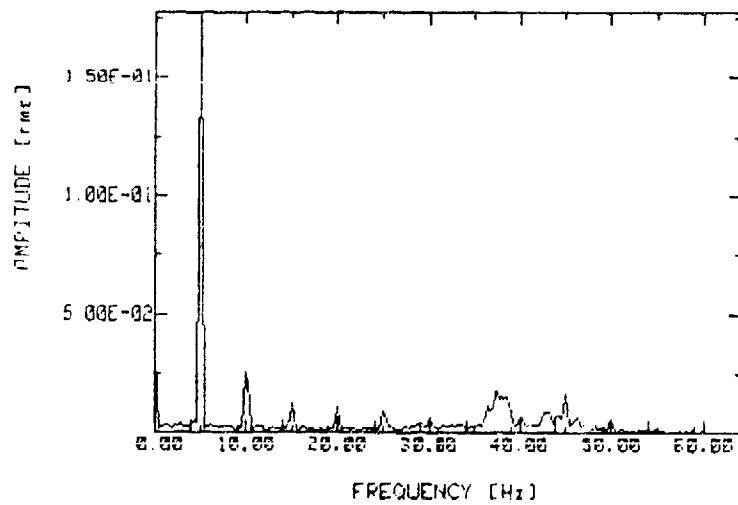
A SPEC 2 DELT_7171 #AV: 10



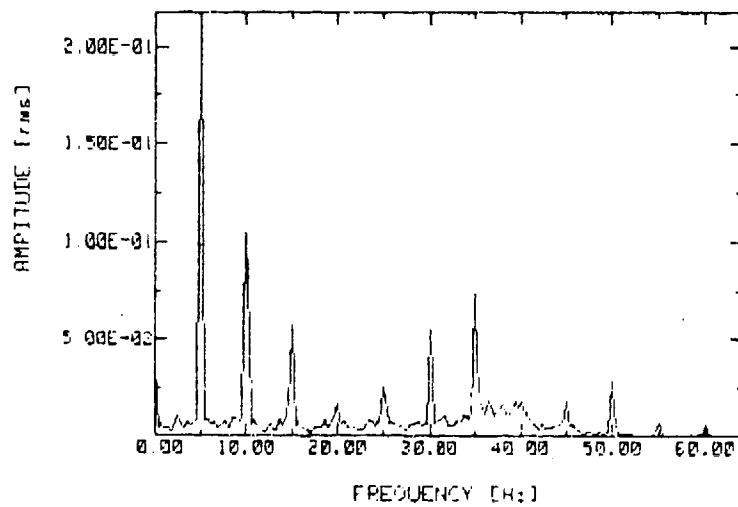
A SPEC 2 DELT_7172 #RV: 10



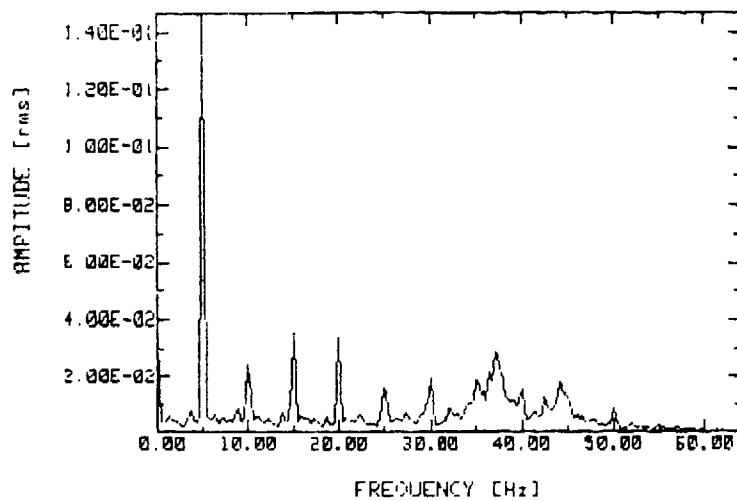
A SPEC 2 DELT_7173 #RV: 10



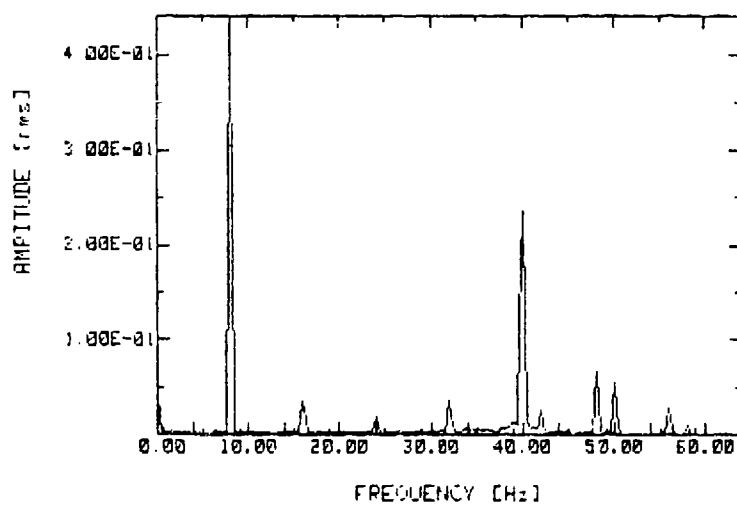
A SPEC 2 DELT_7174 #RV: 10



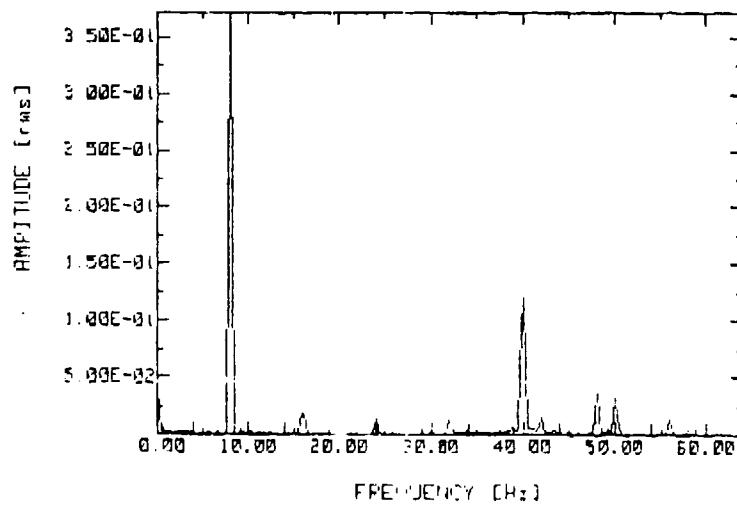
R SPEC 2 DELT_7201 #RV: 10



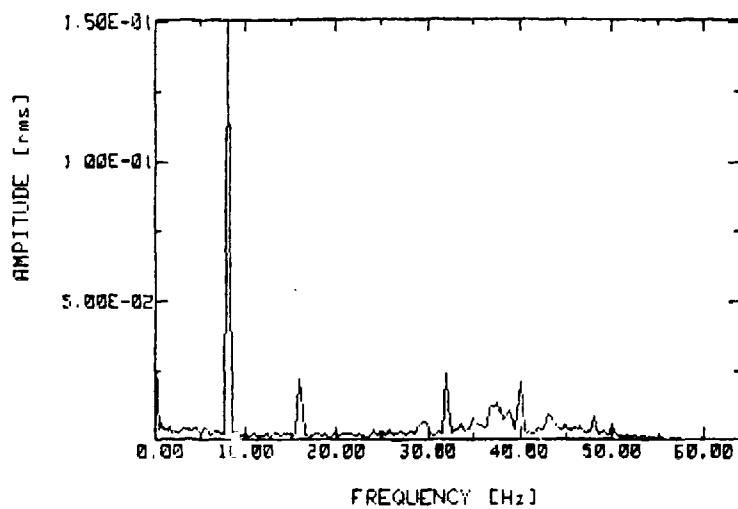
R SPEC 2 DELT_7208 #RV: 10



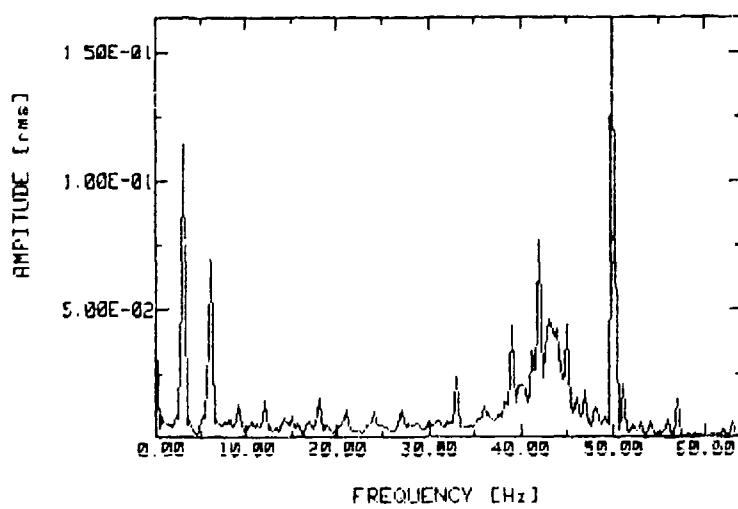
R SPEC 2 DELT_7209 #RV: 10



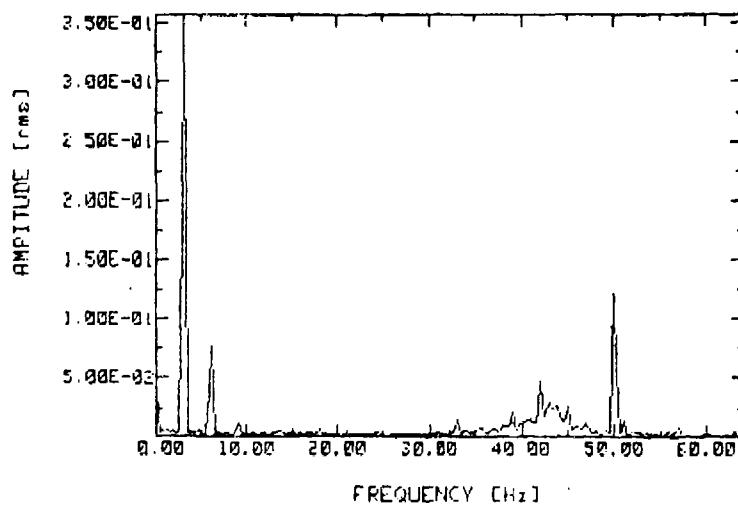
A SPEC 2 DELT_7210 #RV: 10



A SPEC 2 DELT_7217 #RV: 10



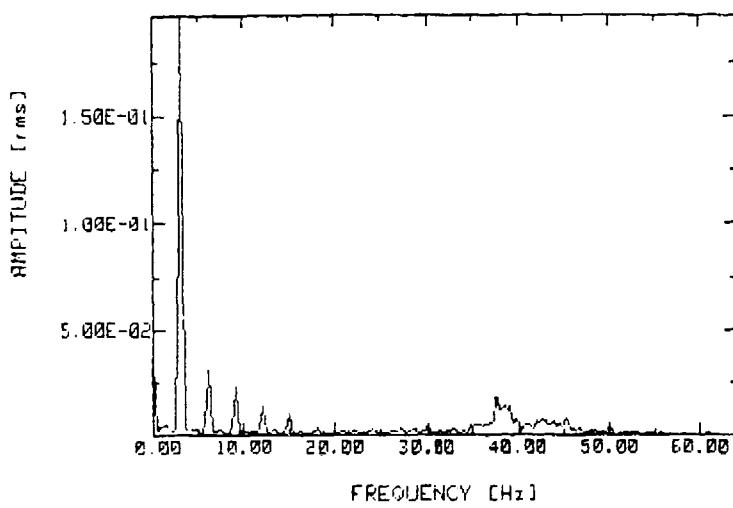
A SPEC 2 DELT_7219 #RV: 10



A SPEC 2

DELT_7219

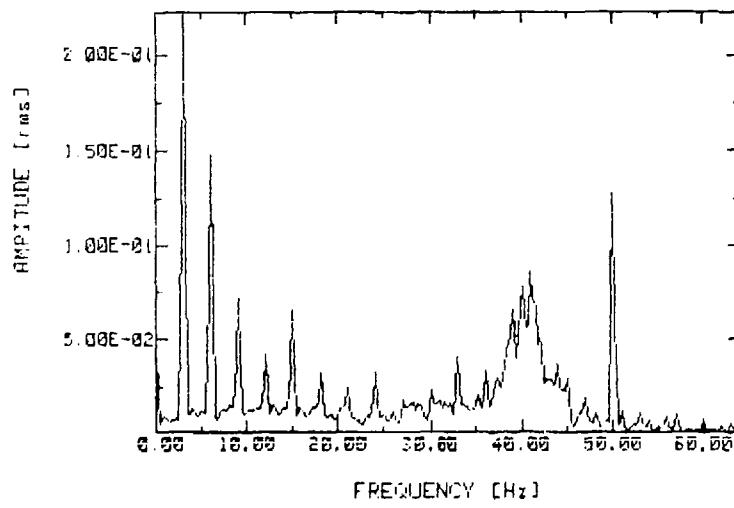
#AV: 10



A SPEC 2

DELT_7220

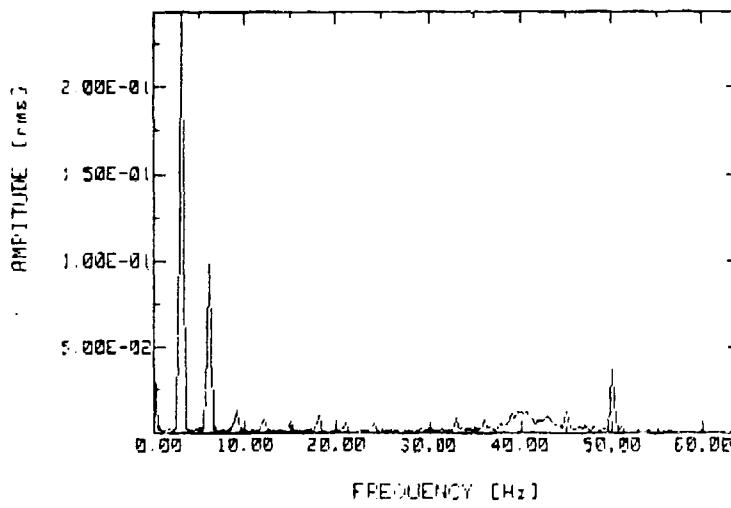
#AV: 10



A SPEC 2

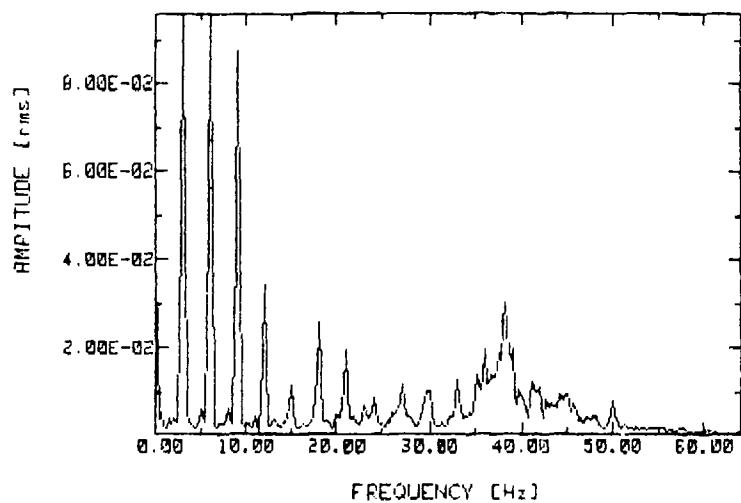
DELT_7221

#AV: 10



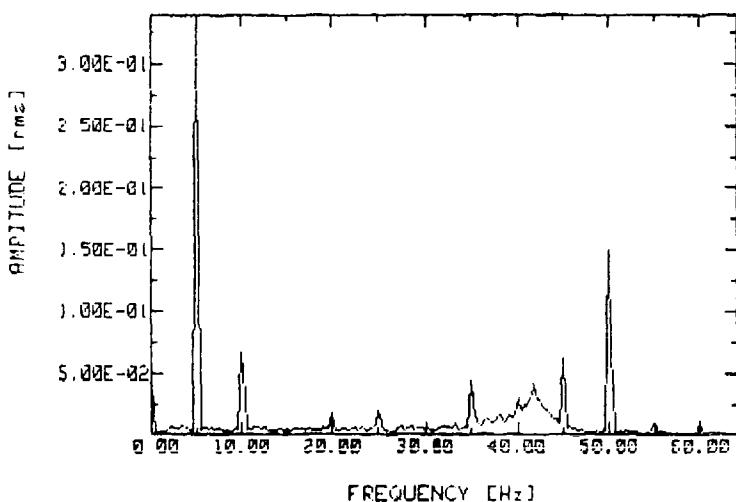
A SPEC 2 DELT_7232

#AV: 10



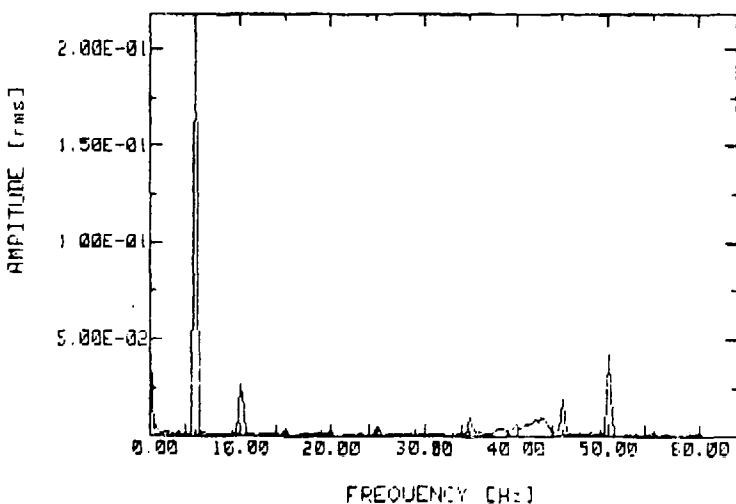
A SPEC 2 DELT_7226

#AV: 10

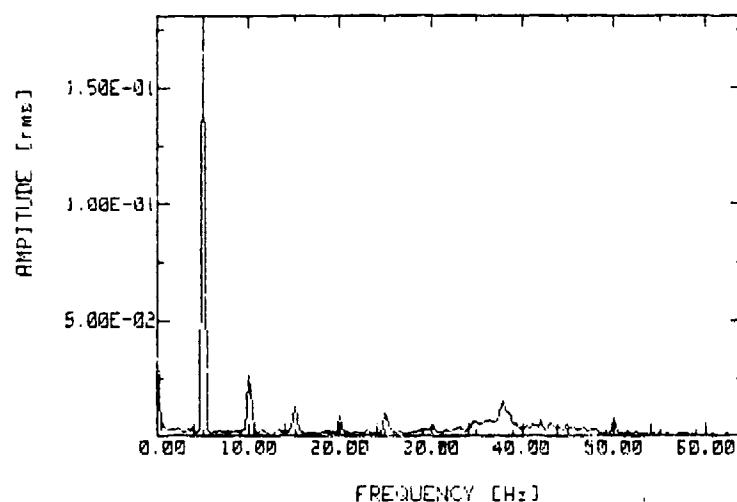


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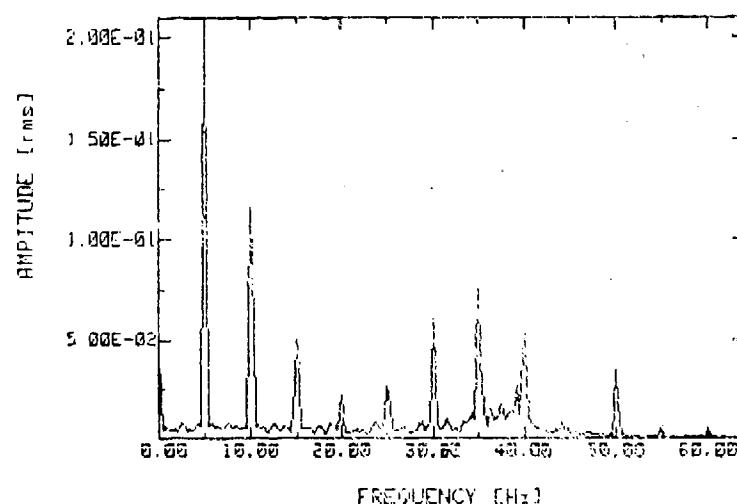
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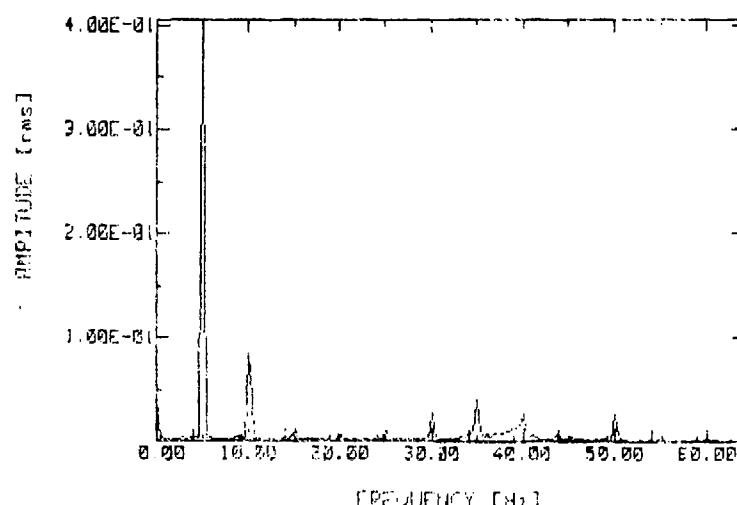
A SPEC 2 DELT_722B #PV: 10



A SPEC 2 DELT_722B #PV: 10

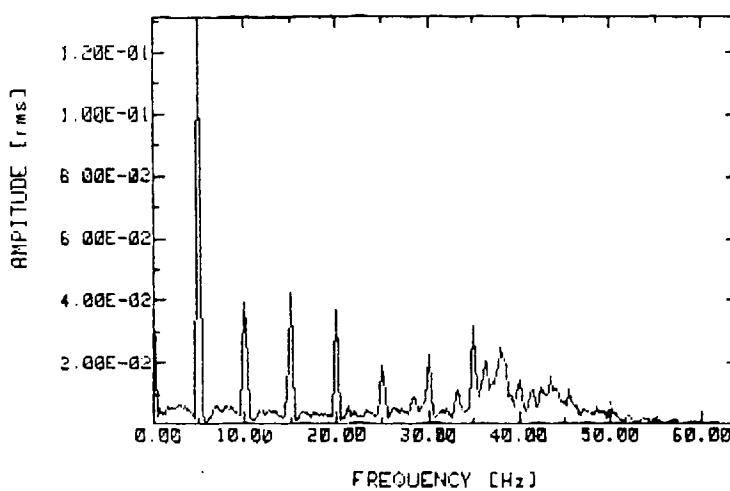


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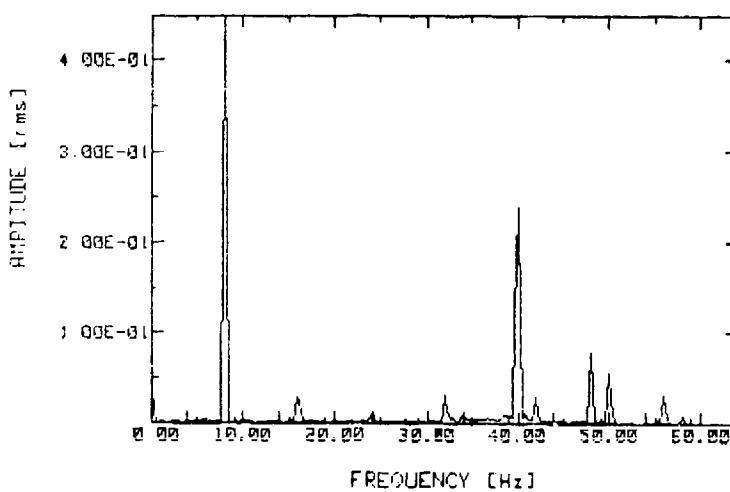
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#AV: 10



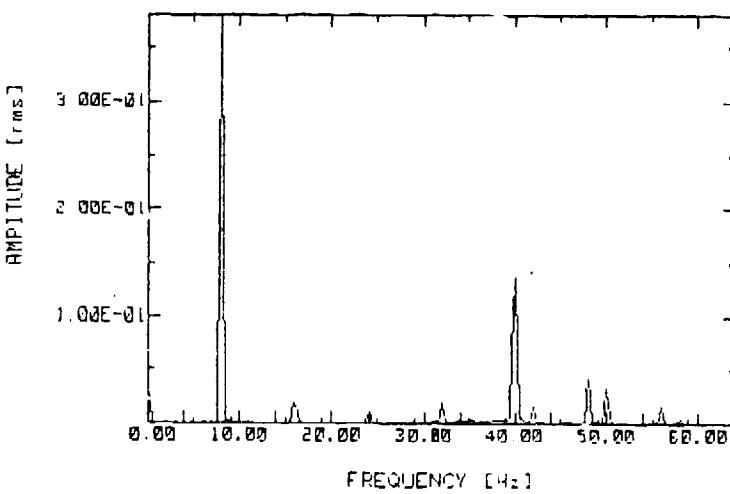
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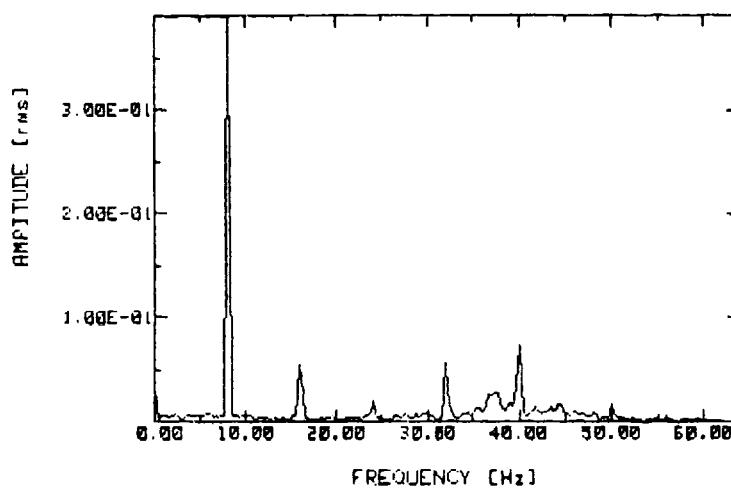


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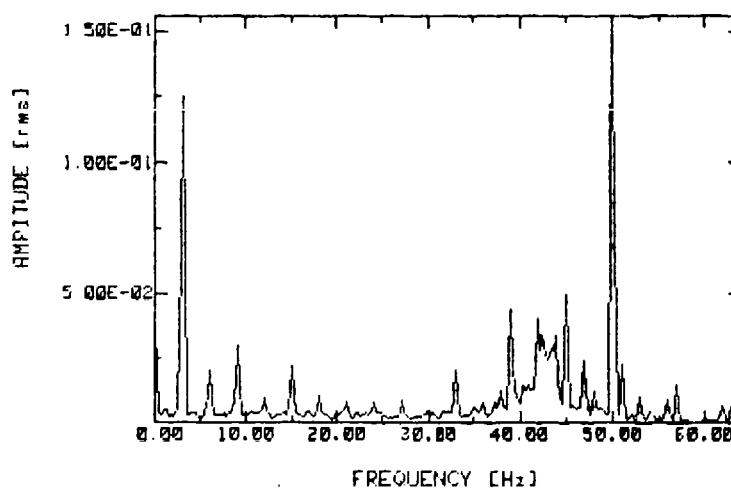
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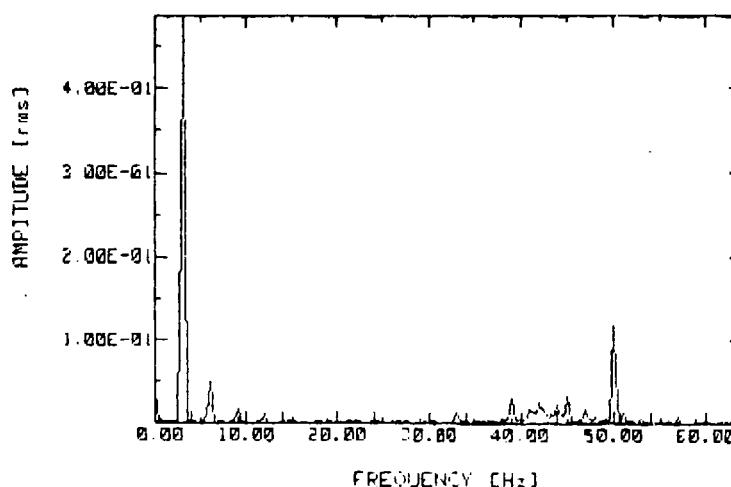
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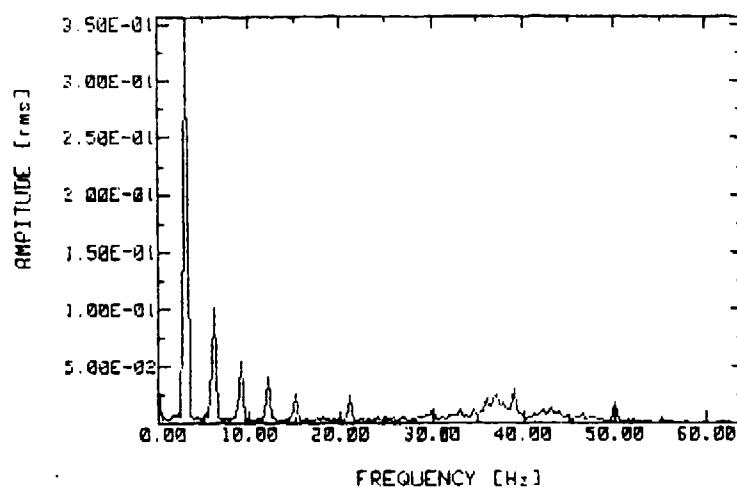
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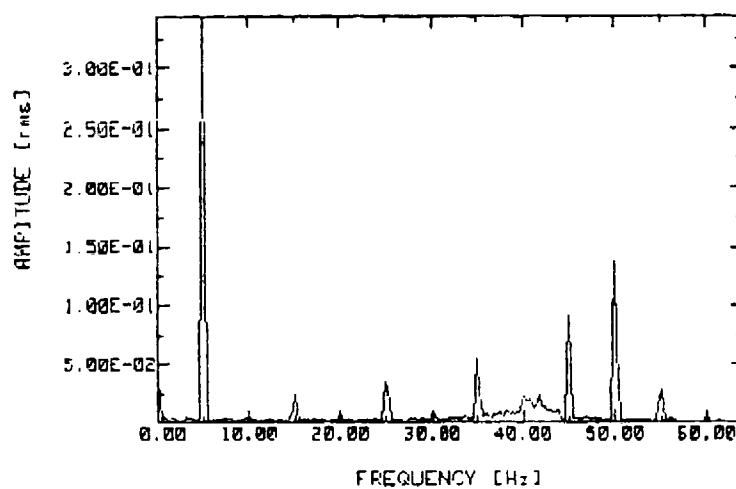
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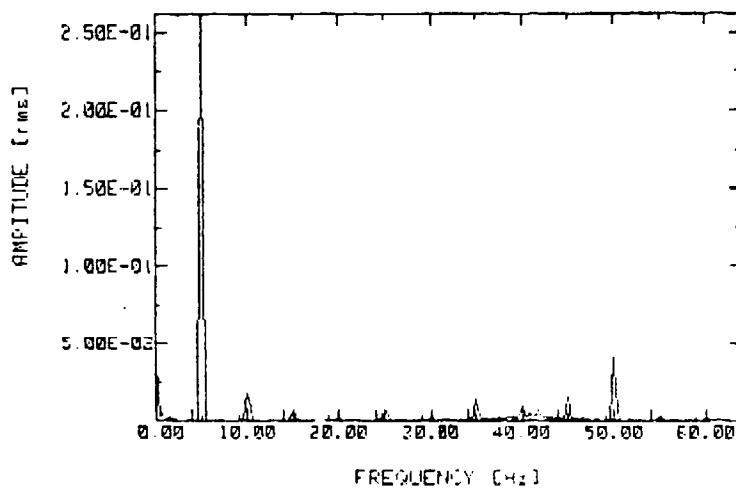
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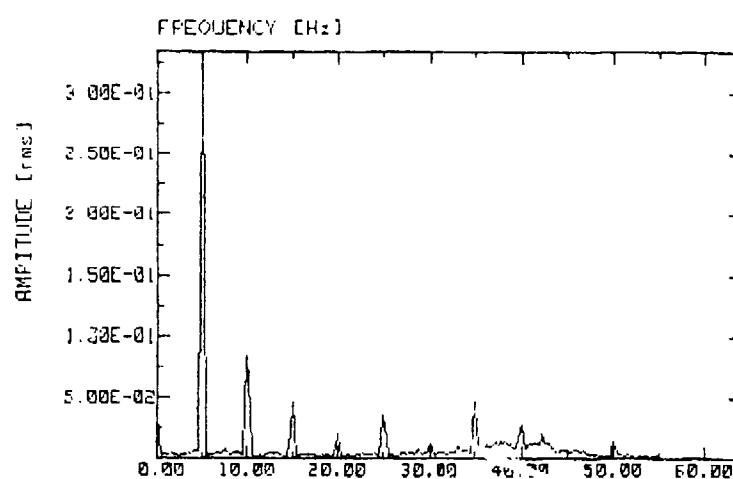


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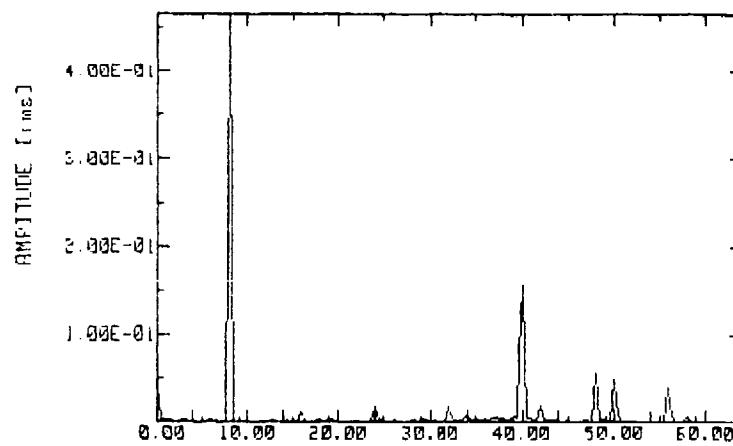


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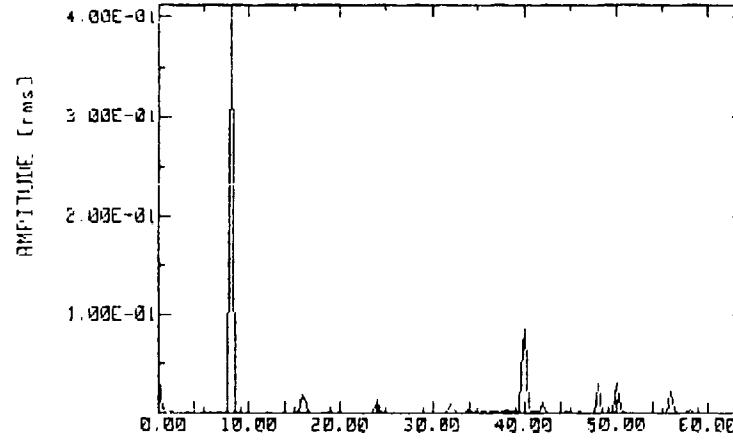




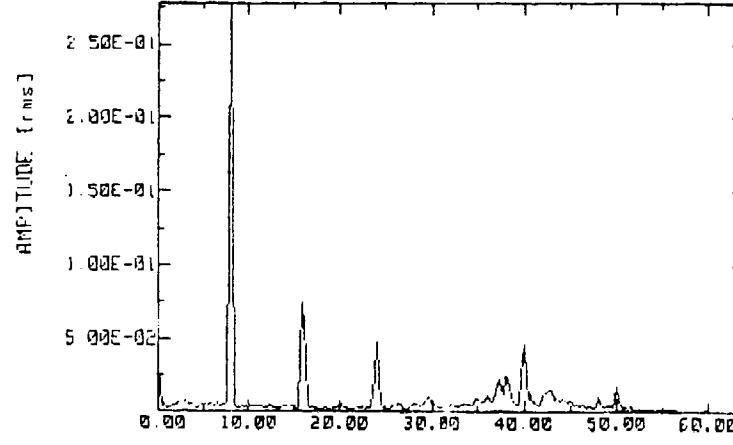
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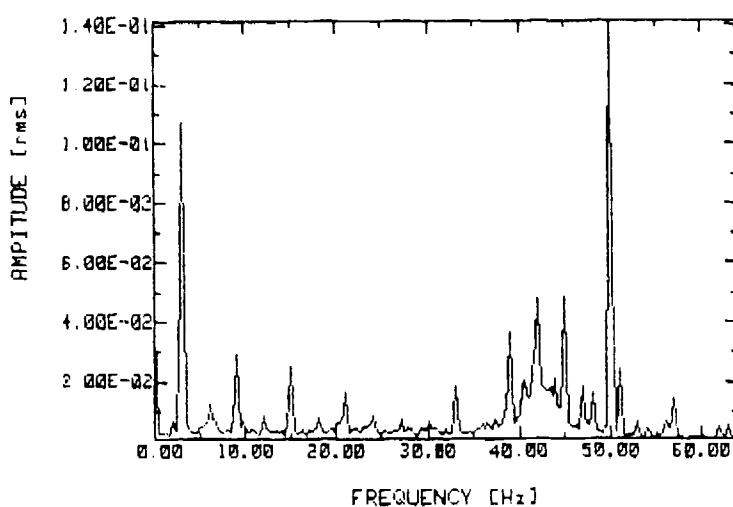
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R SPEC 2 DELT_7270 #AV: 10

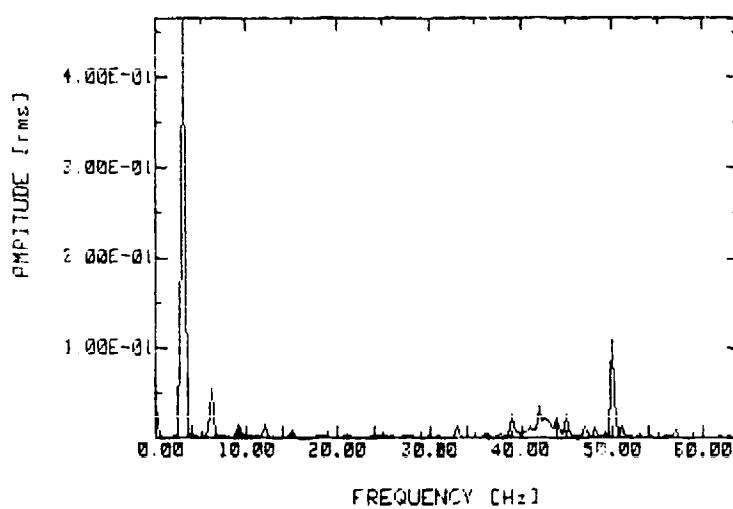
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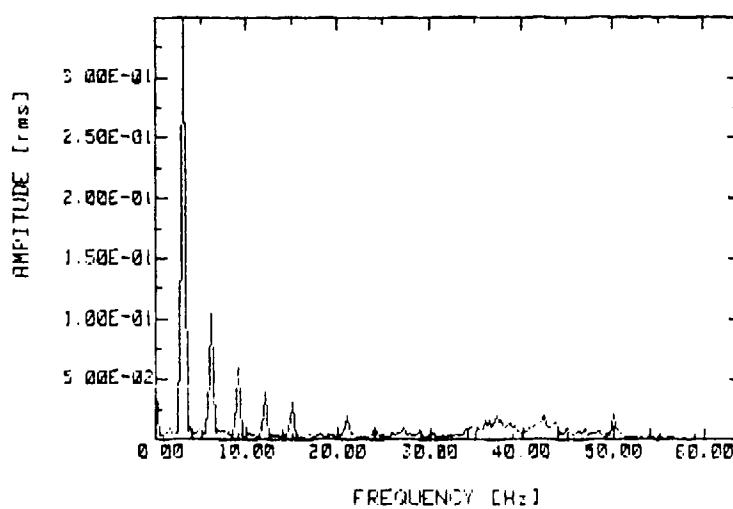
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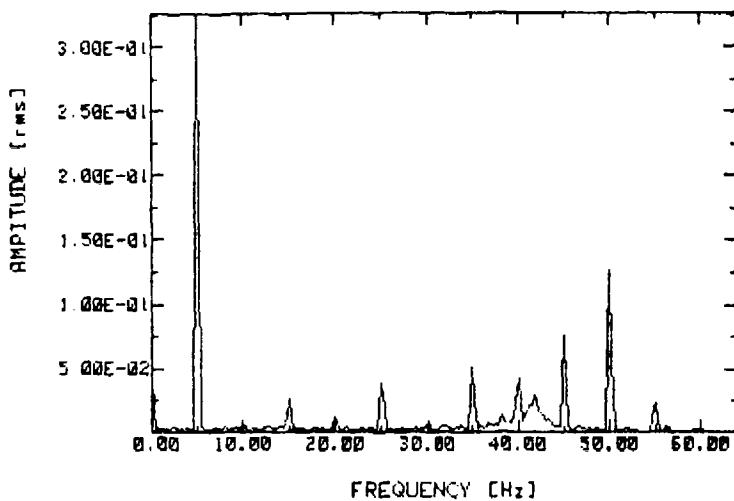
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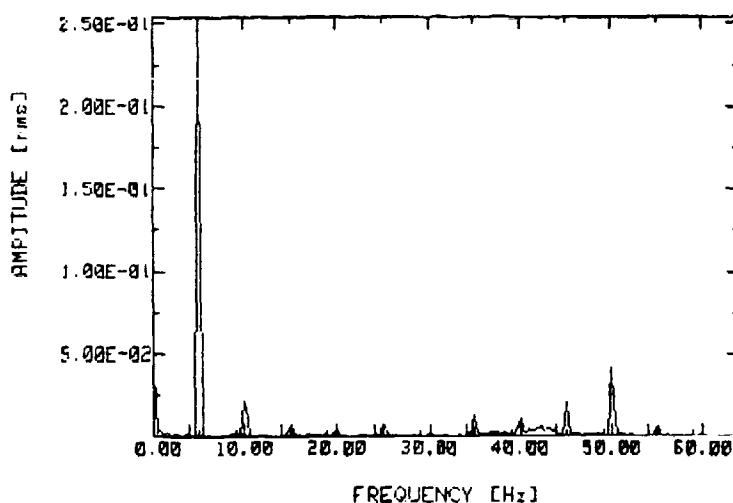
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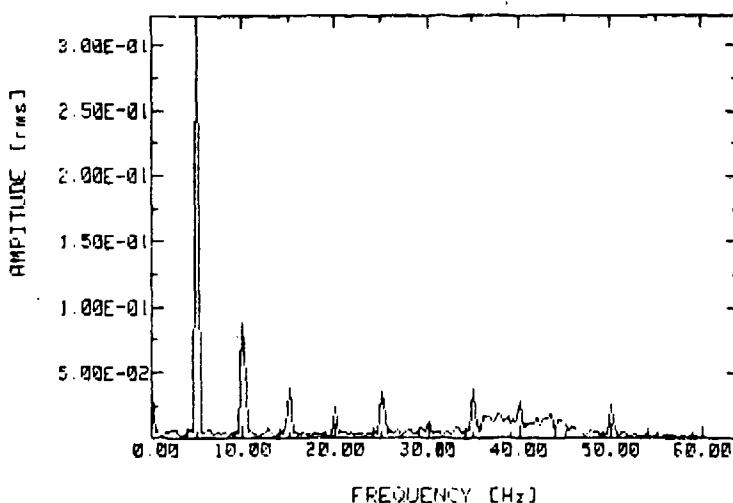
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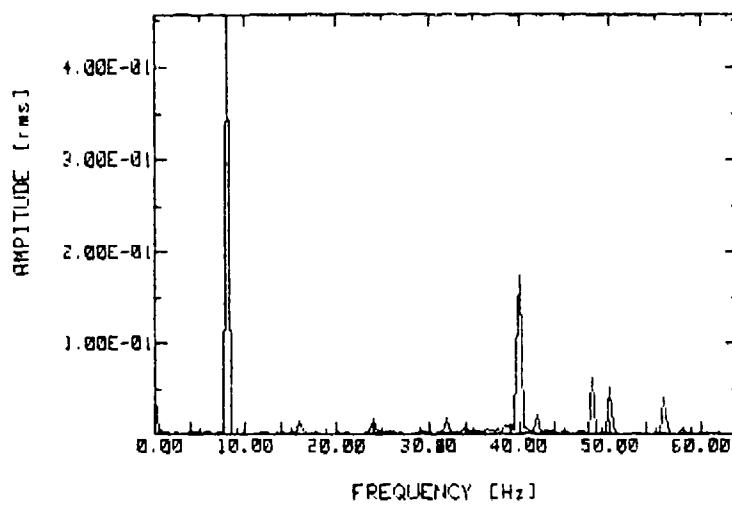


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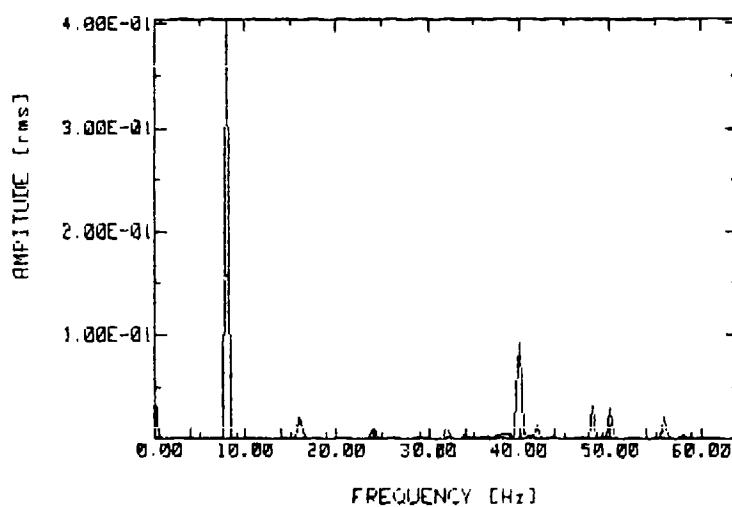
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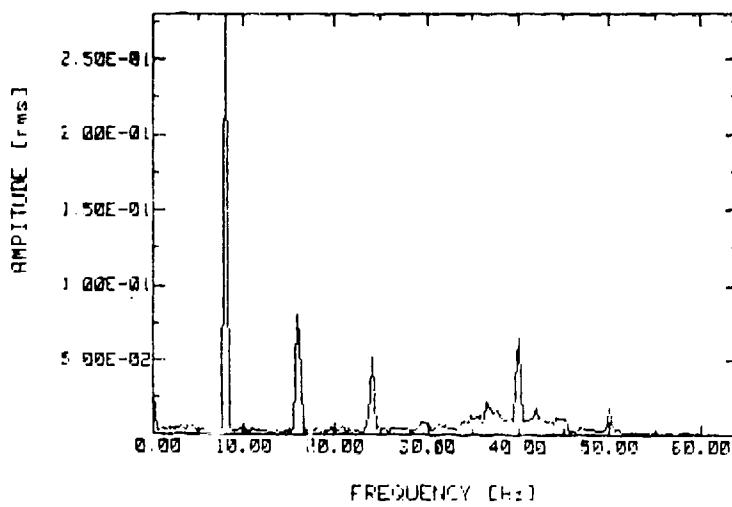
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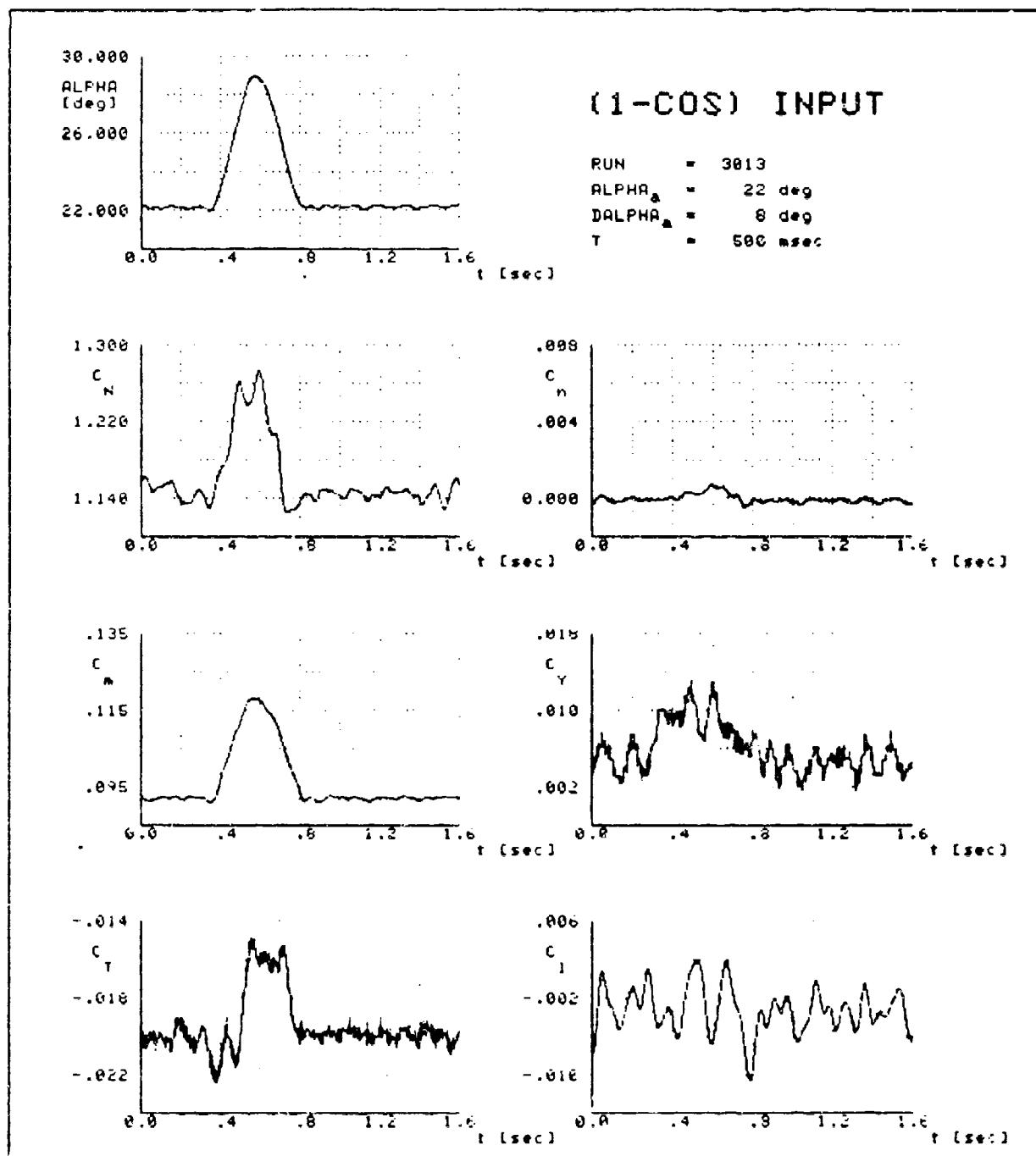


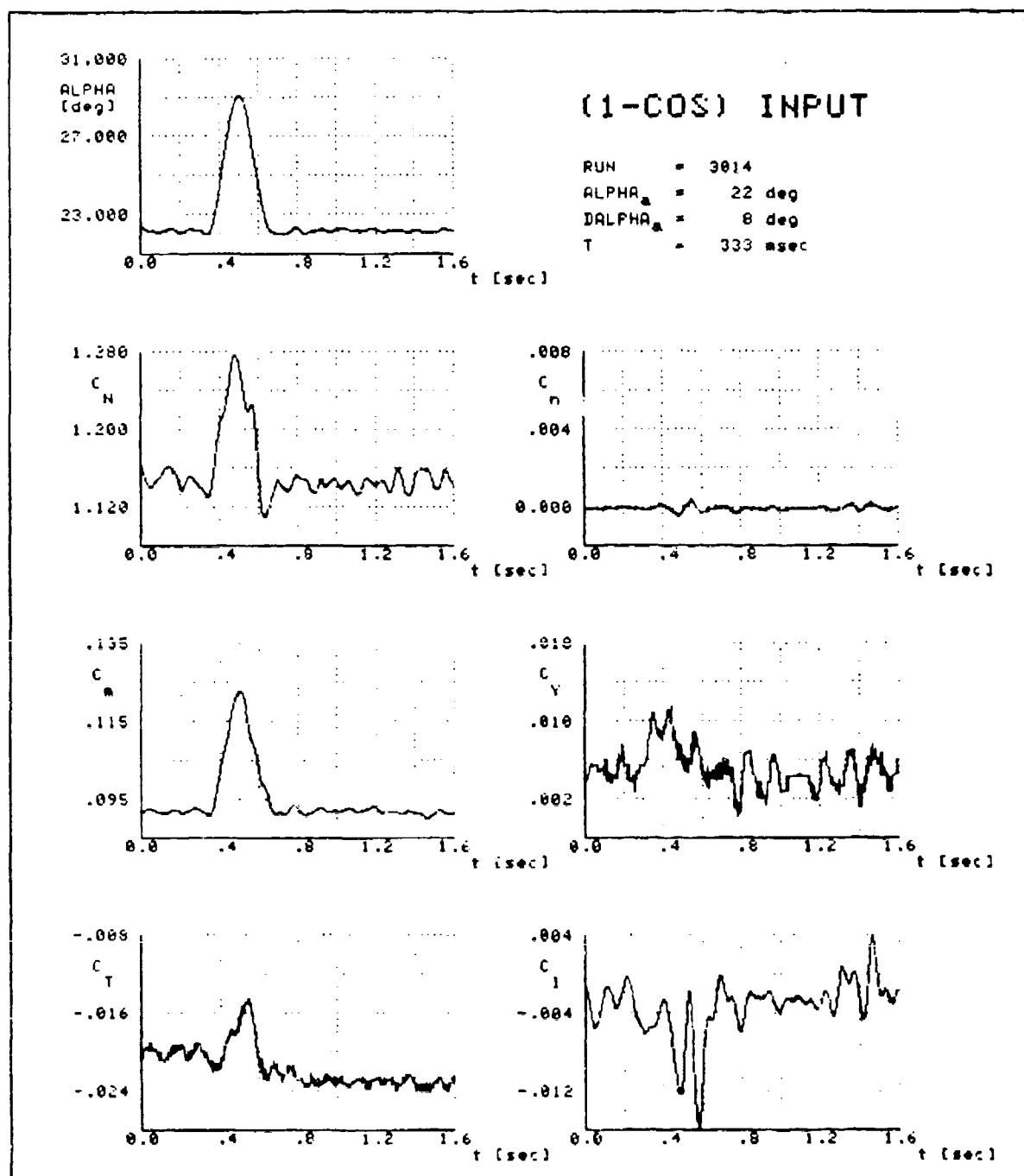
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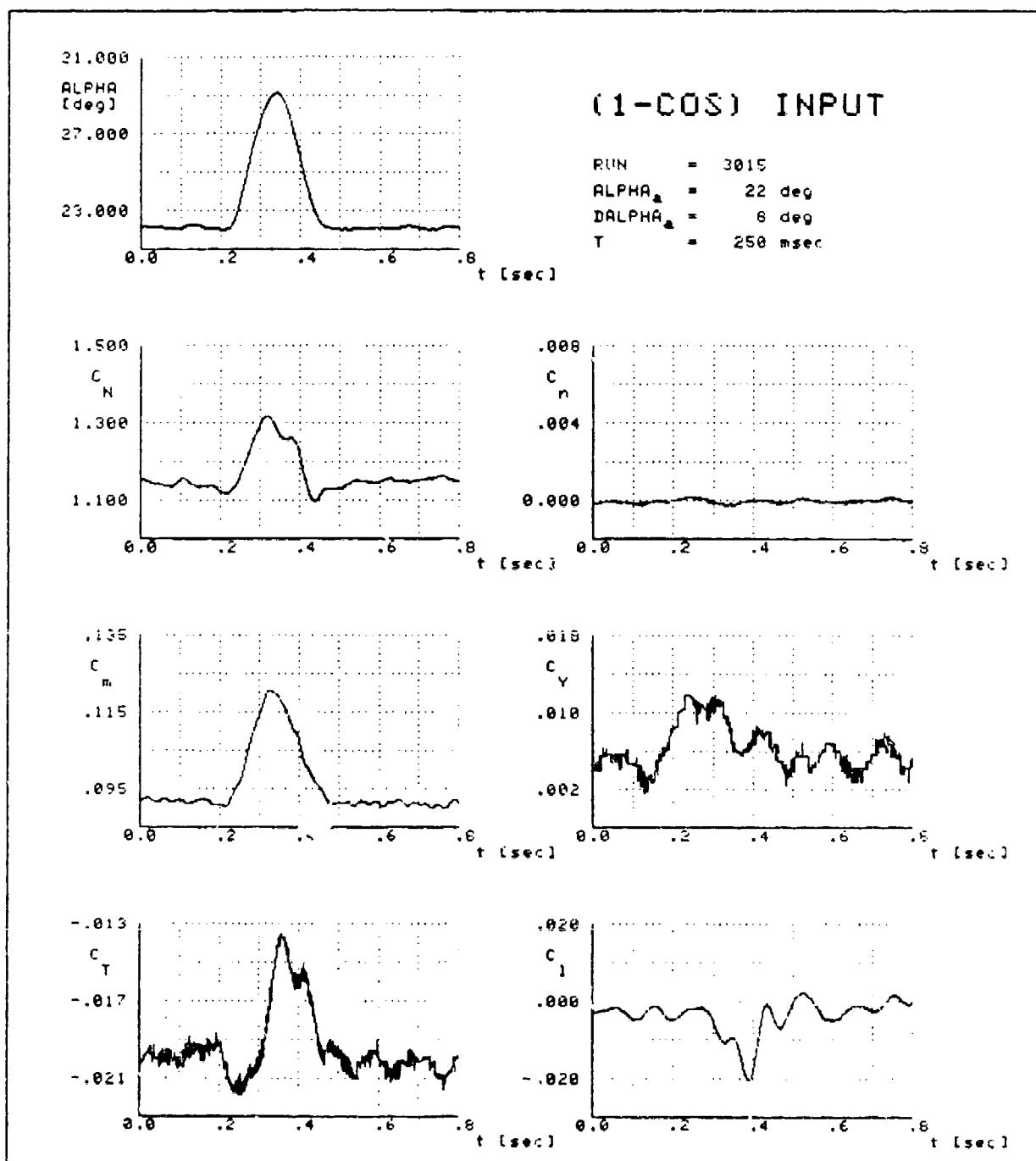


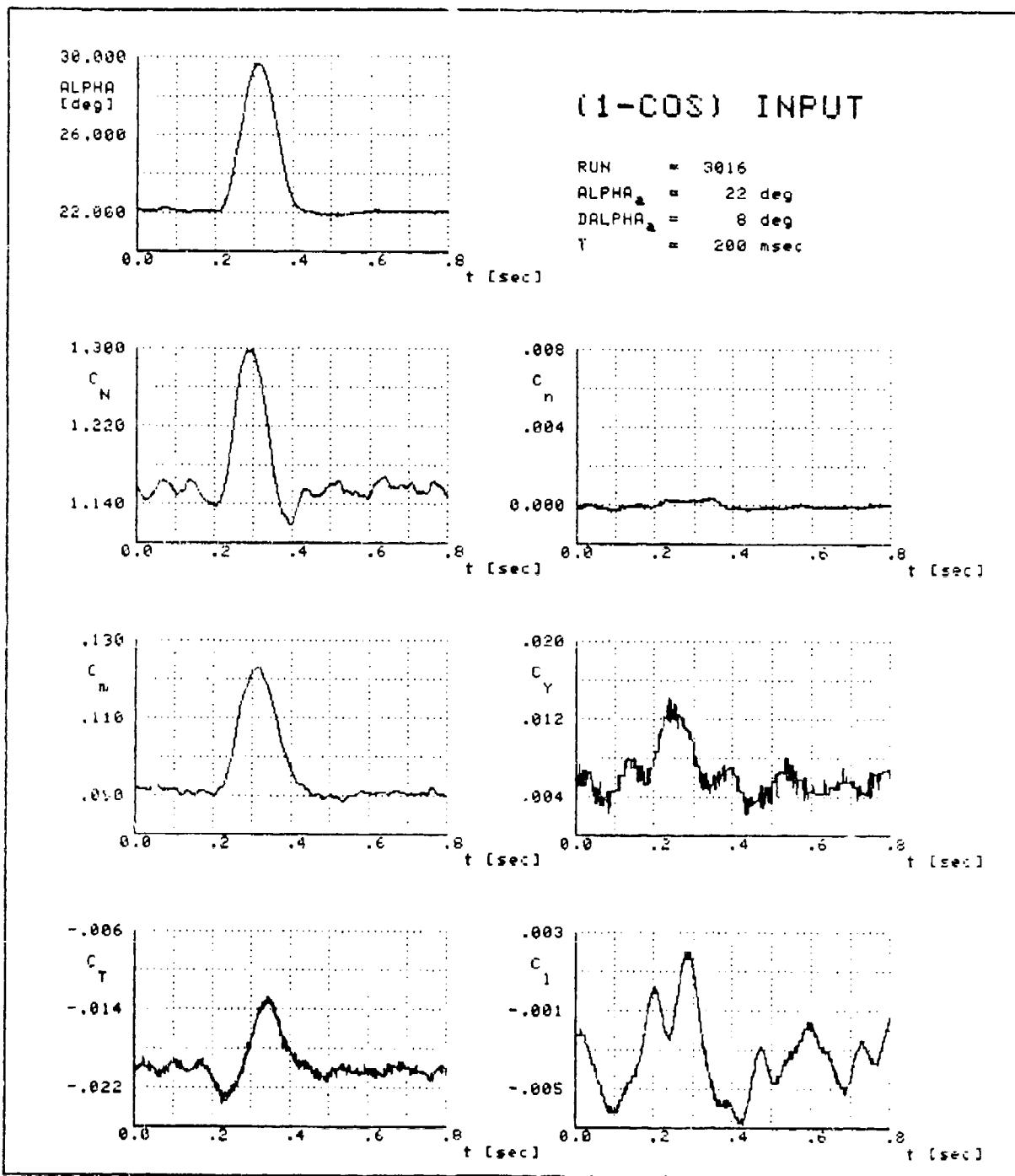
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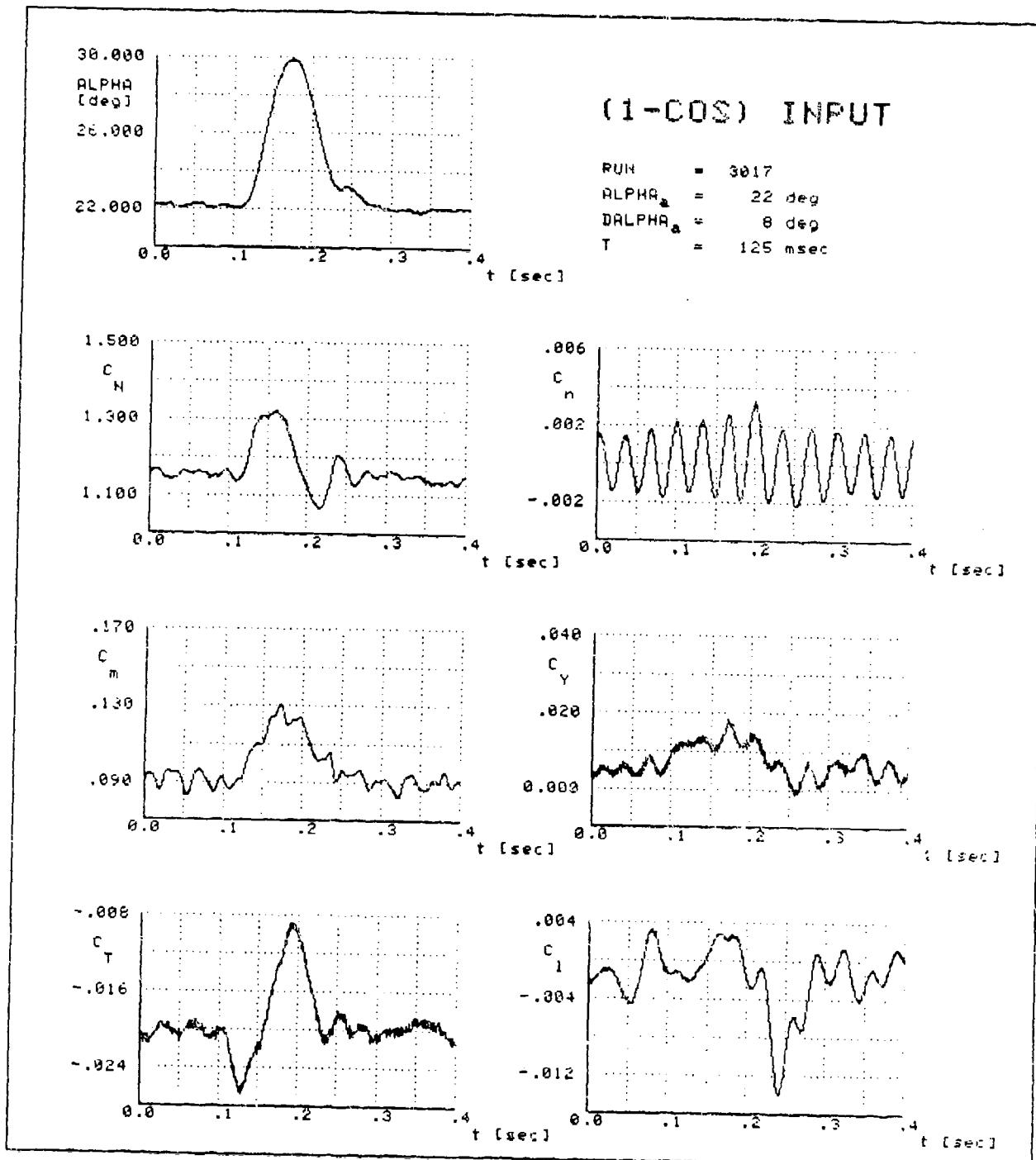
APPENDIX B
PLOTS OF TIME HISTORIES OF OVERALL LOADS FOR
(1-COS) INPUTS

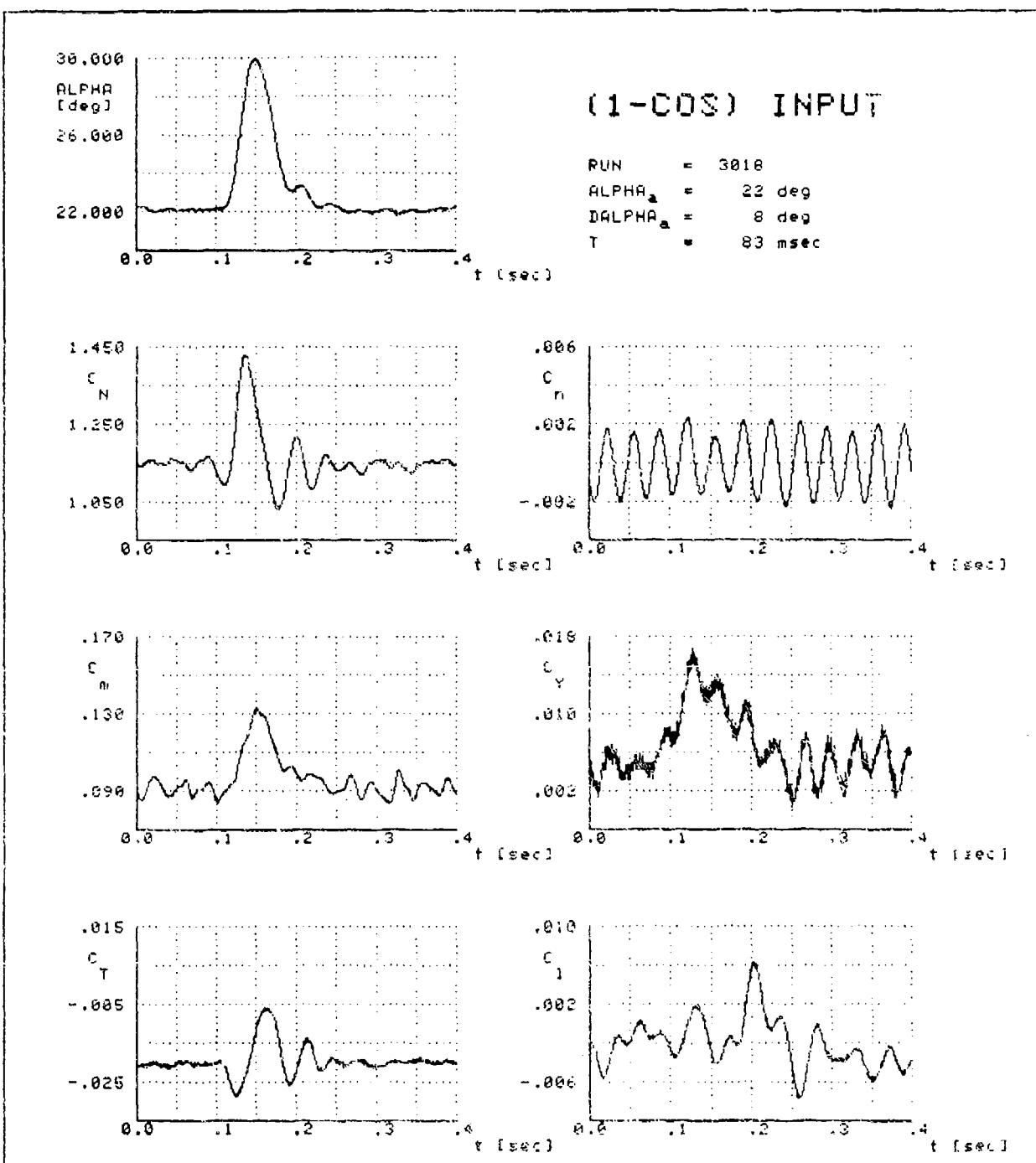


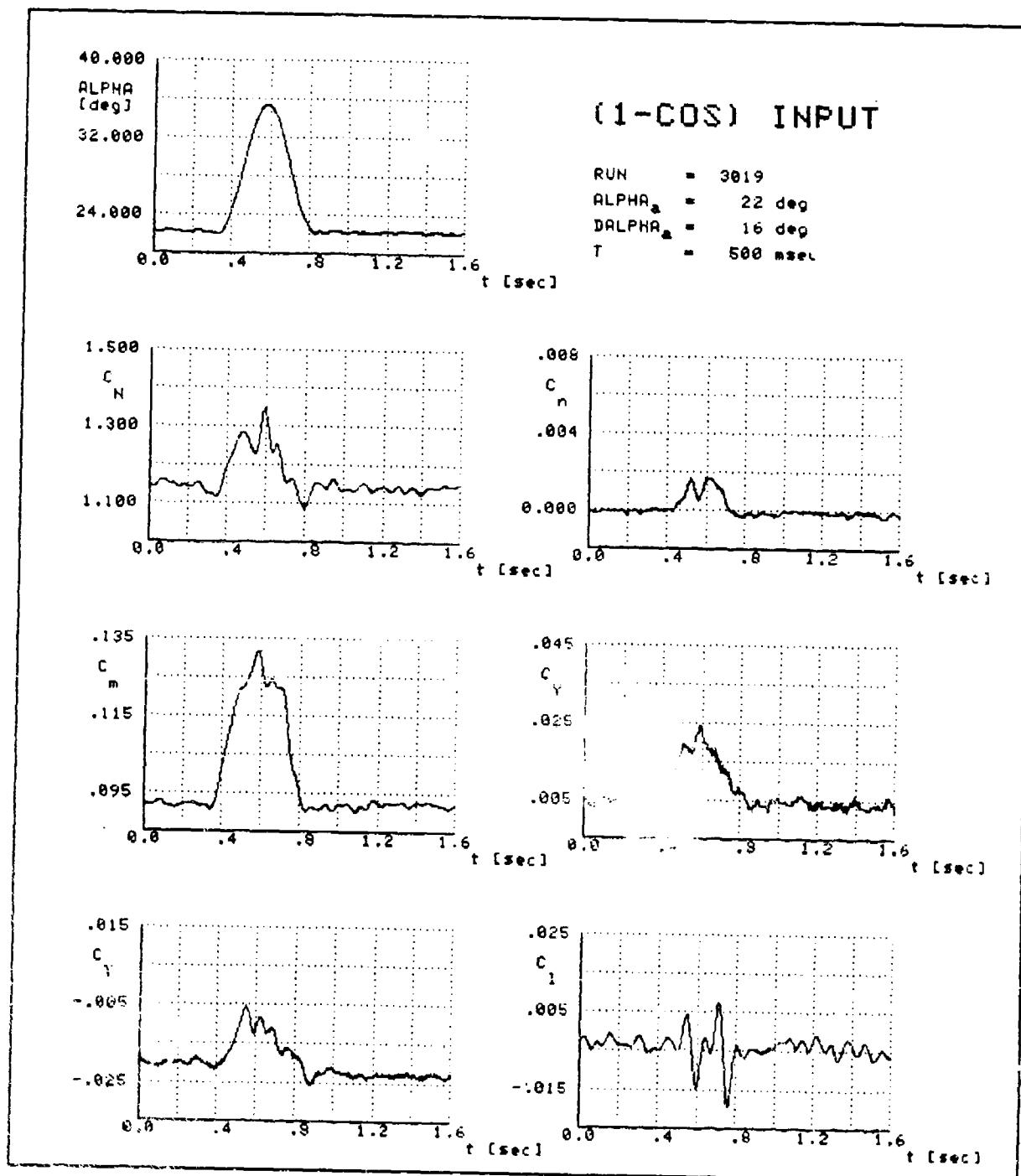


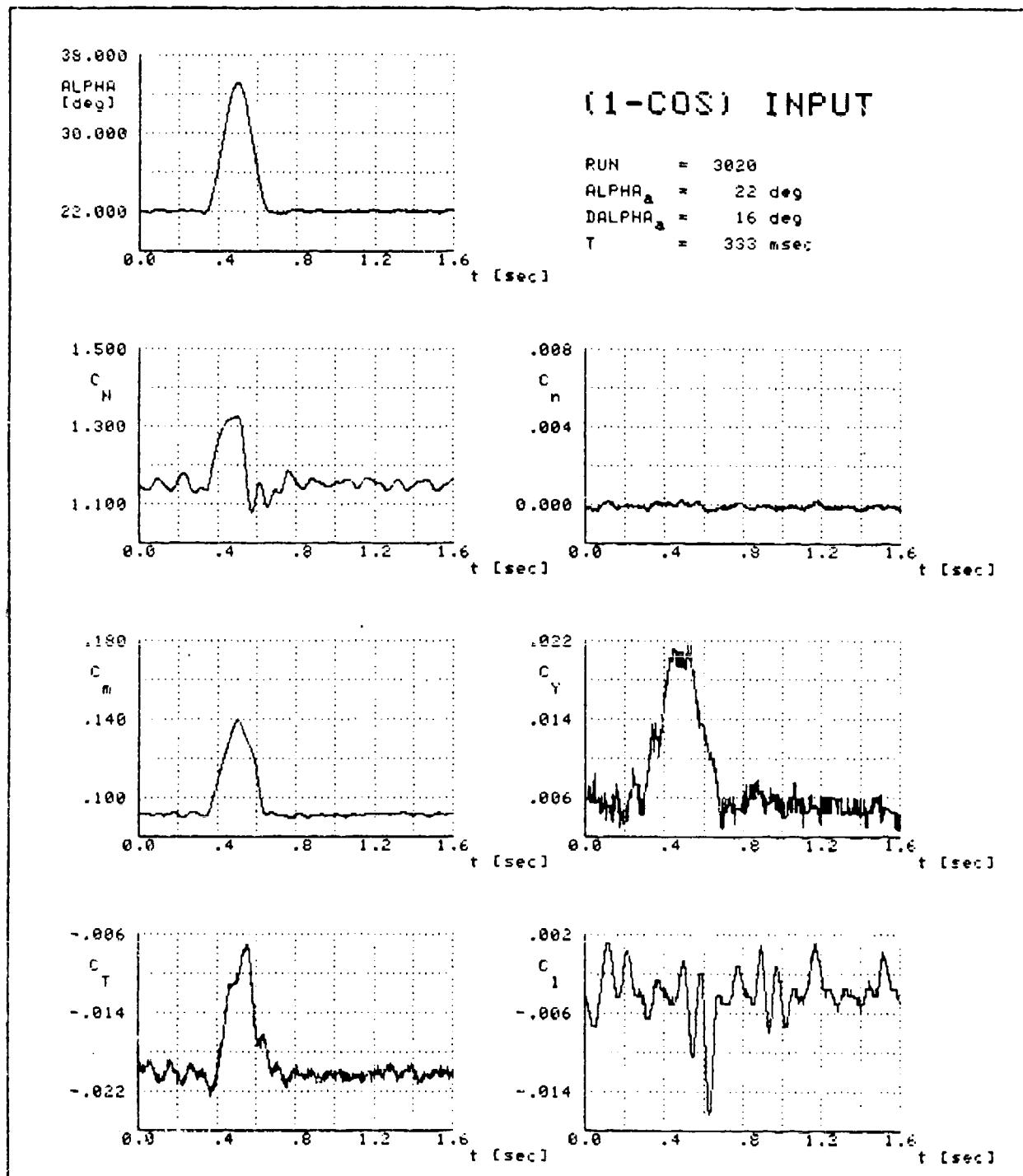


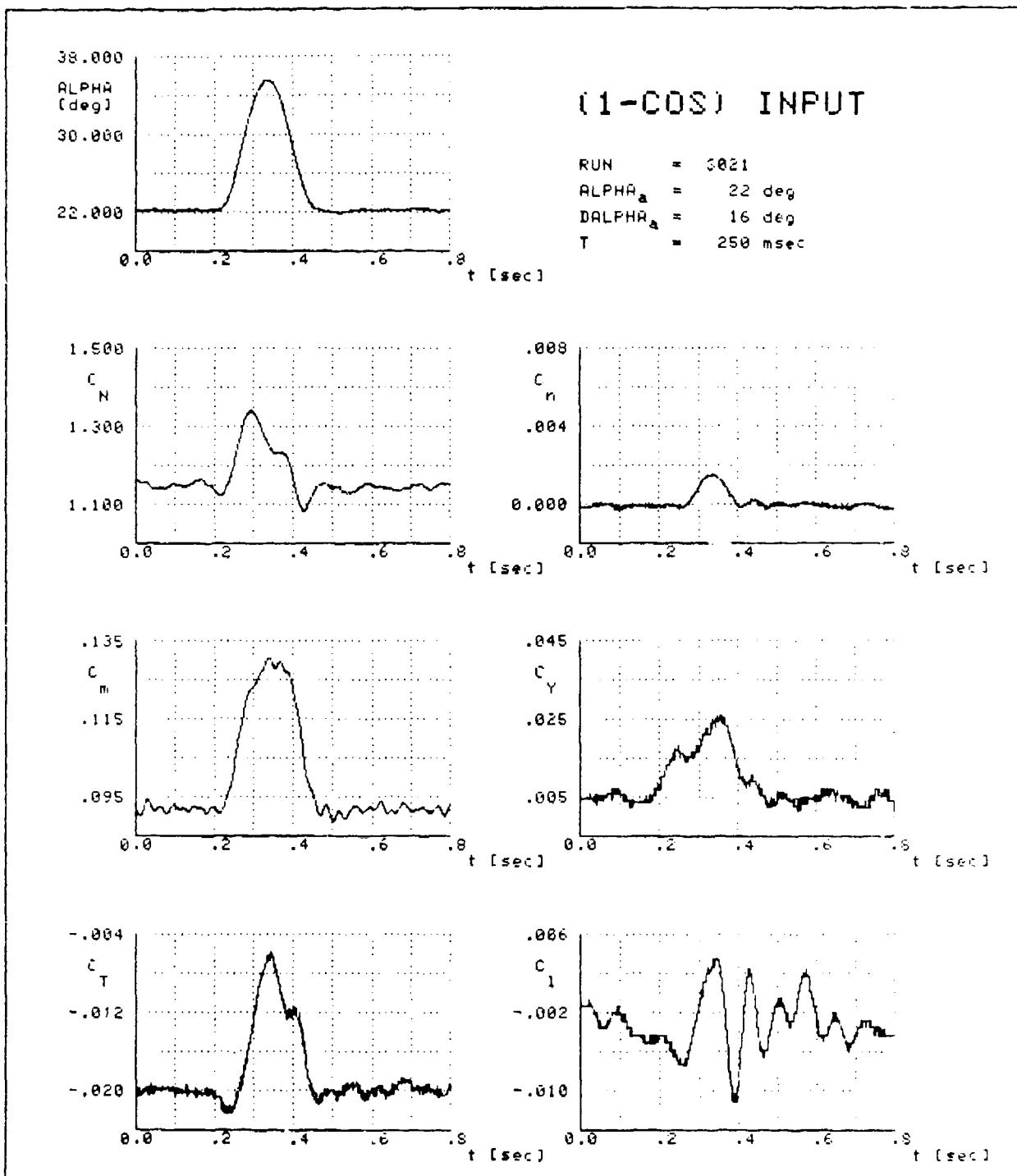


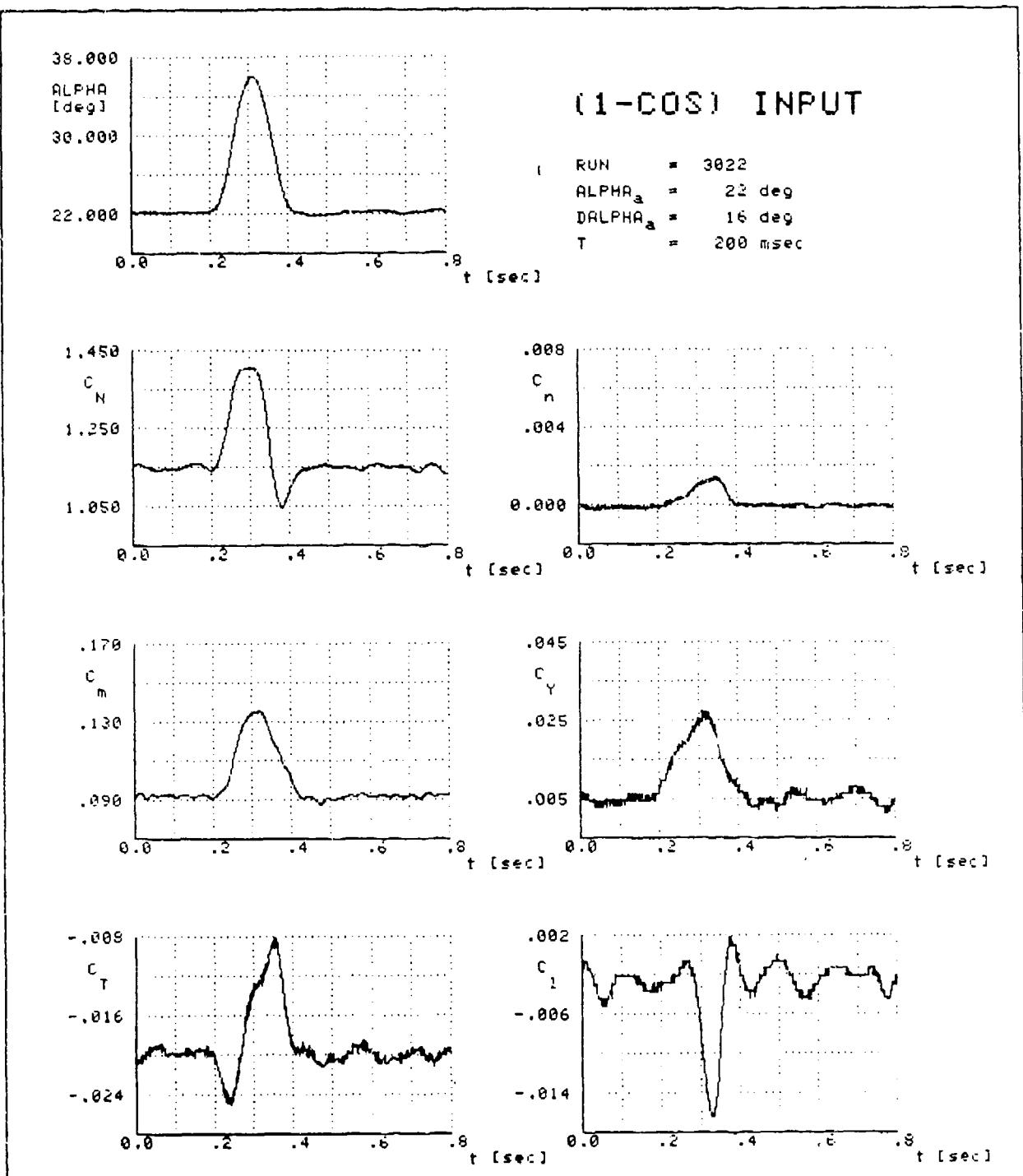


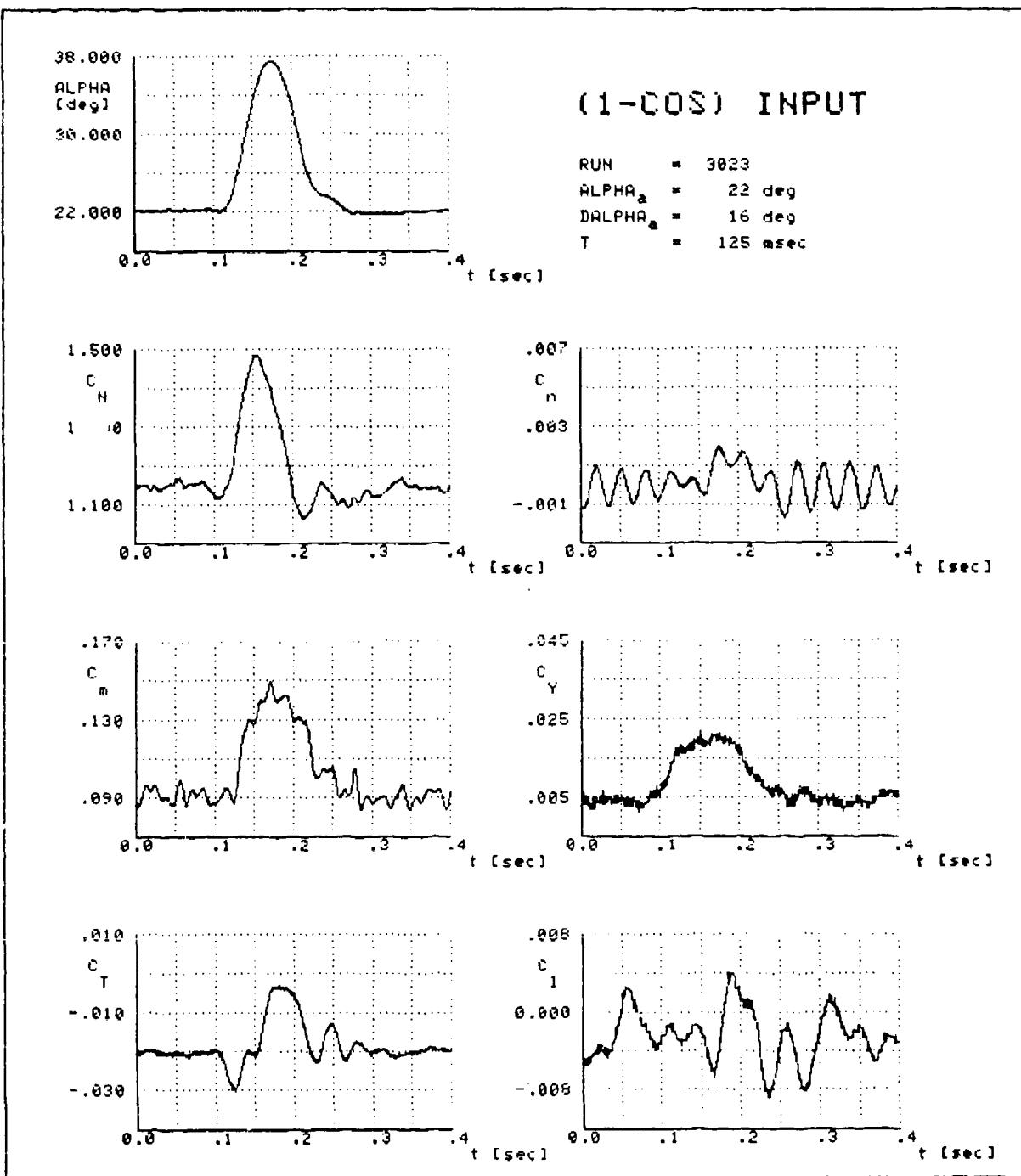


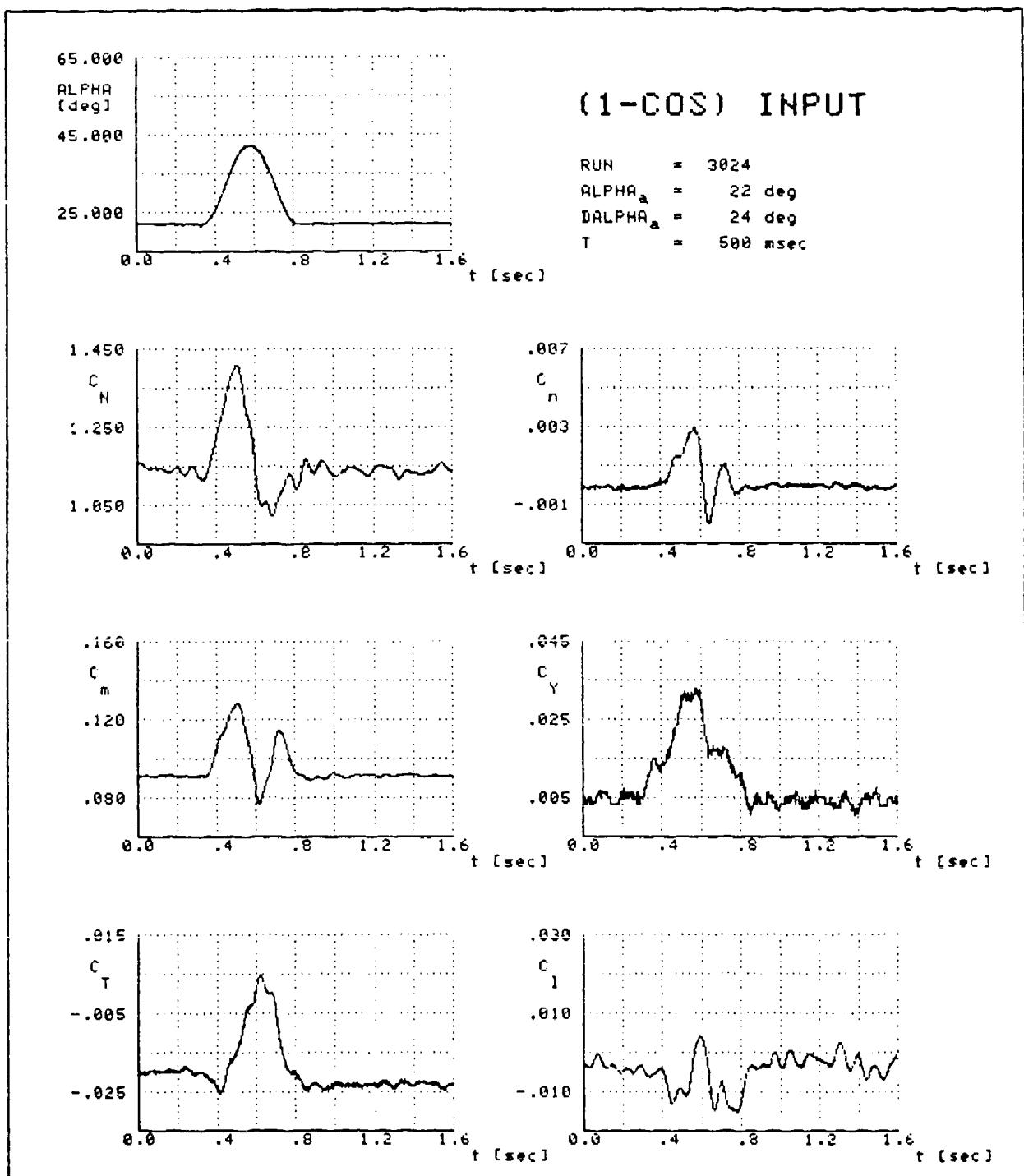


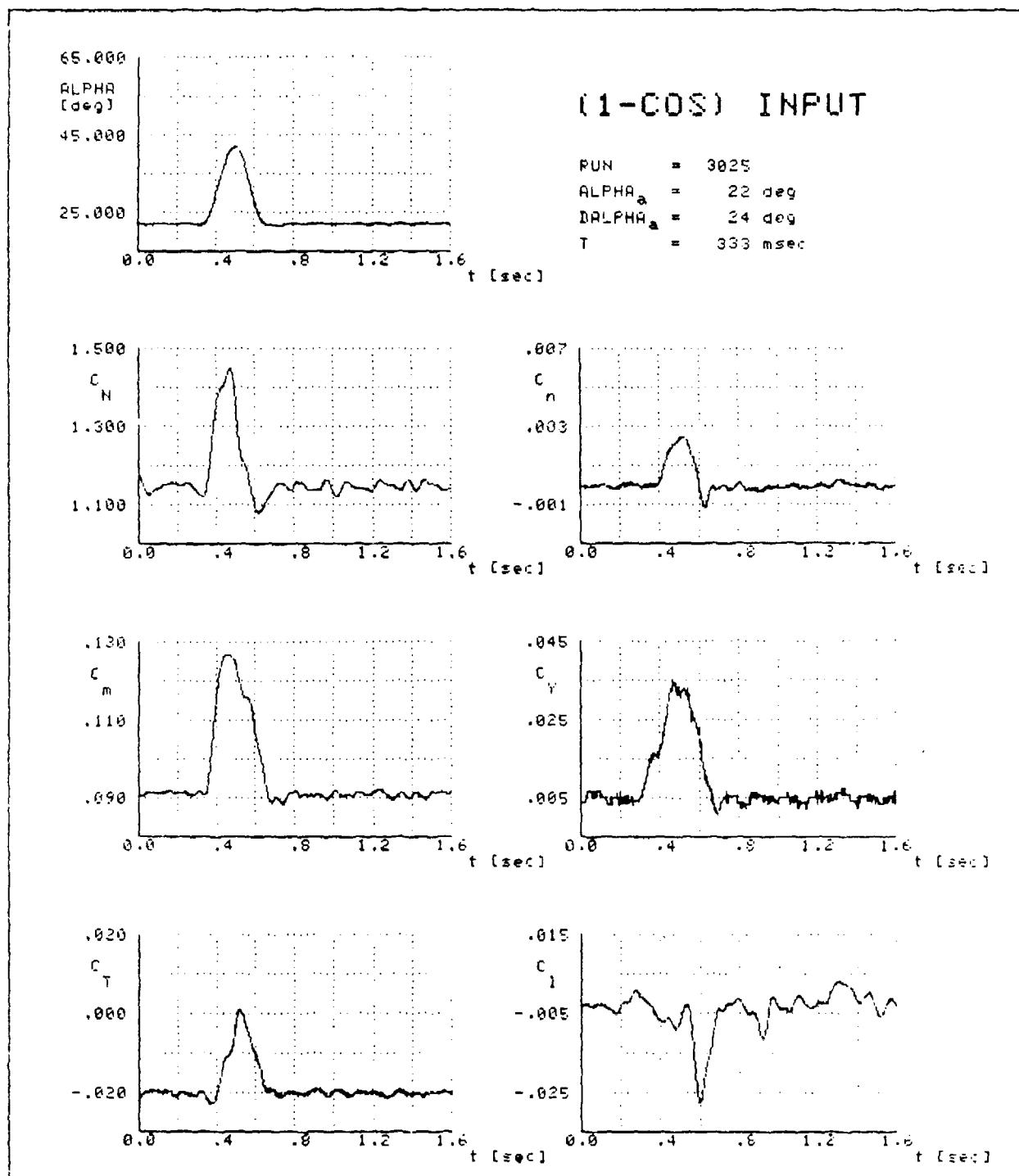


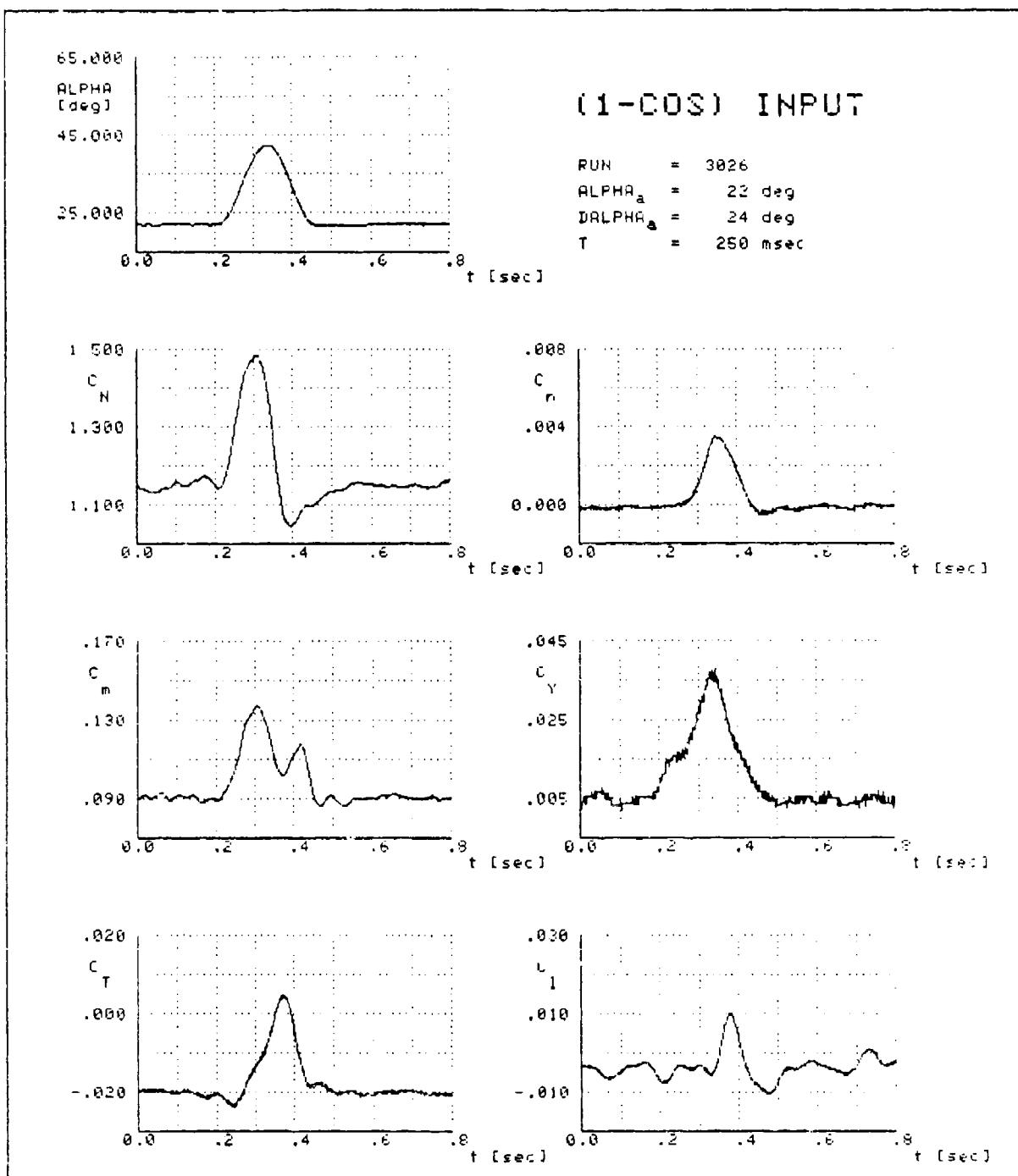


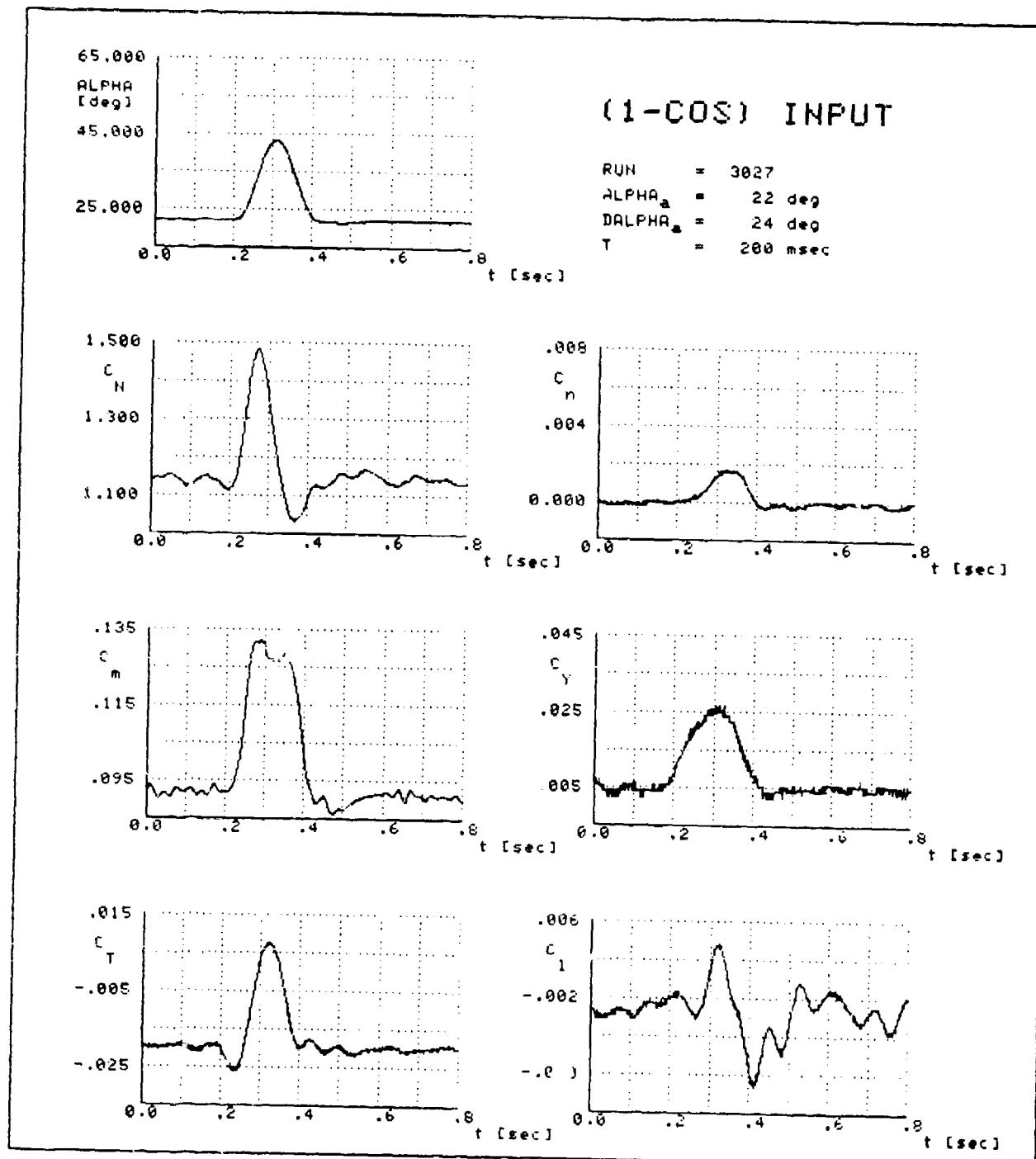


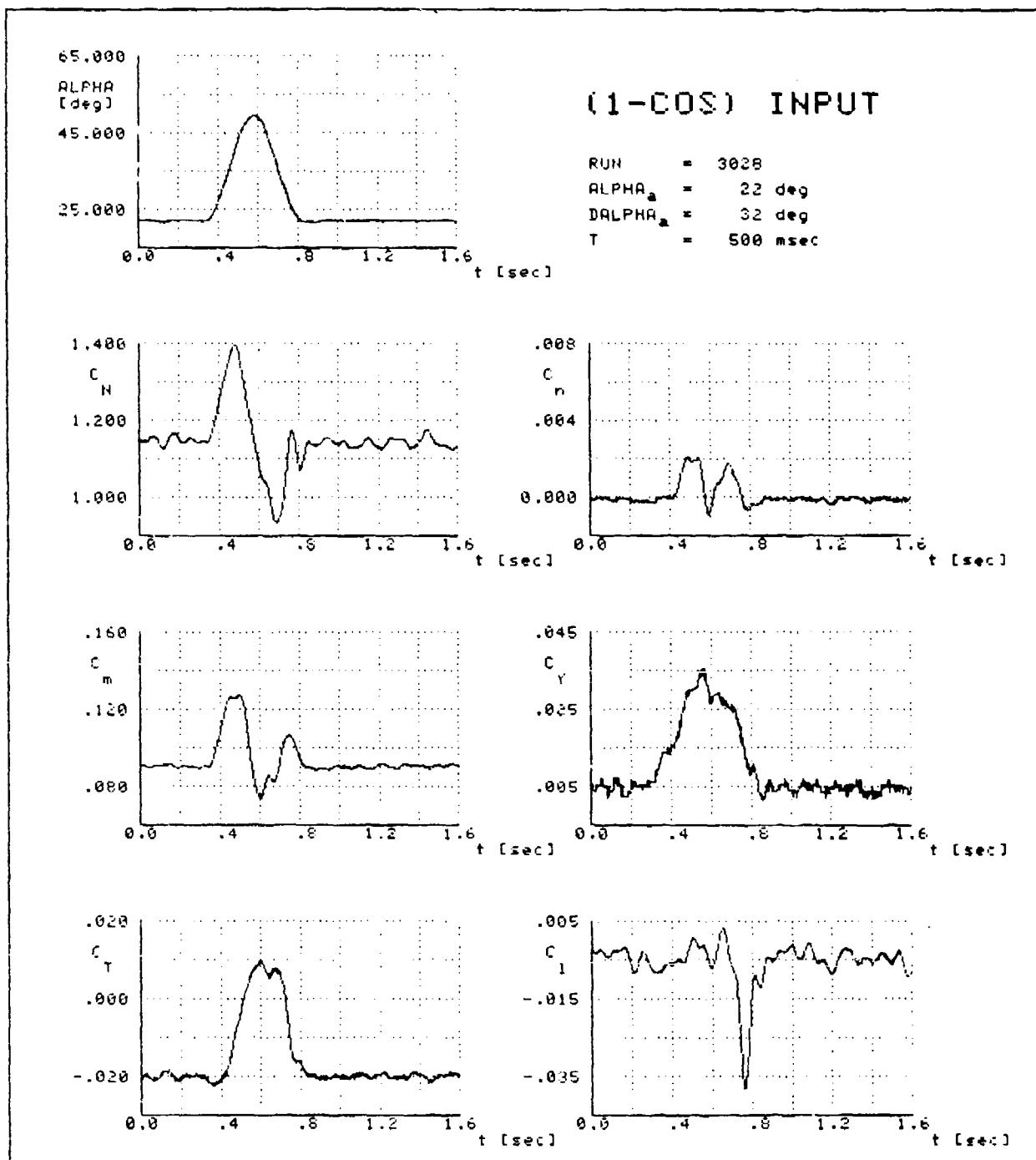


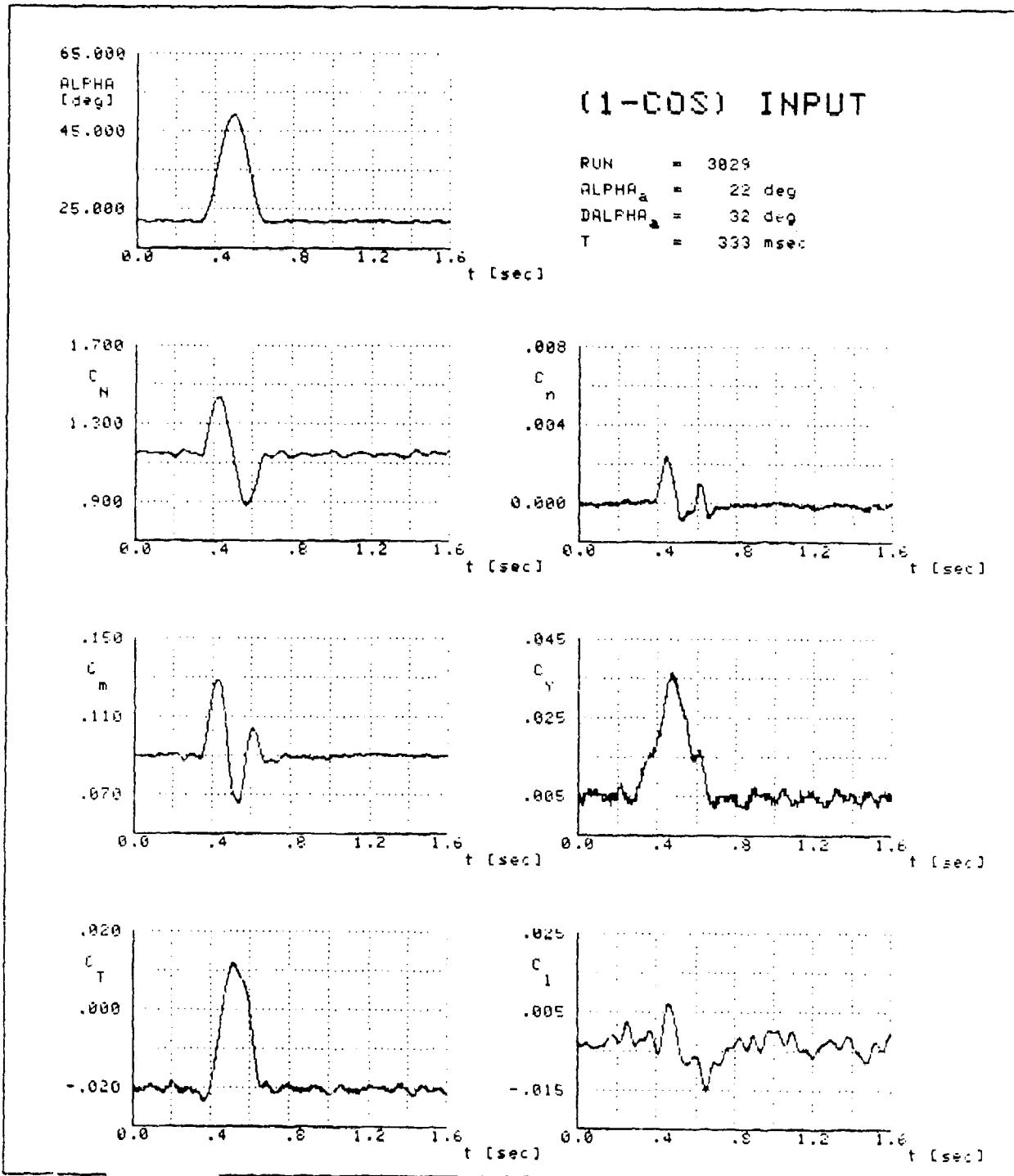


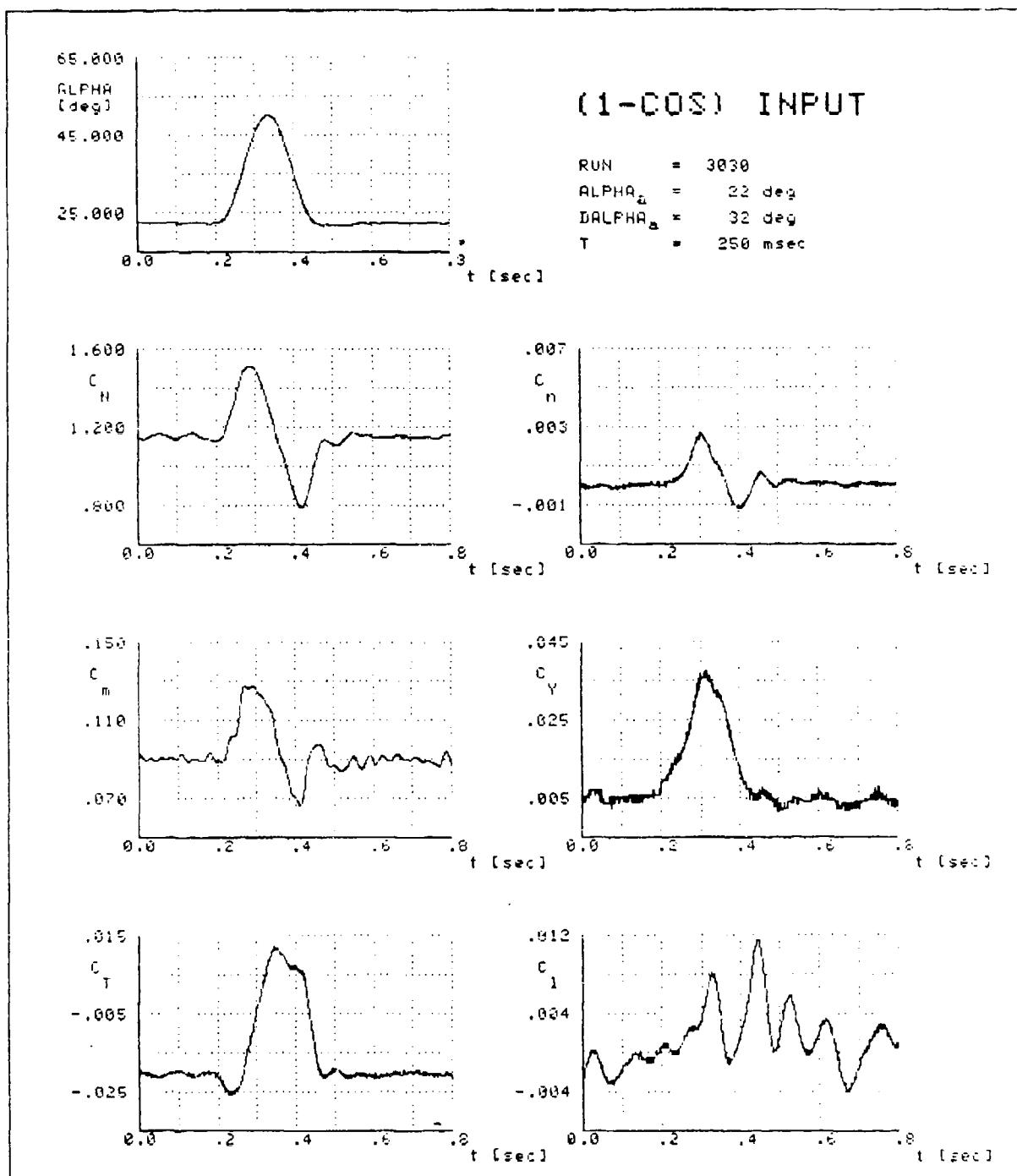


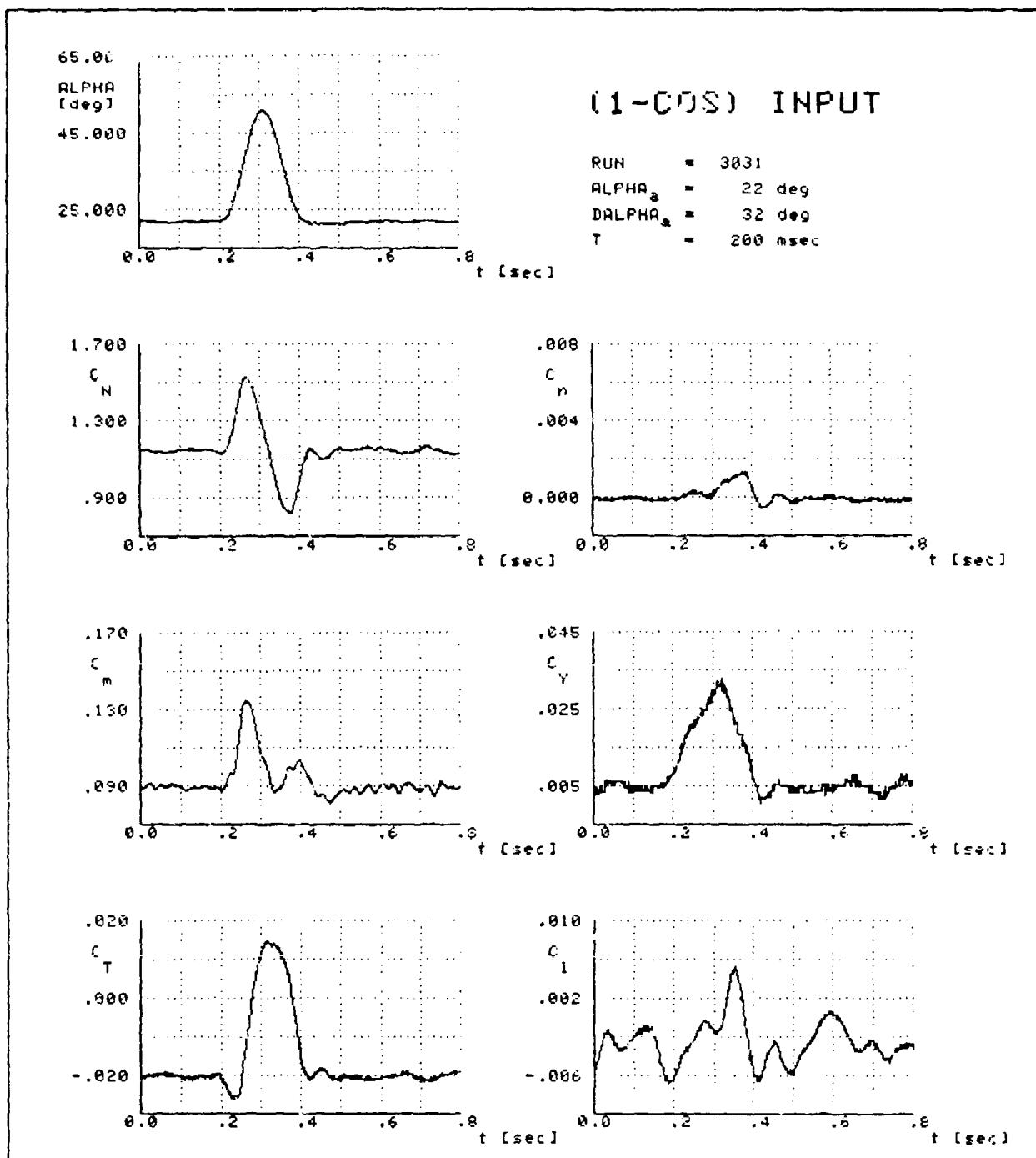












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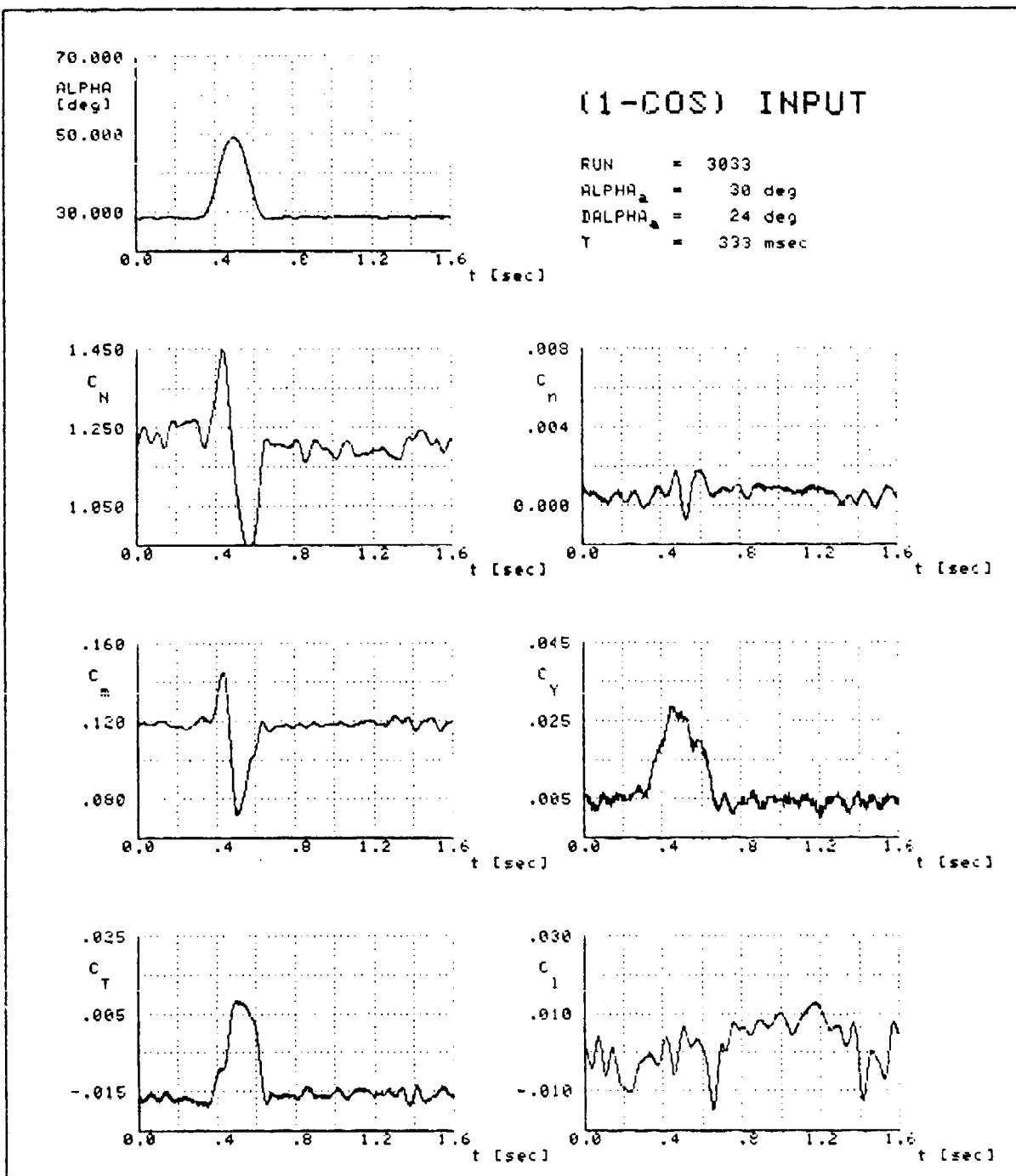
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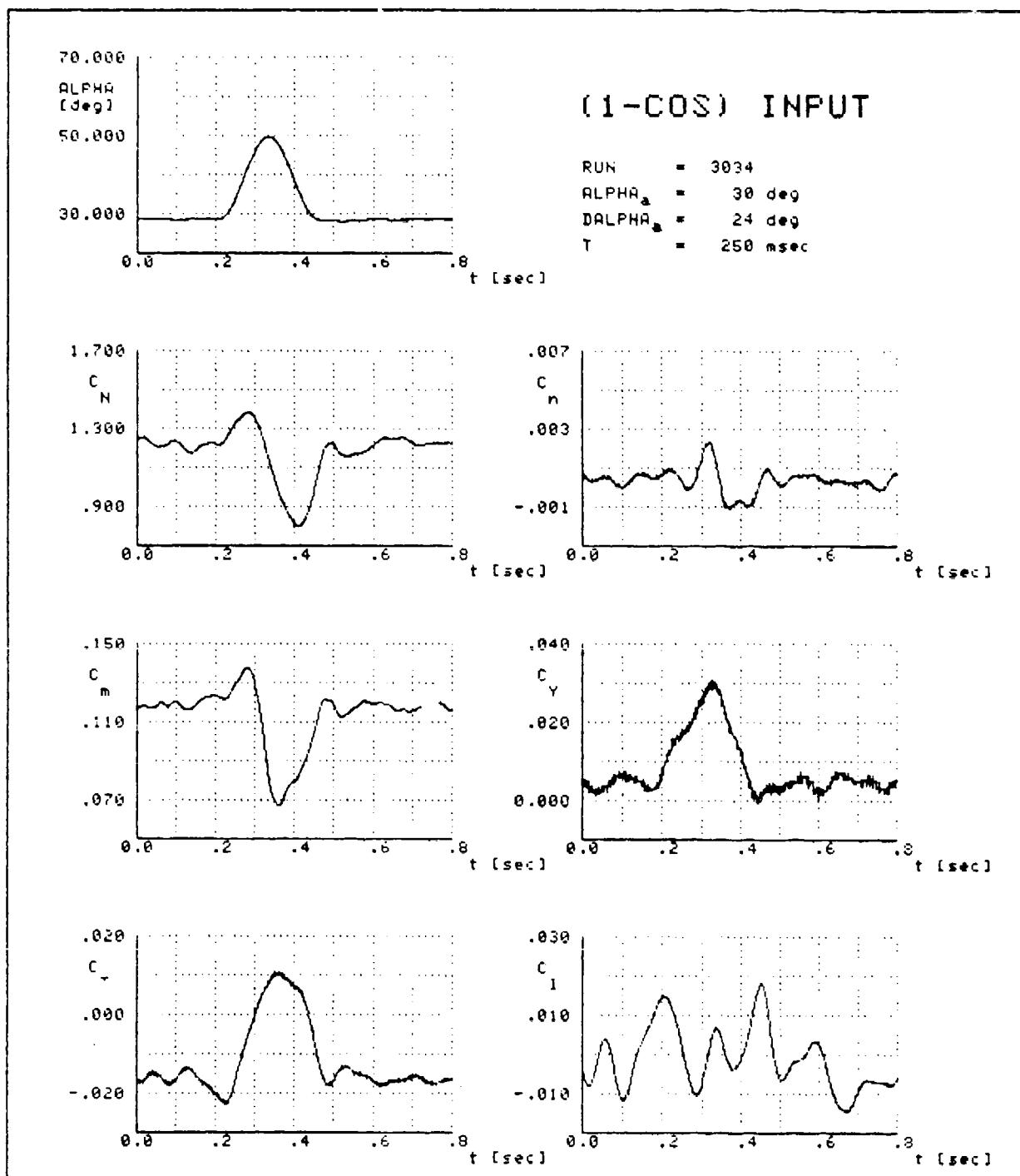
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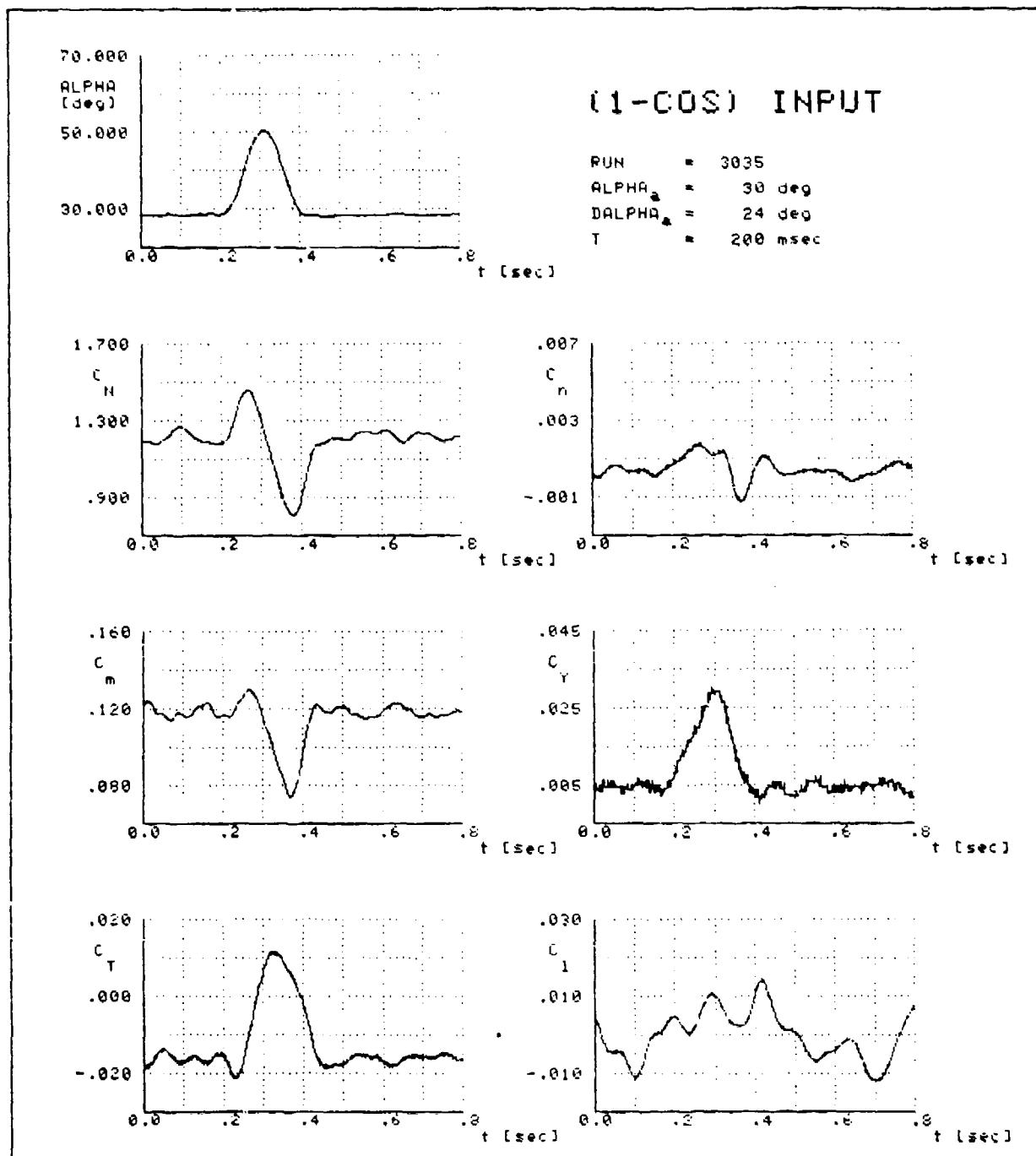
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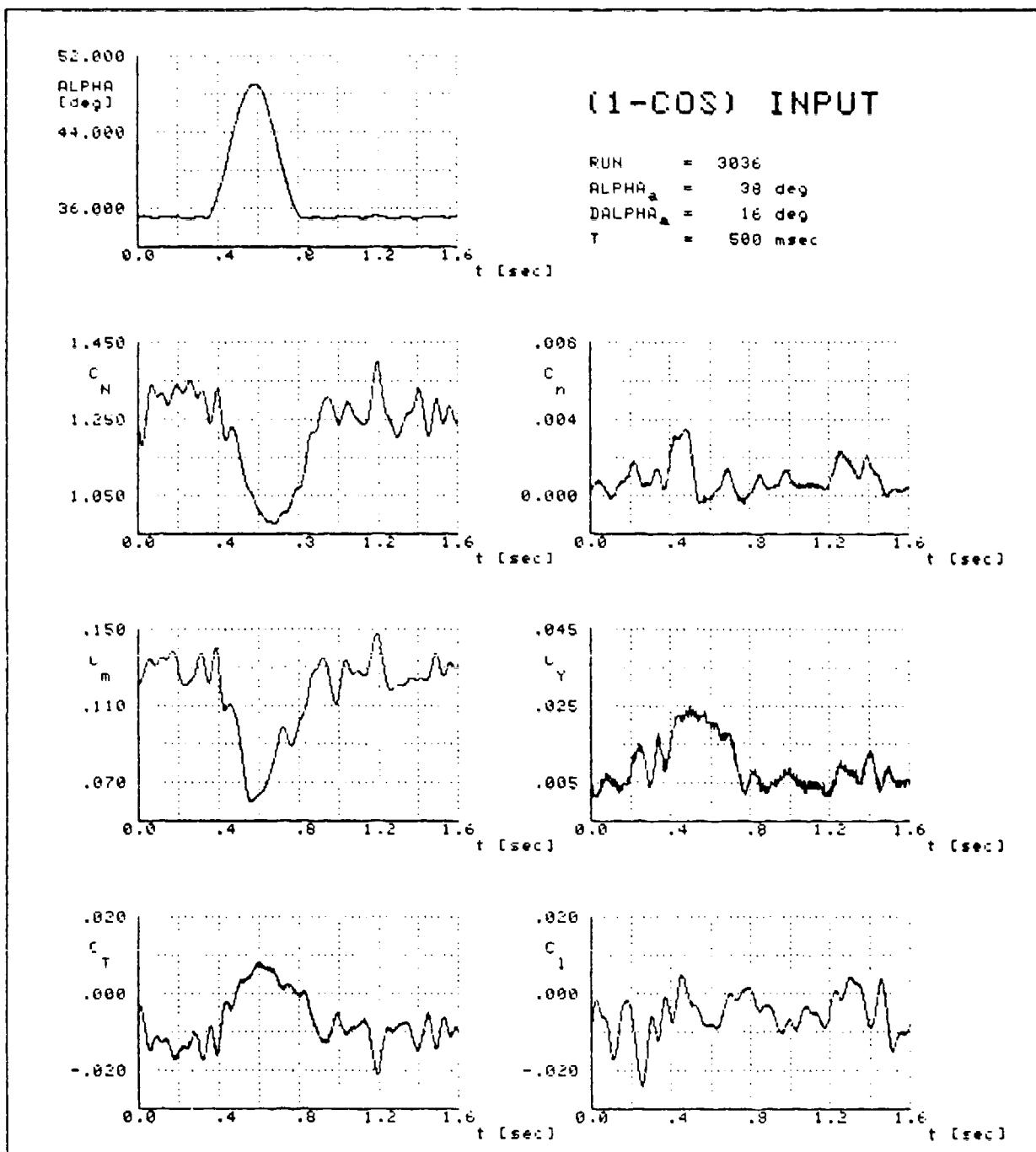
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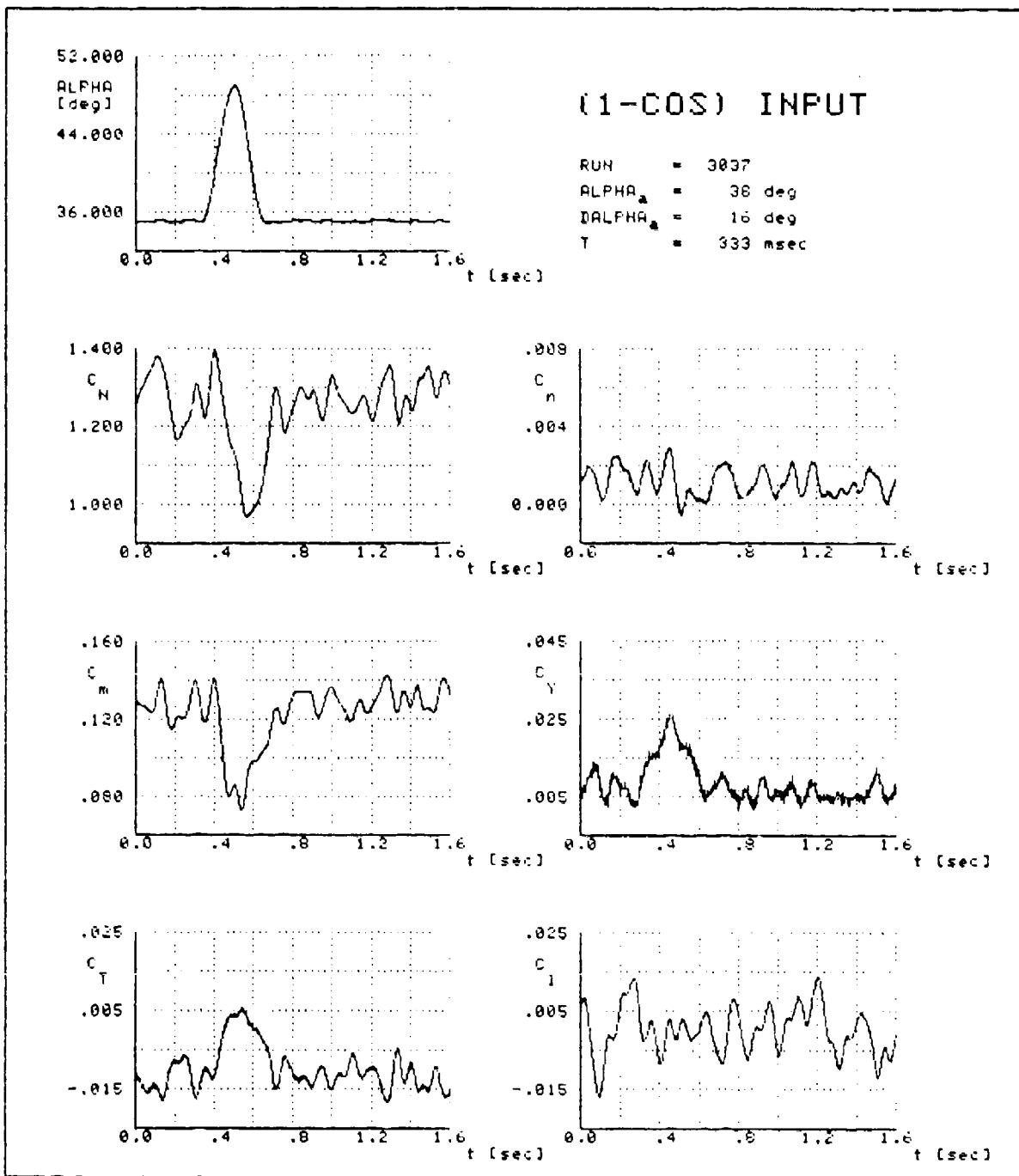
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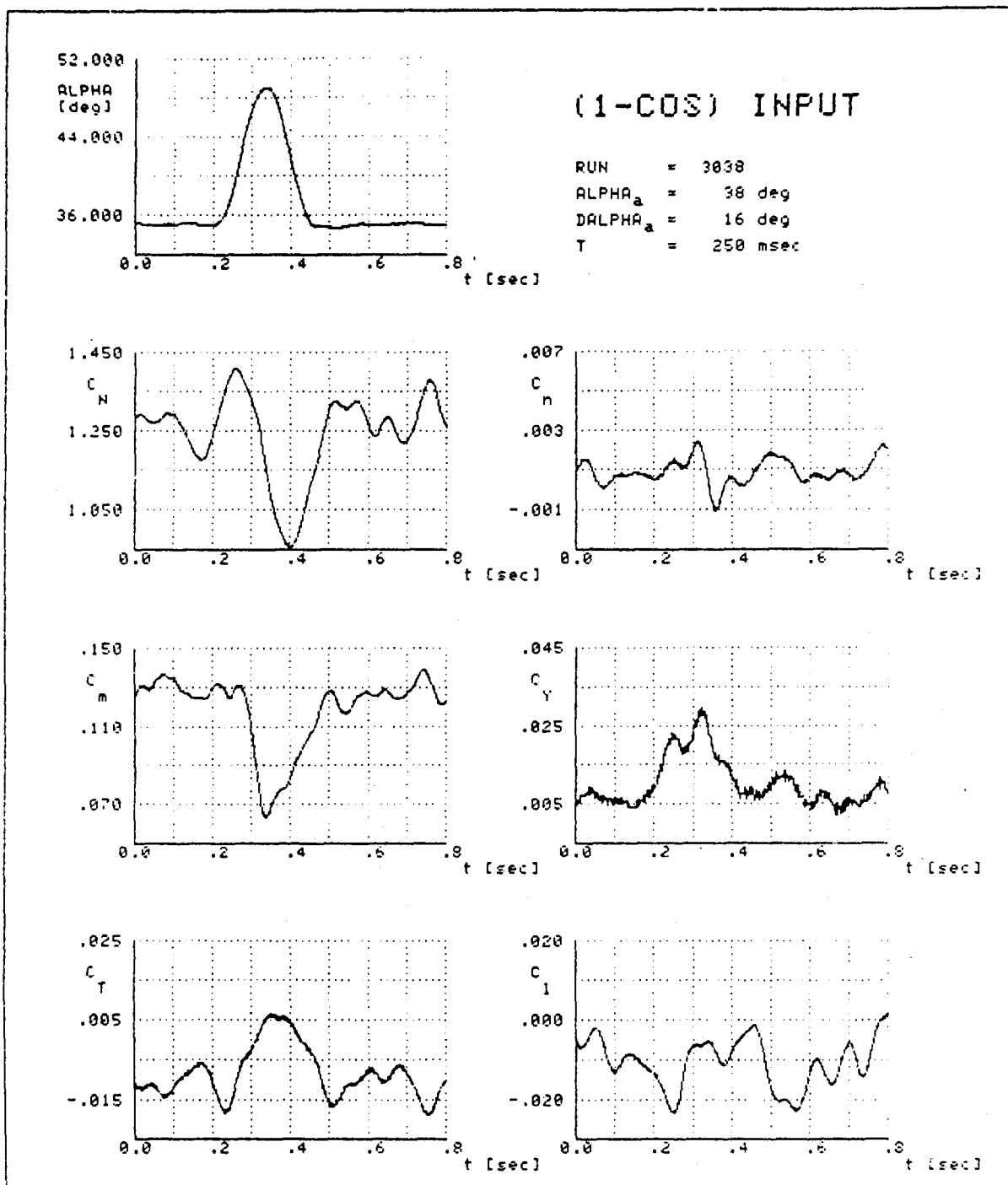


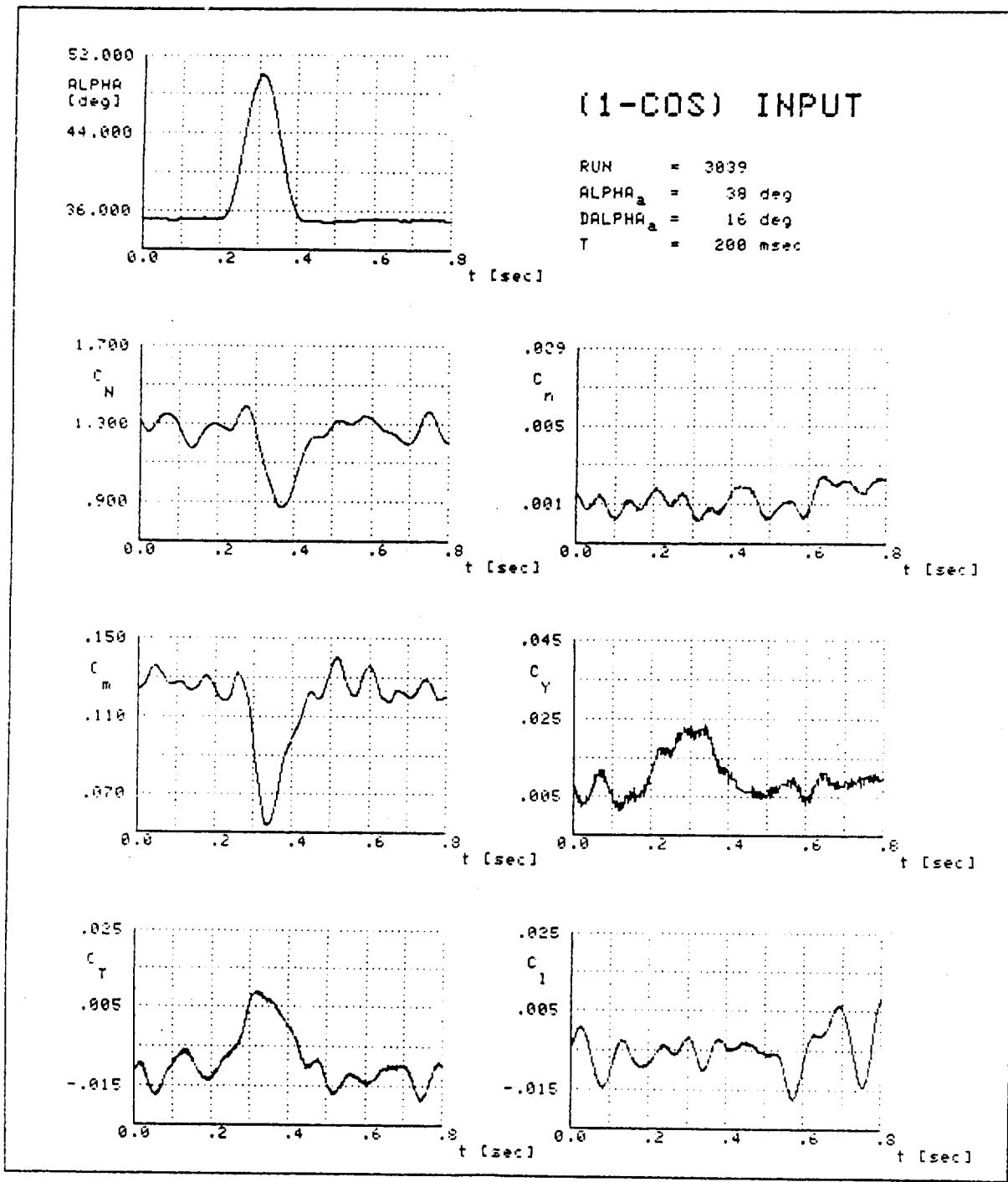


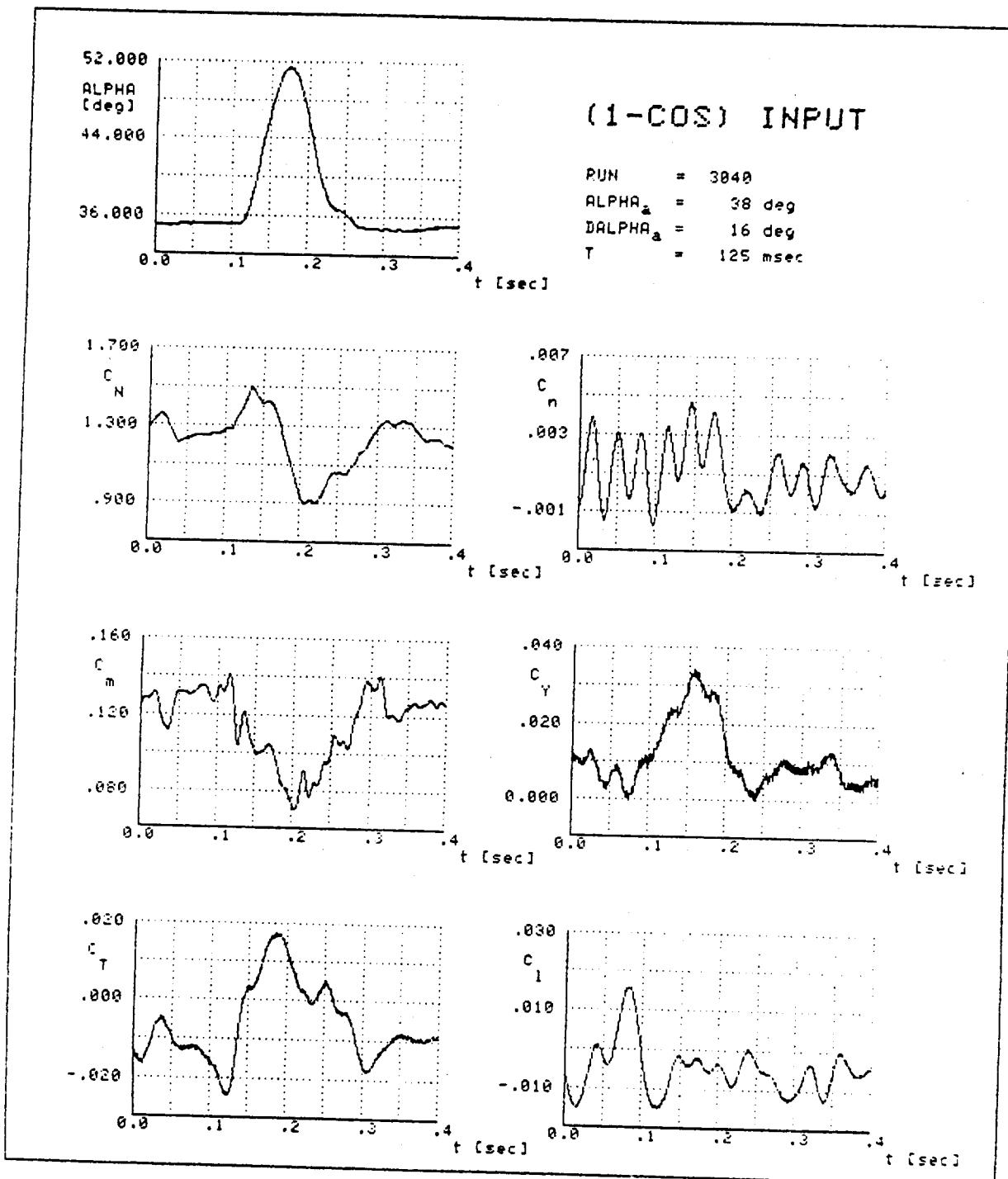


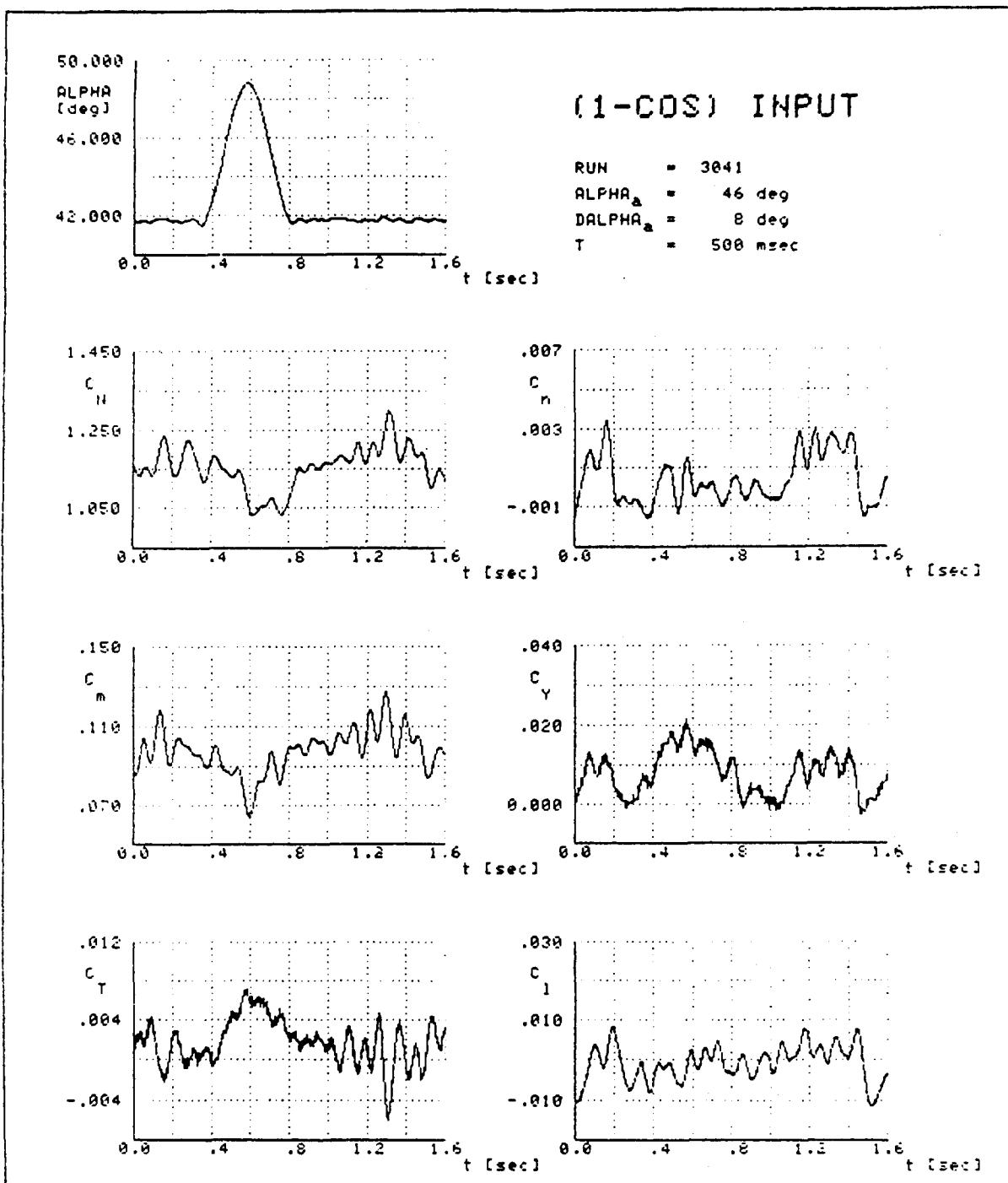


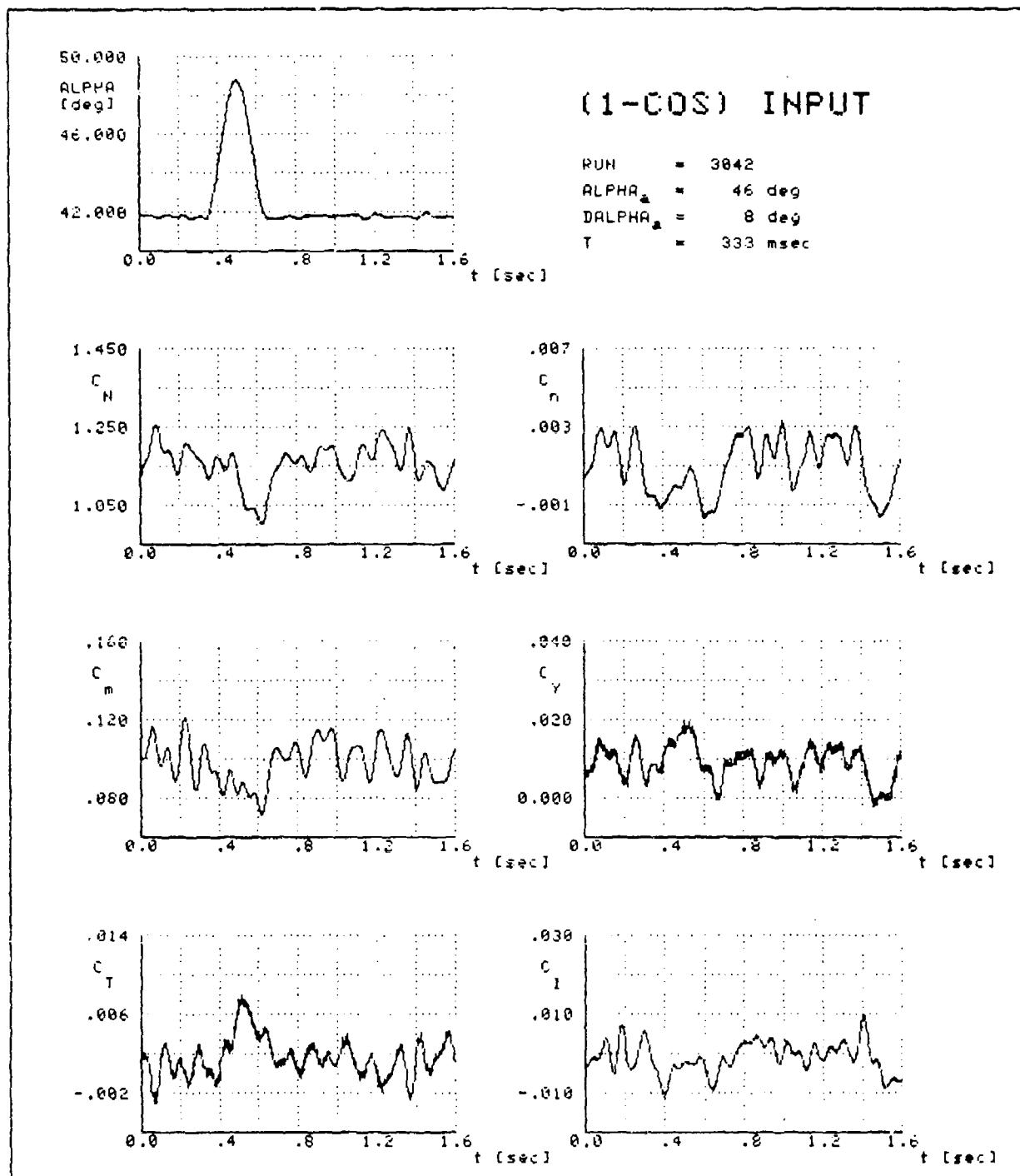


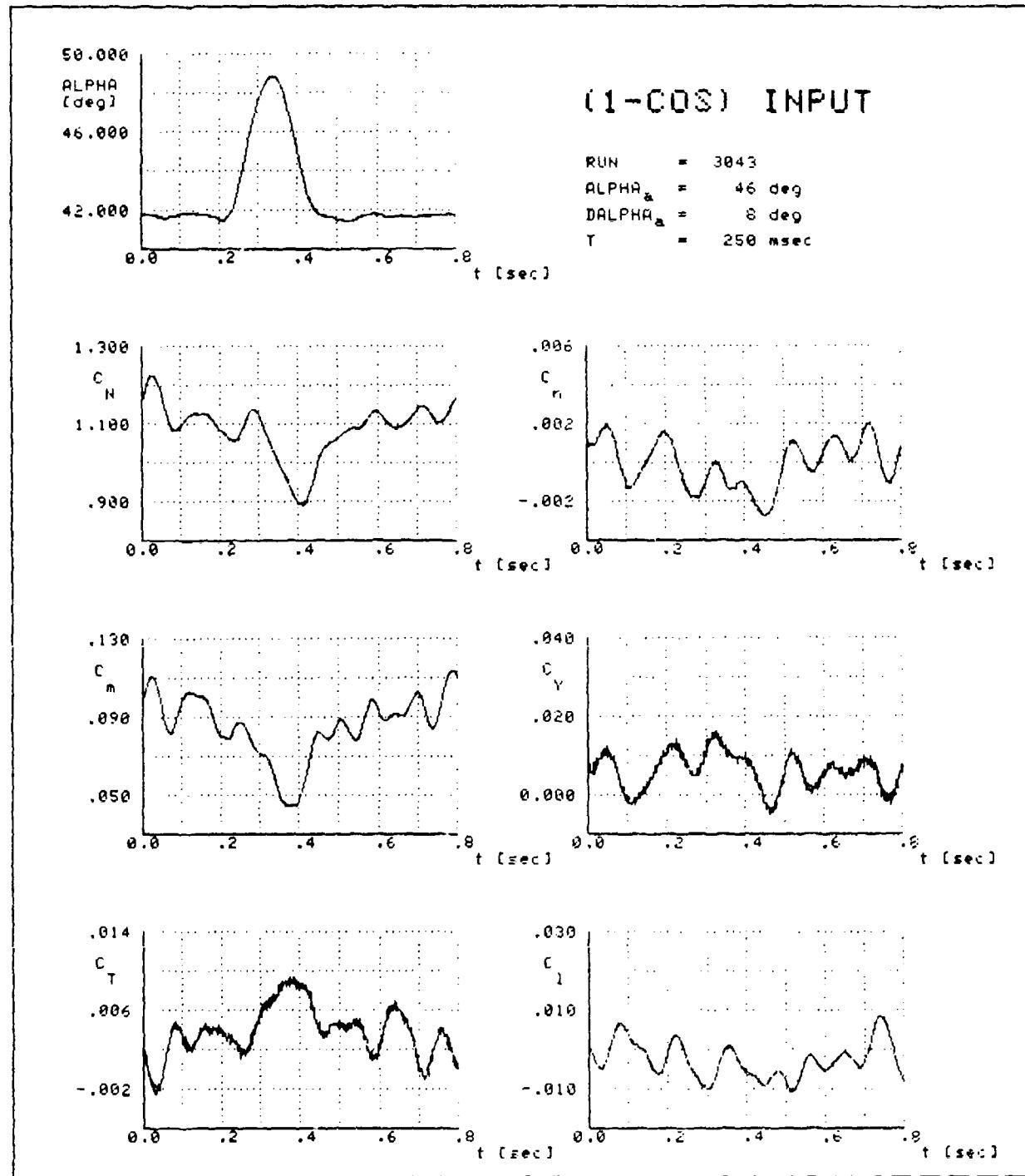


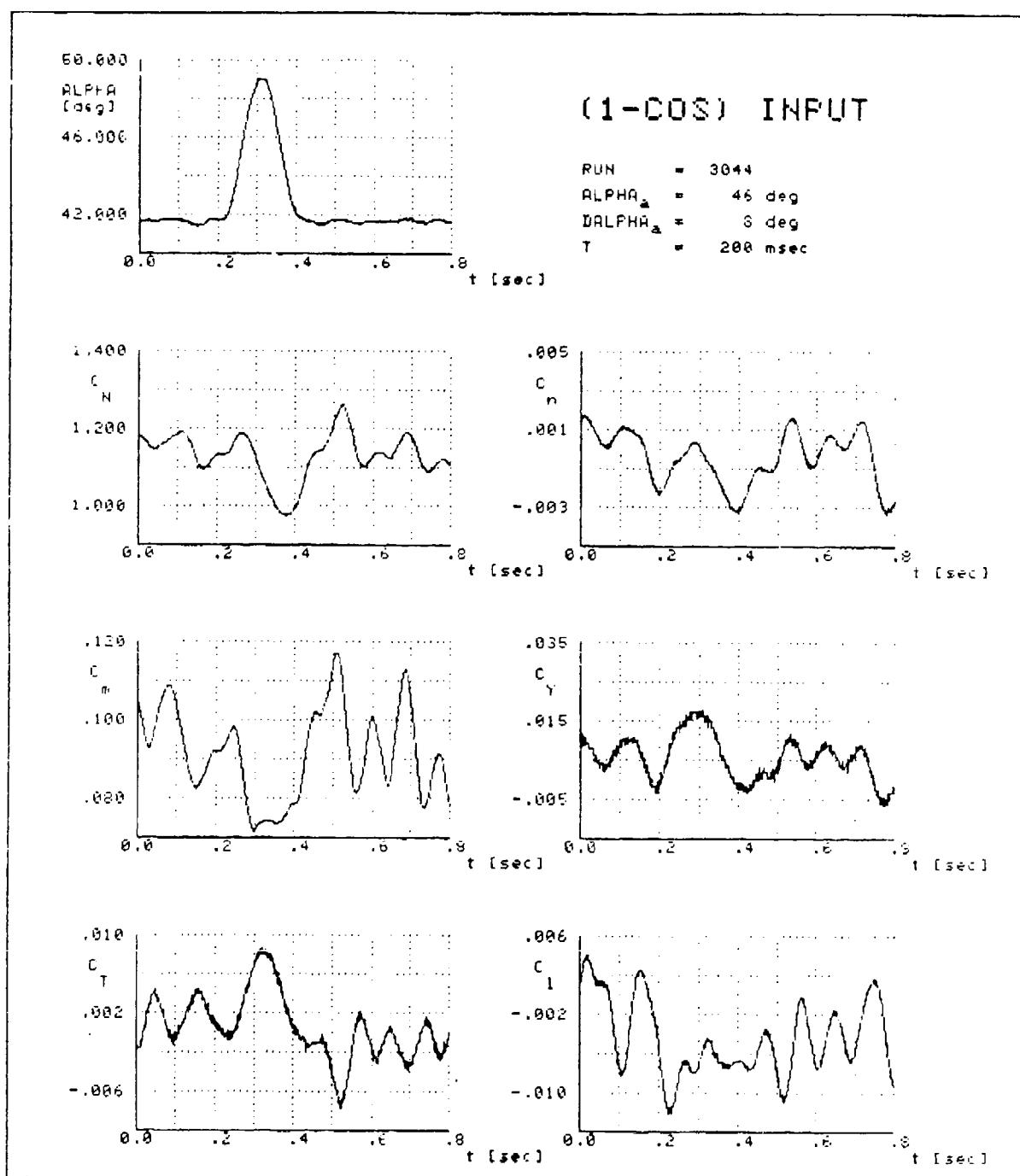


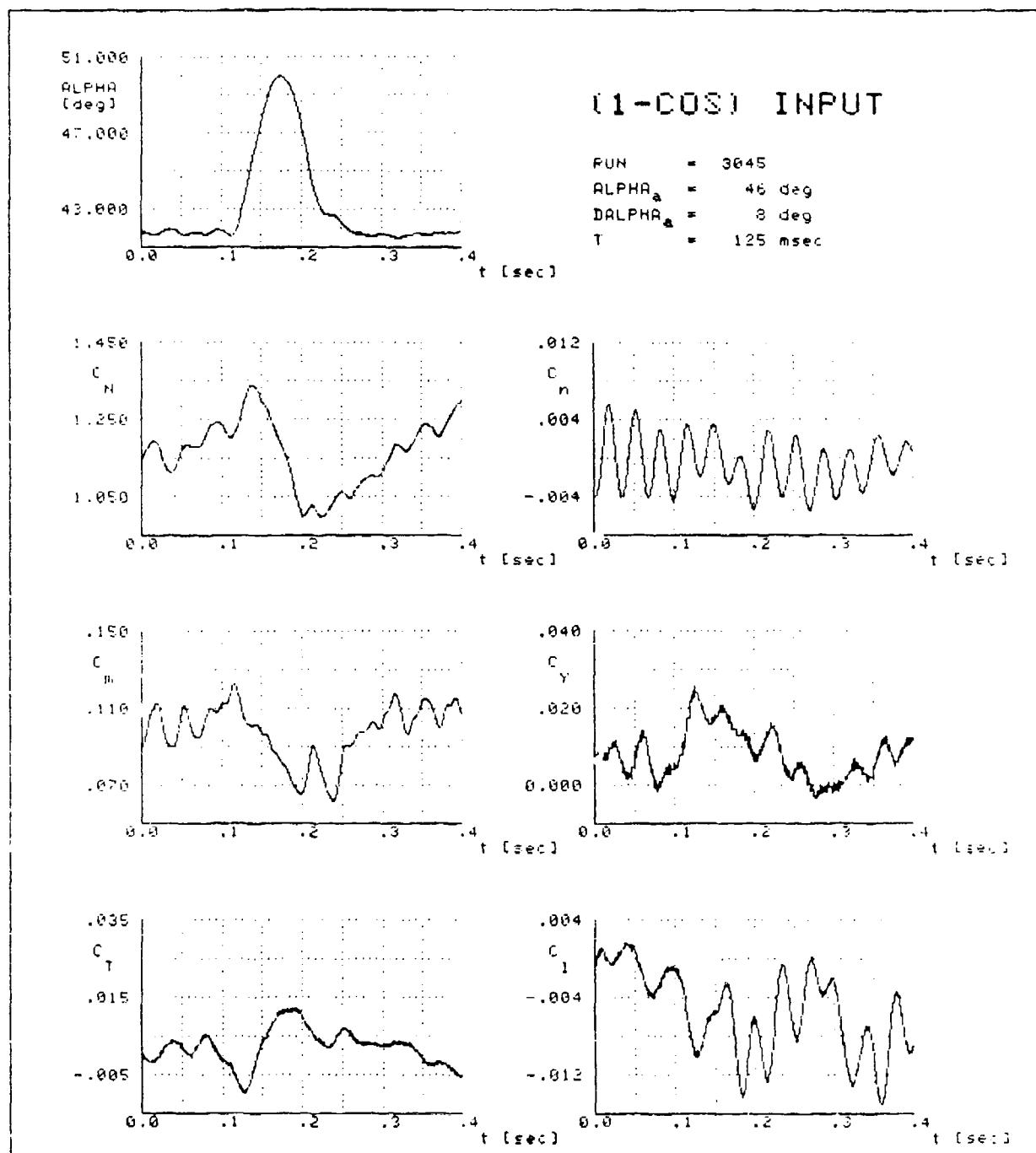


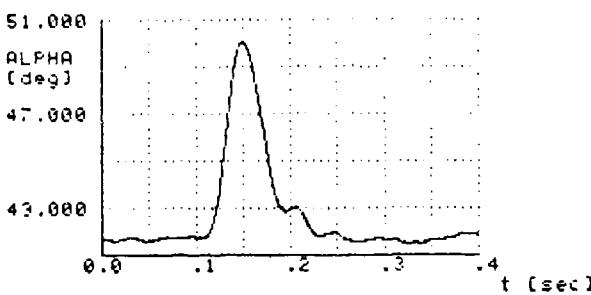






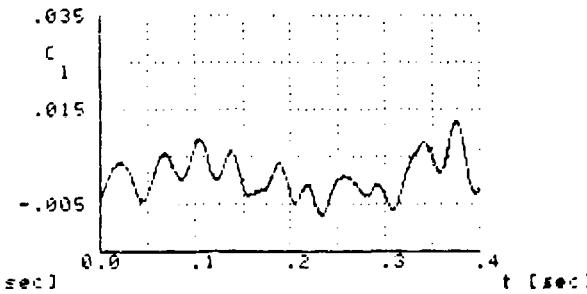
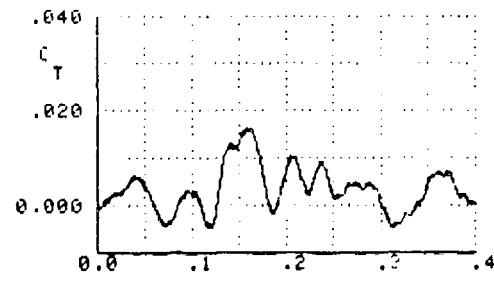
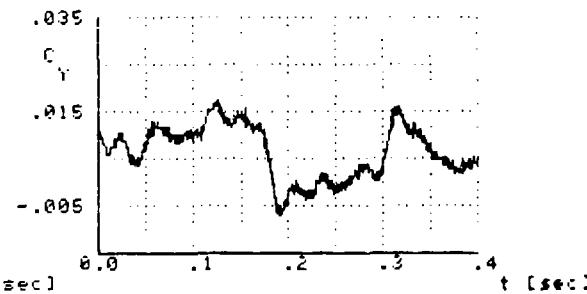
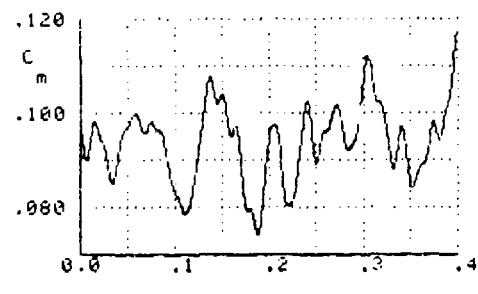
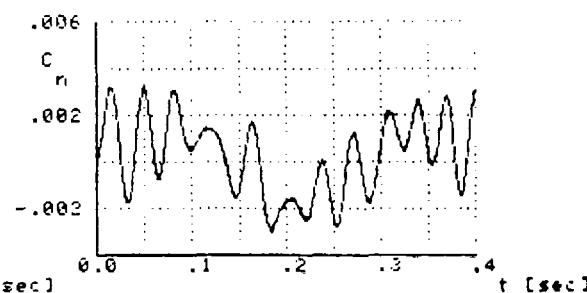
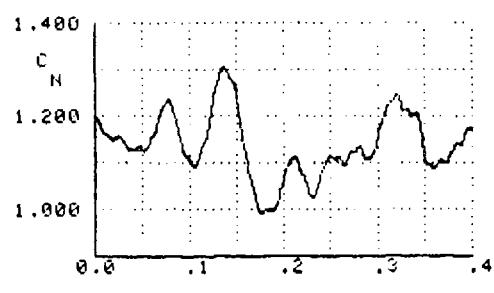


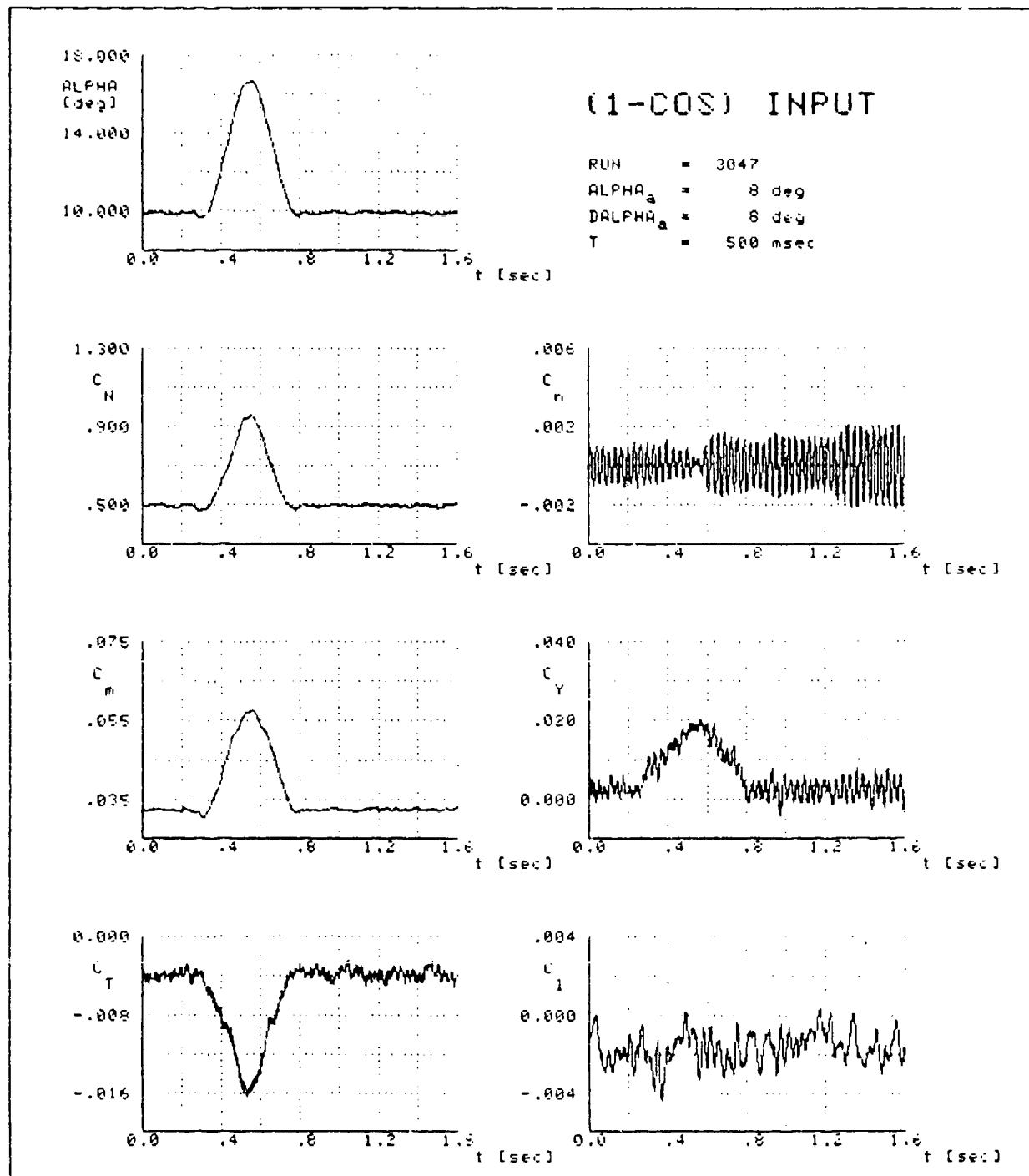


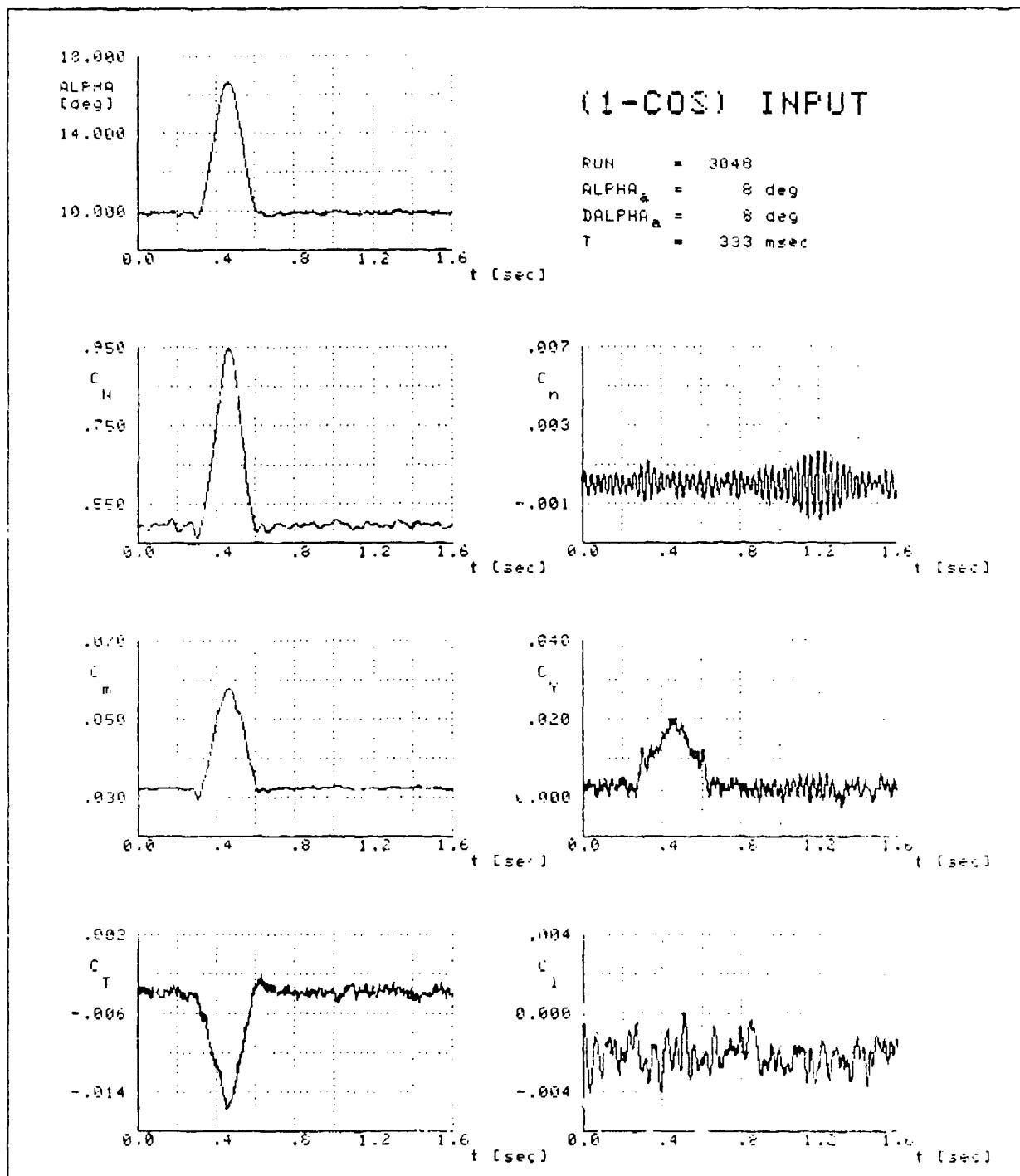


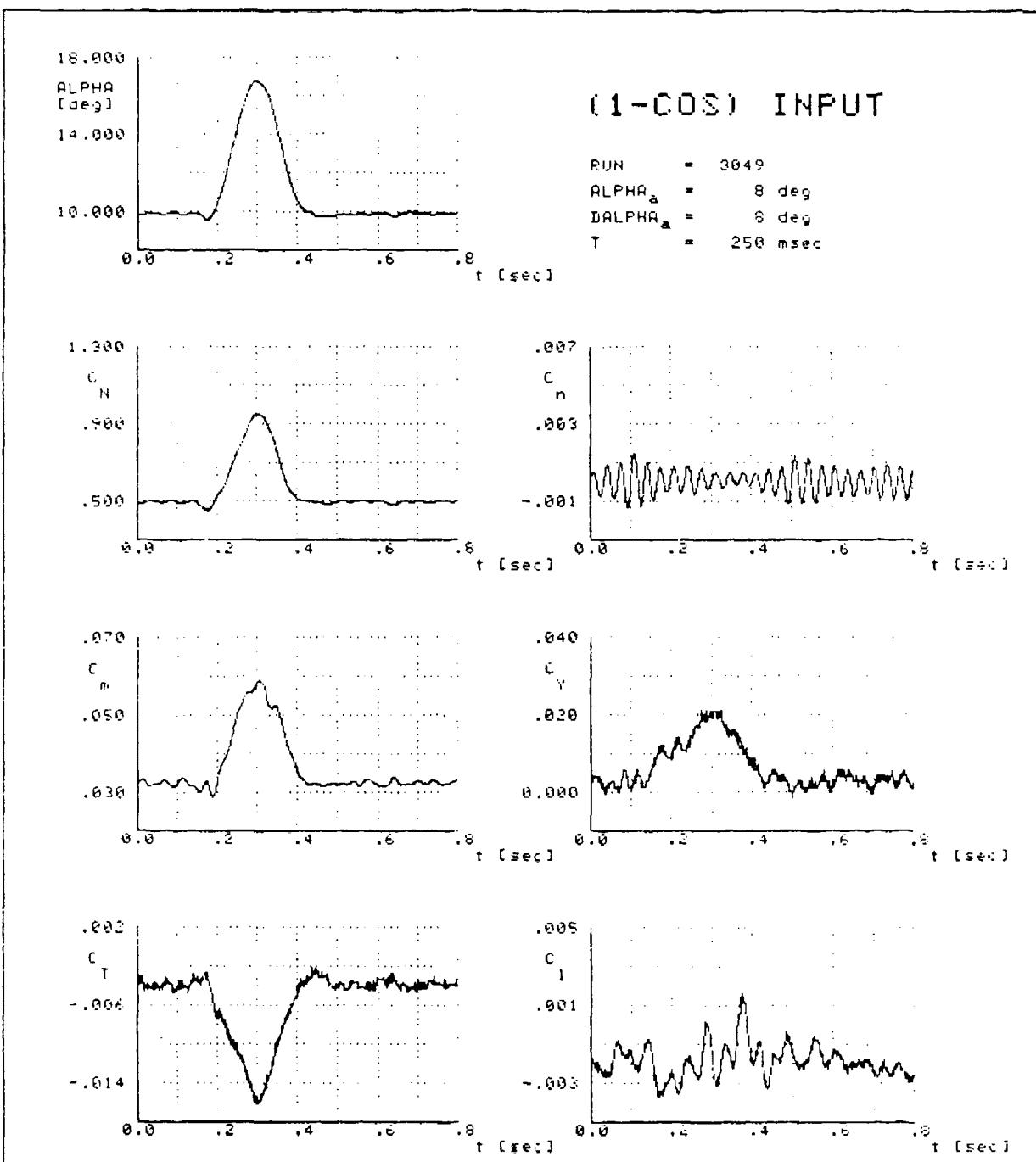
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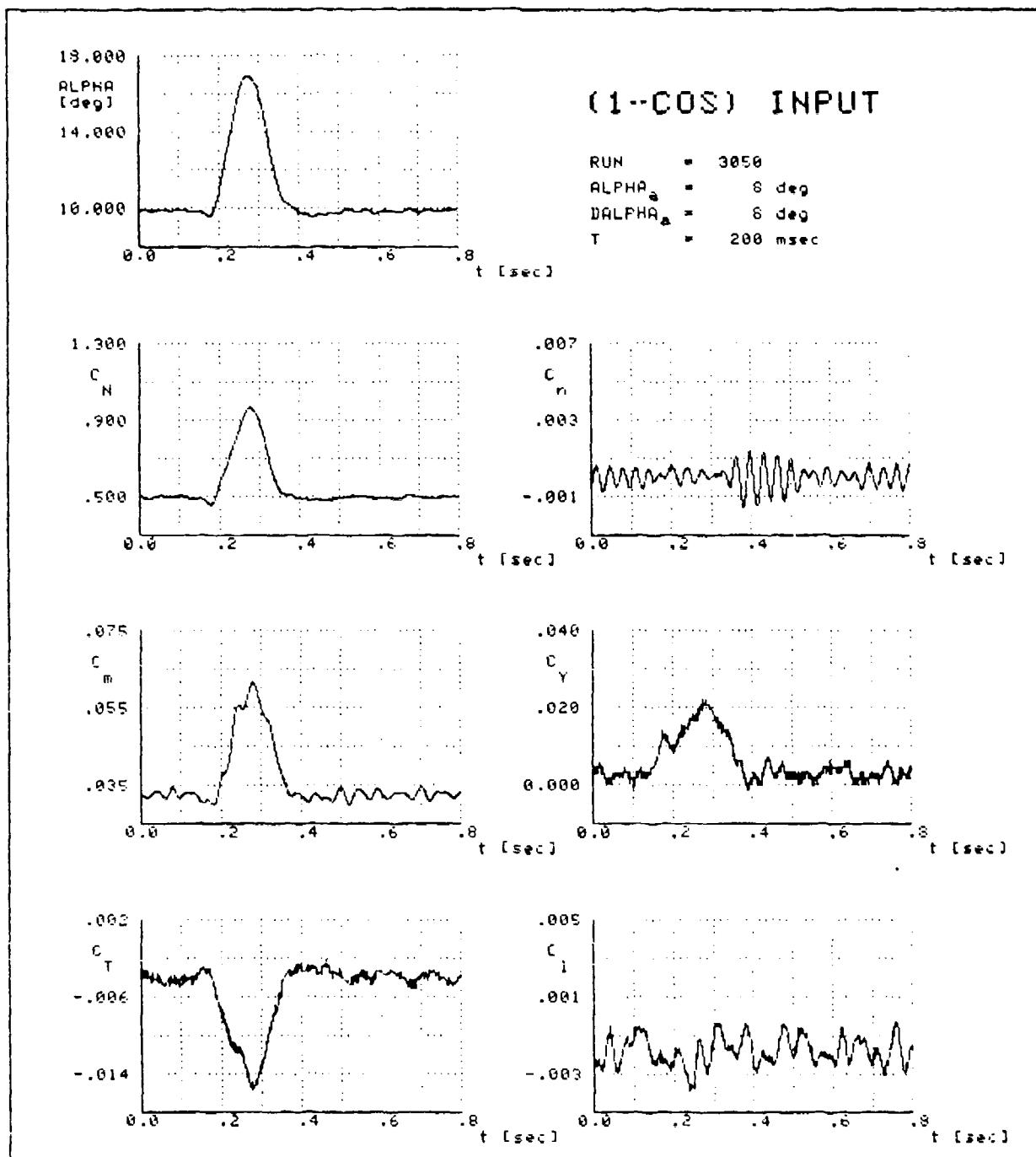
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DALPHA_a = 8 deg
T = 83 msec

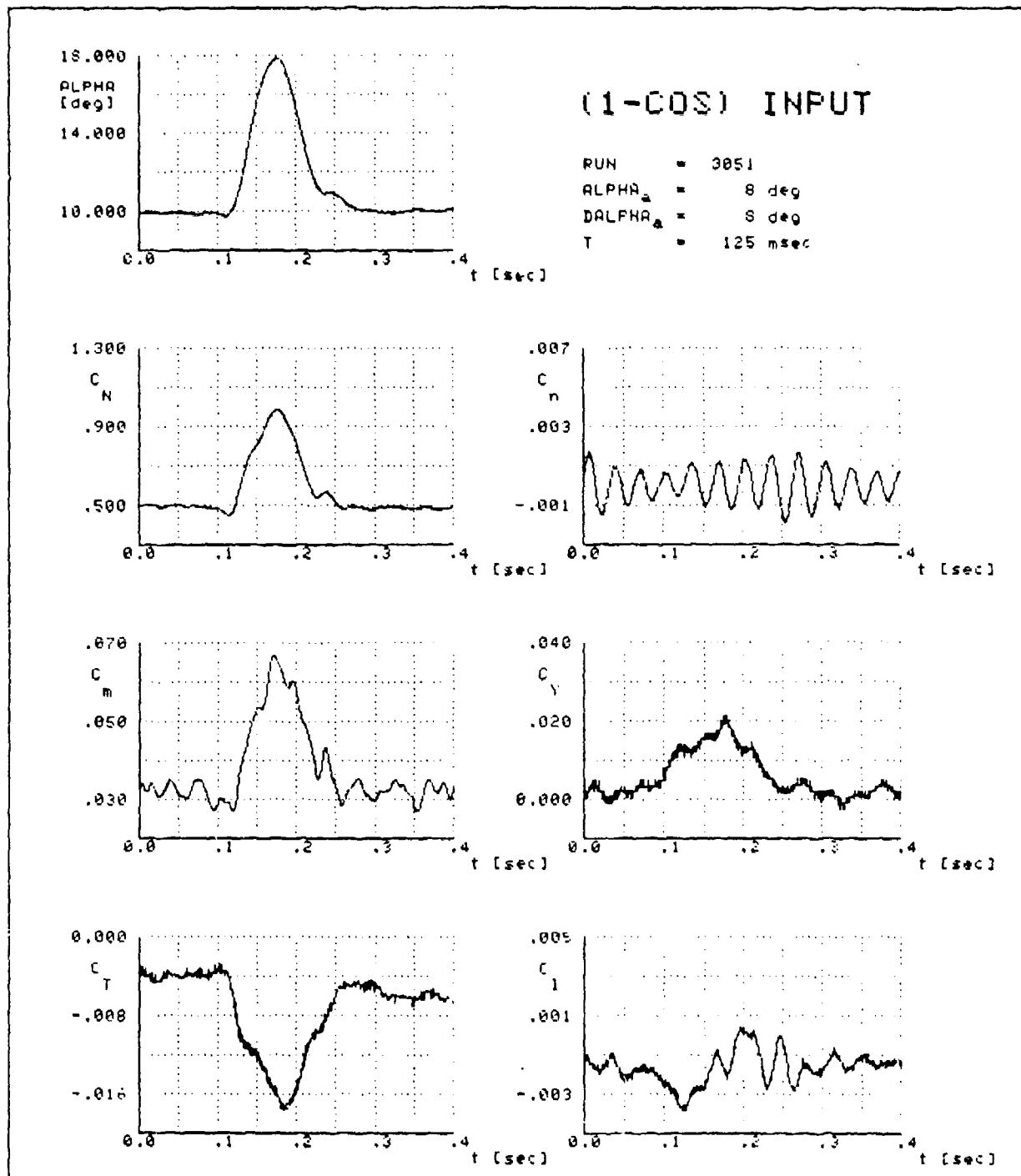


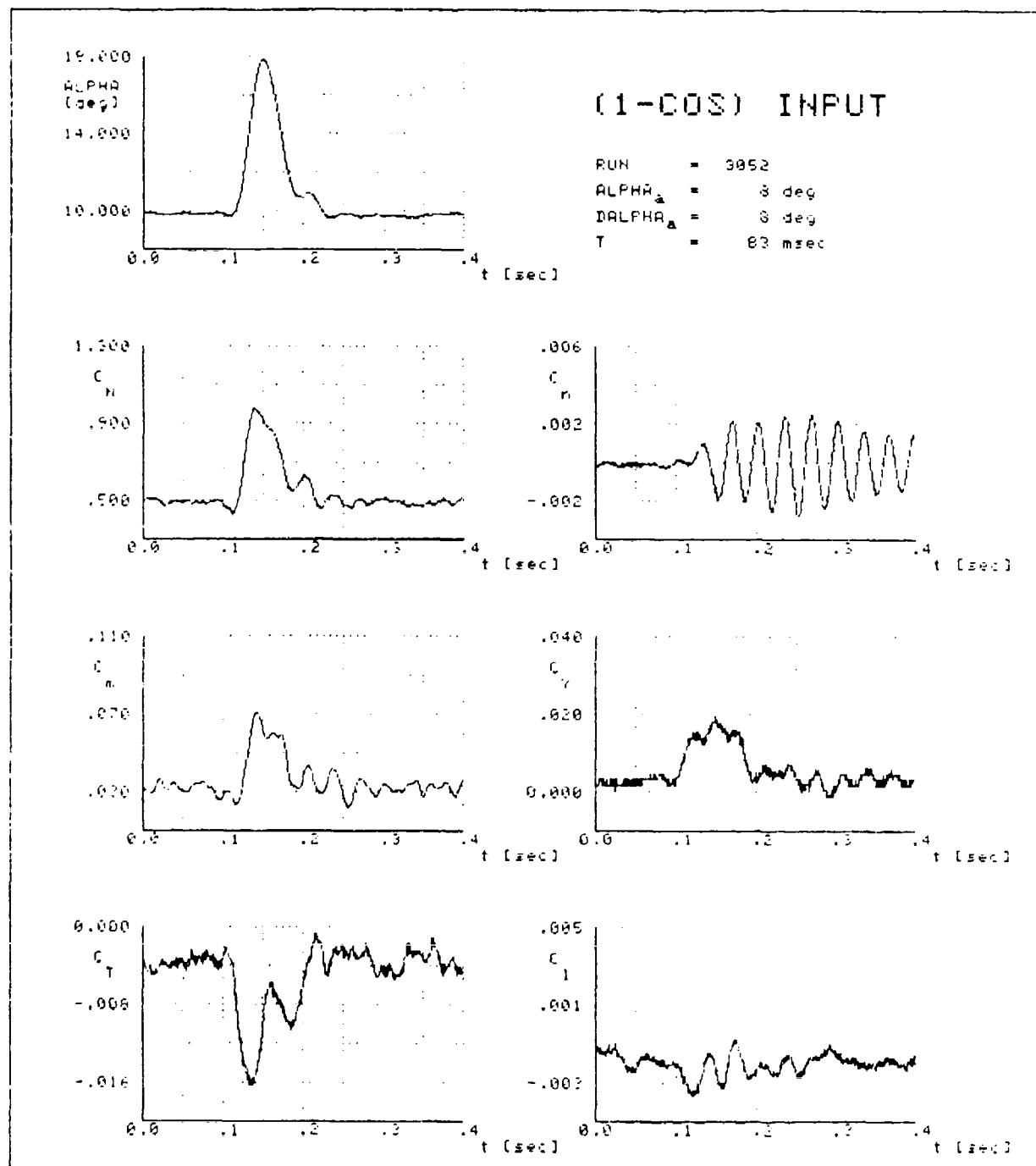


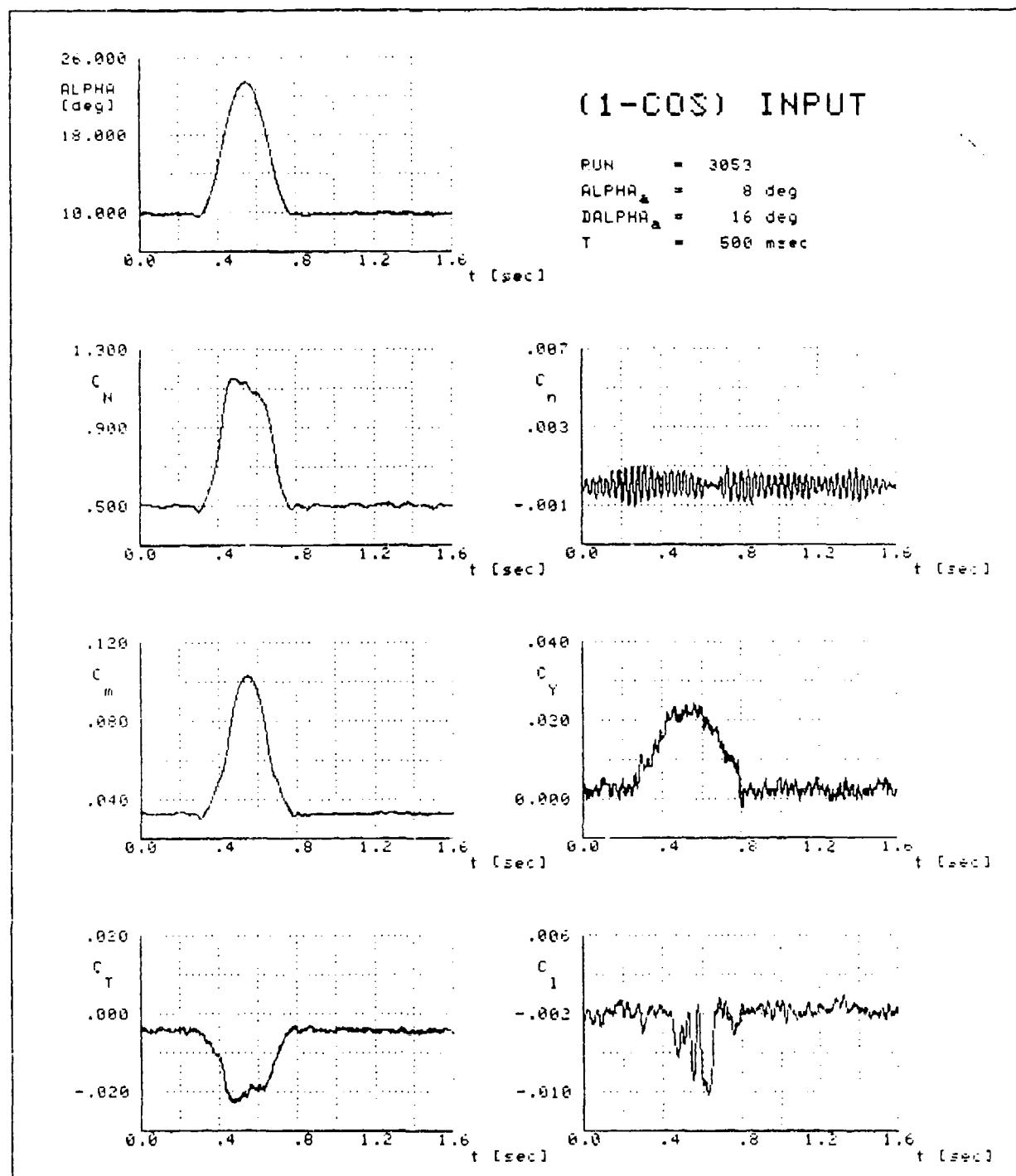


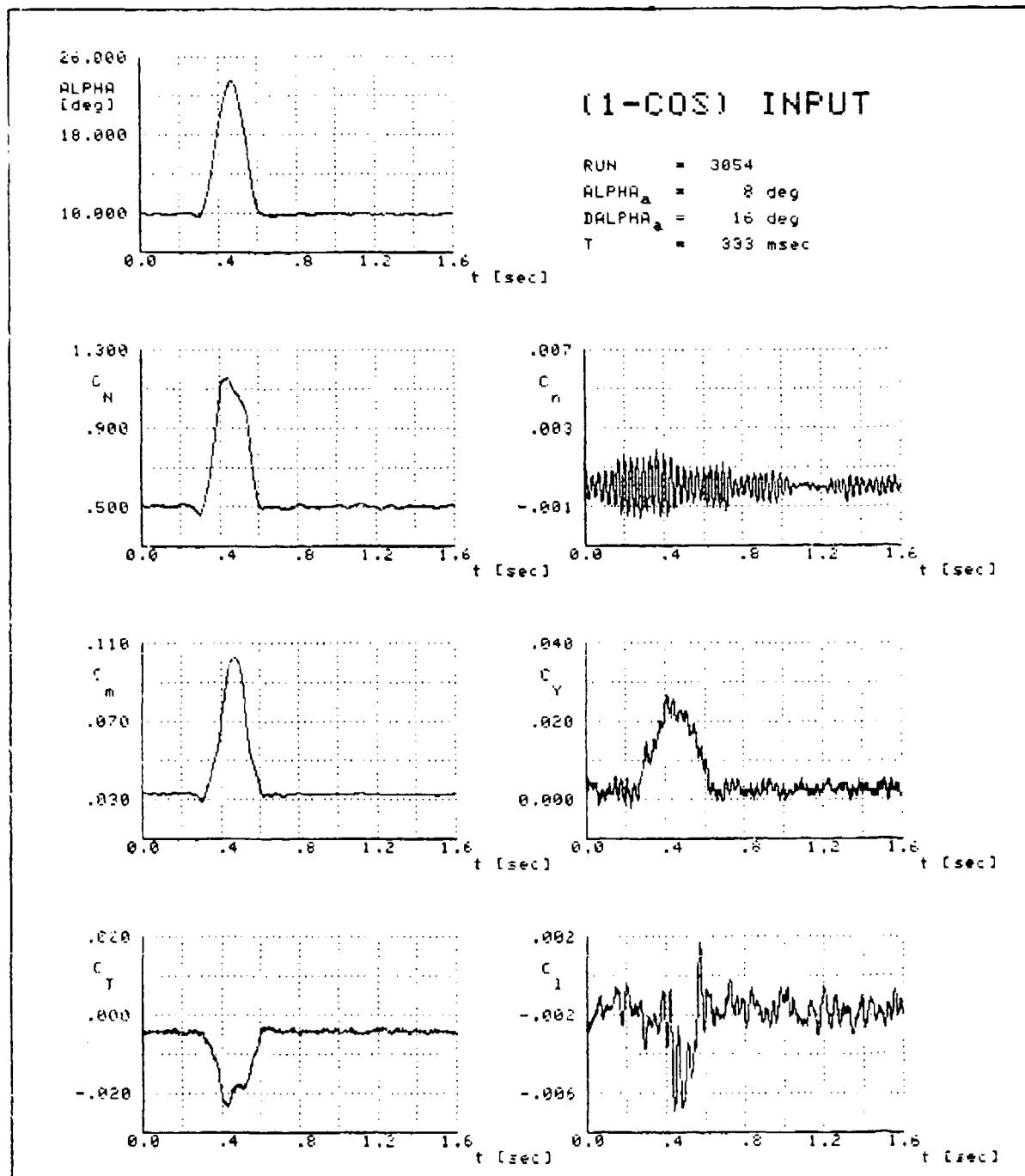


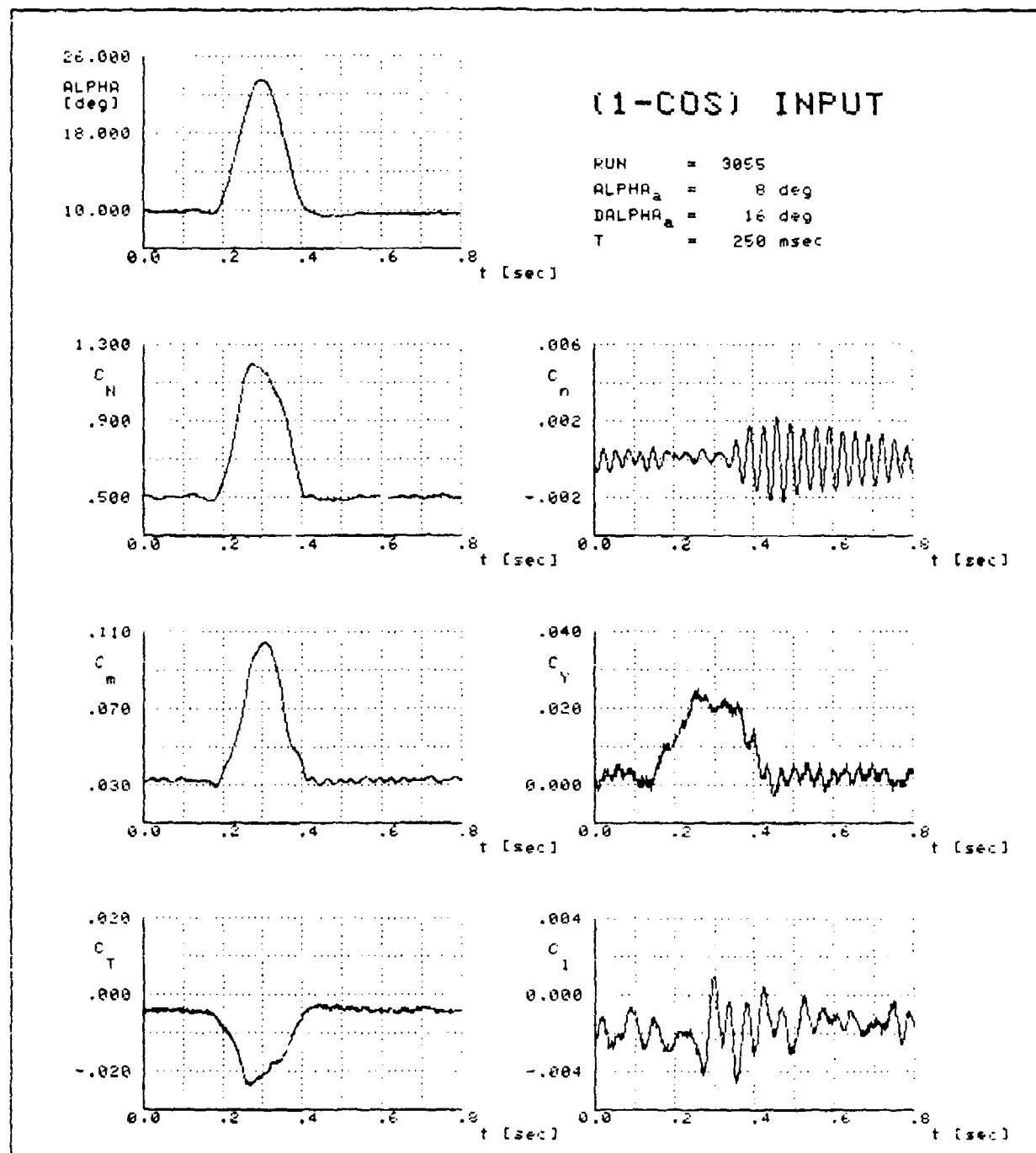


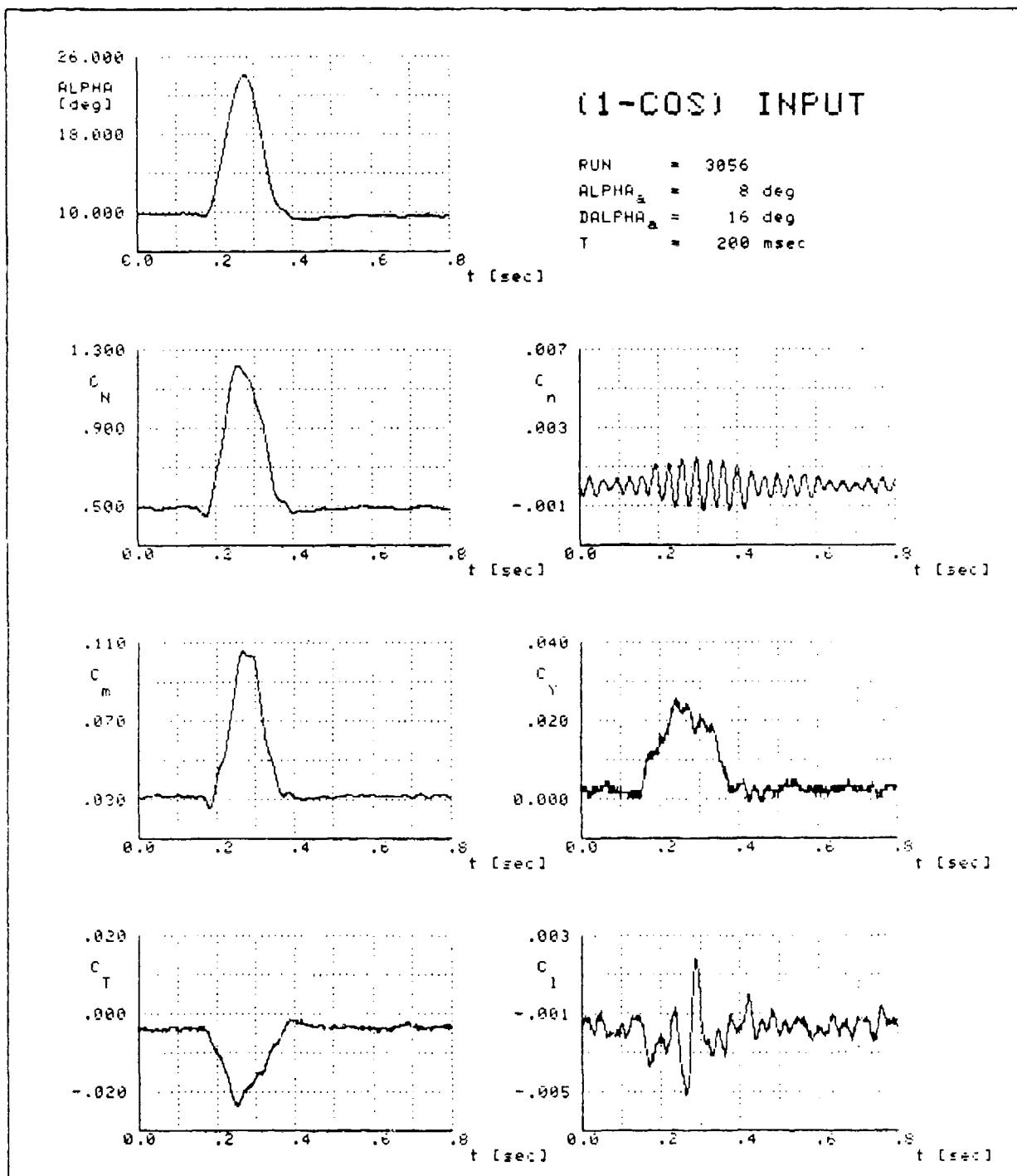


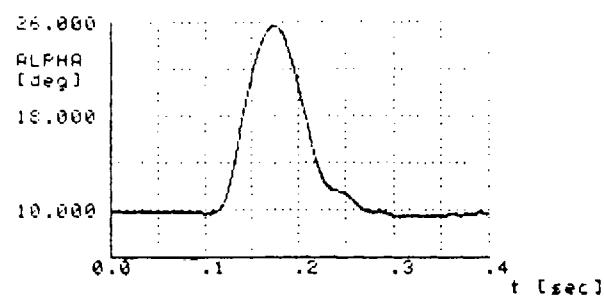






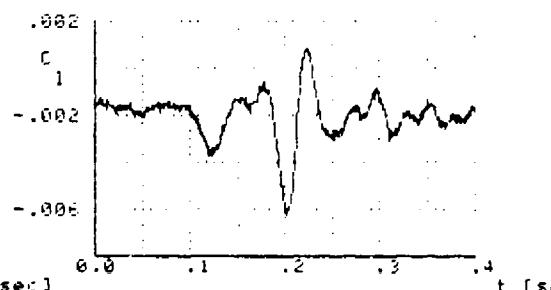
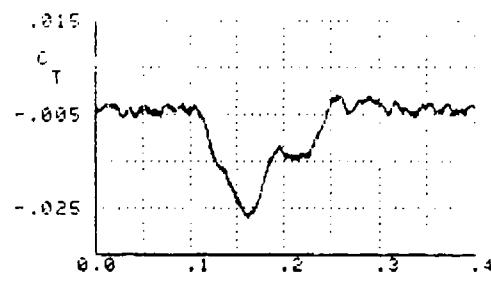
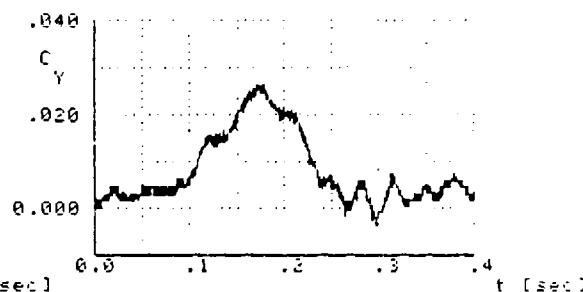
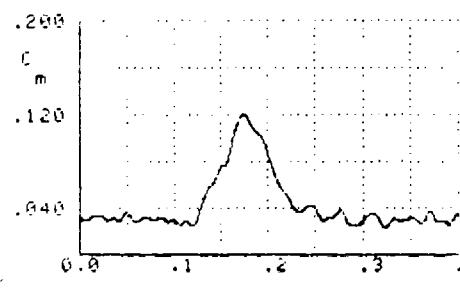
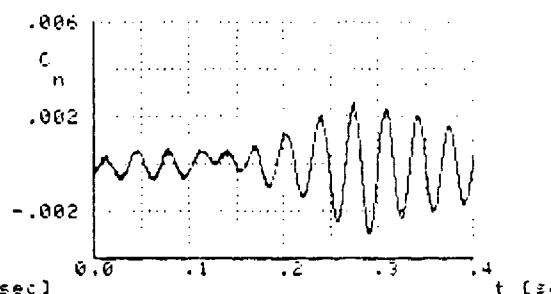
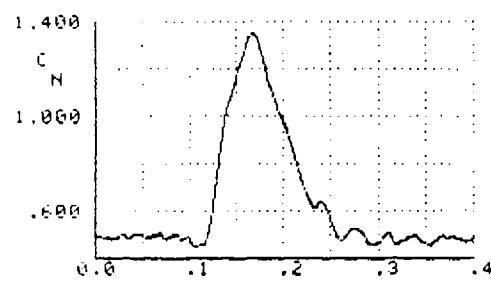


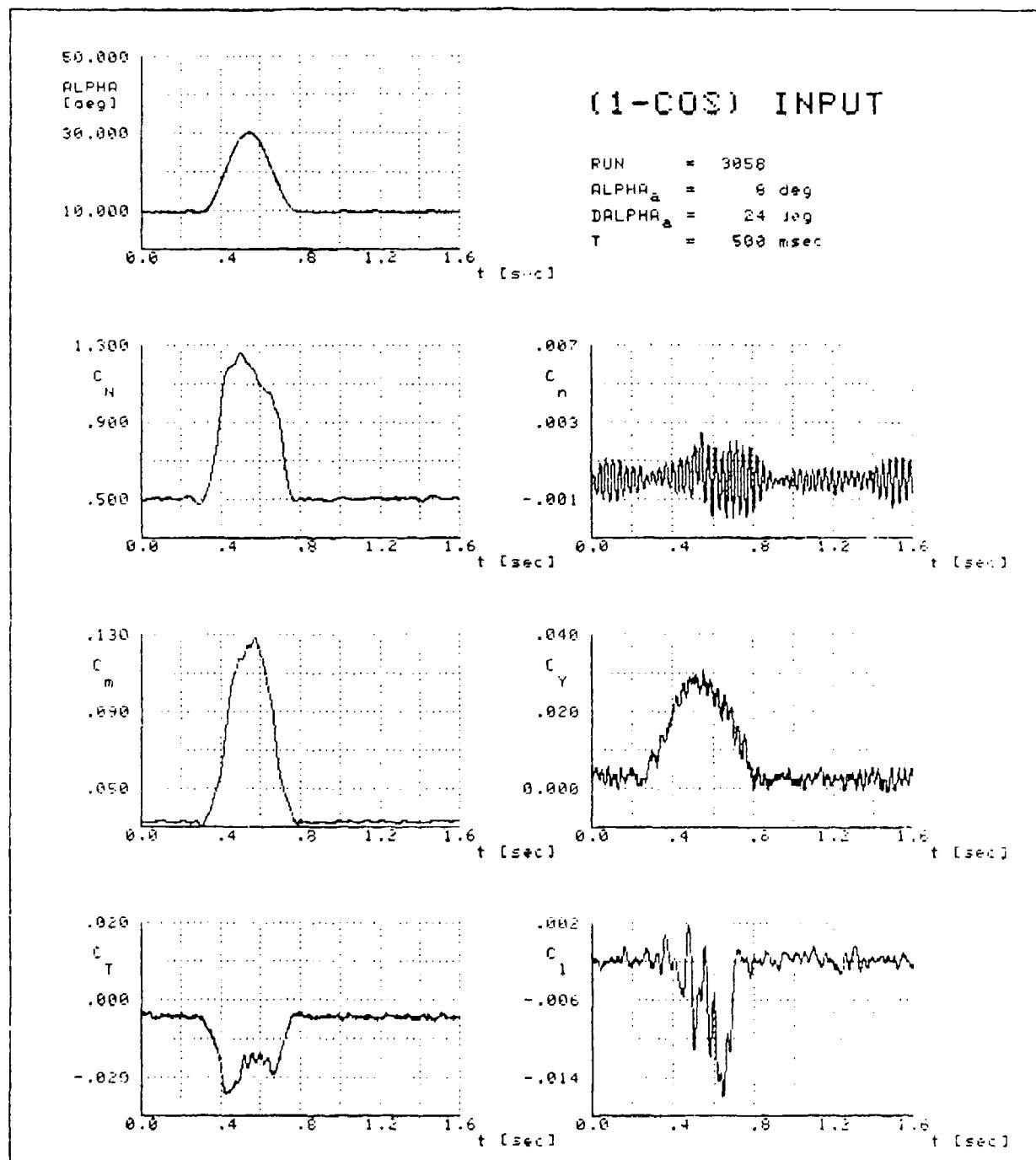


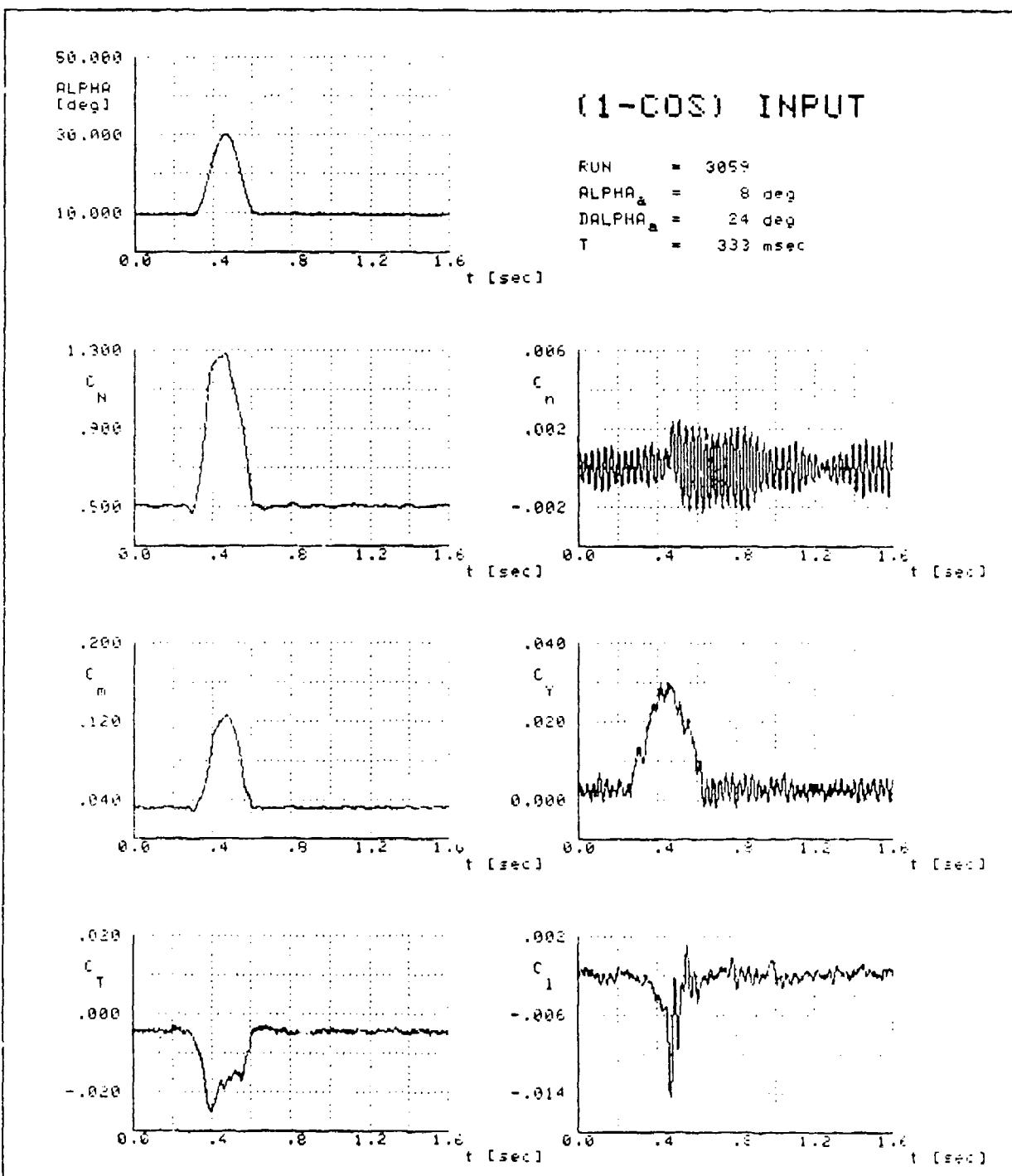


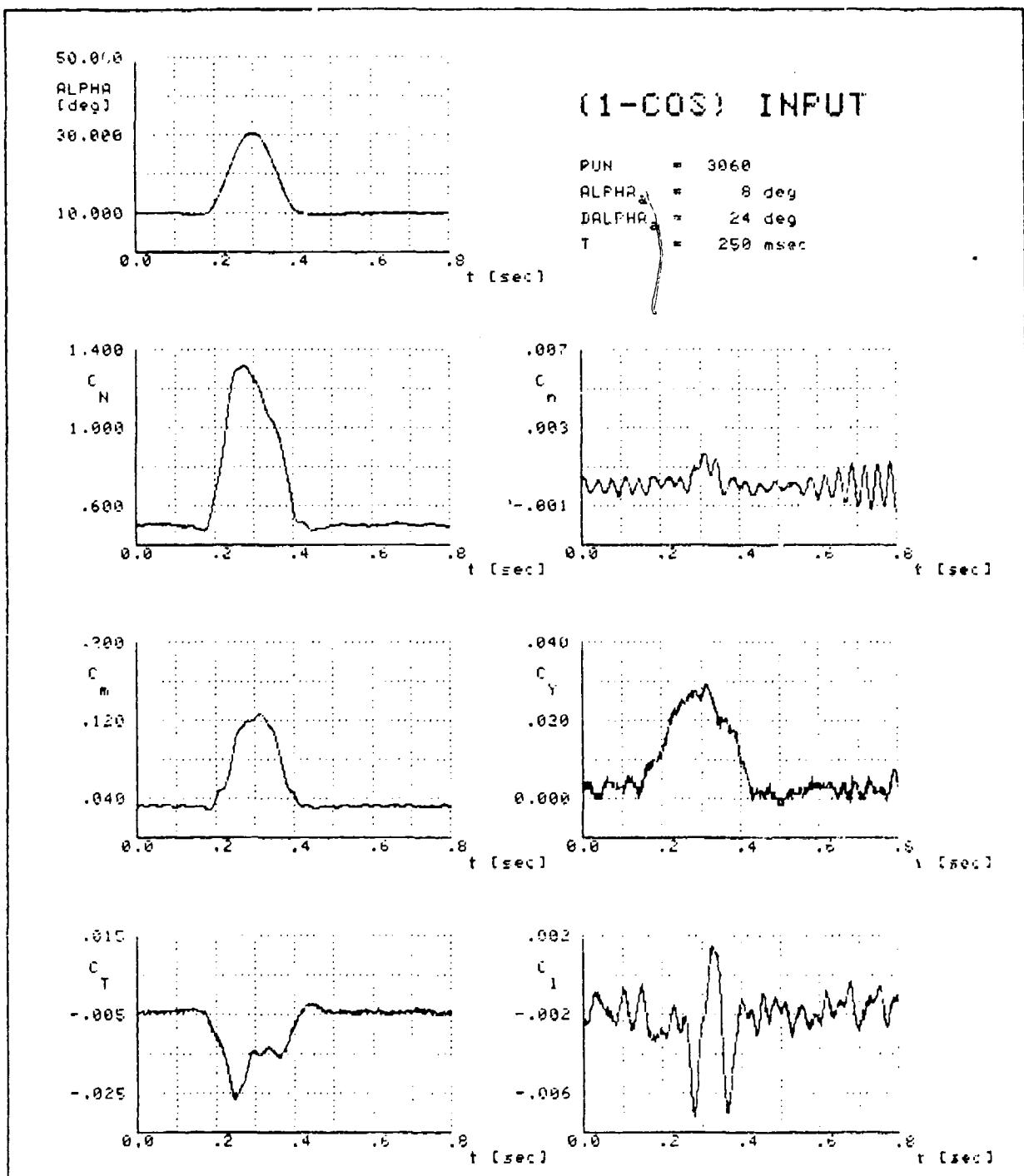
(1-COS) INPUT

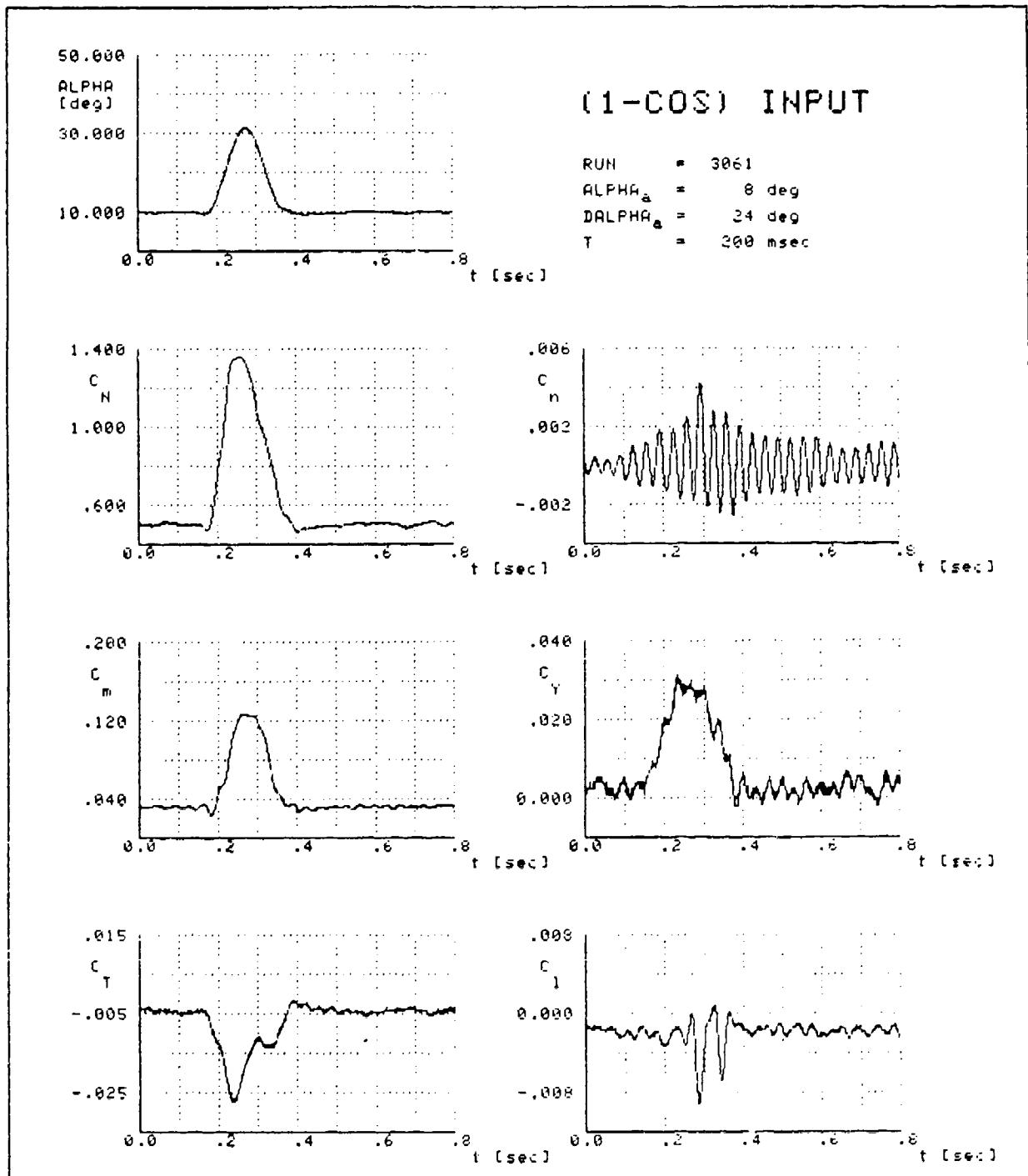
RUN = 3057
 ALPHA_s = 8 deg
 DALPHA_a = 16 deg
 T = 125 msec

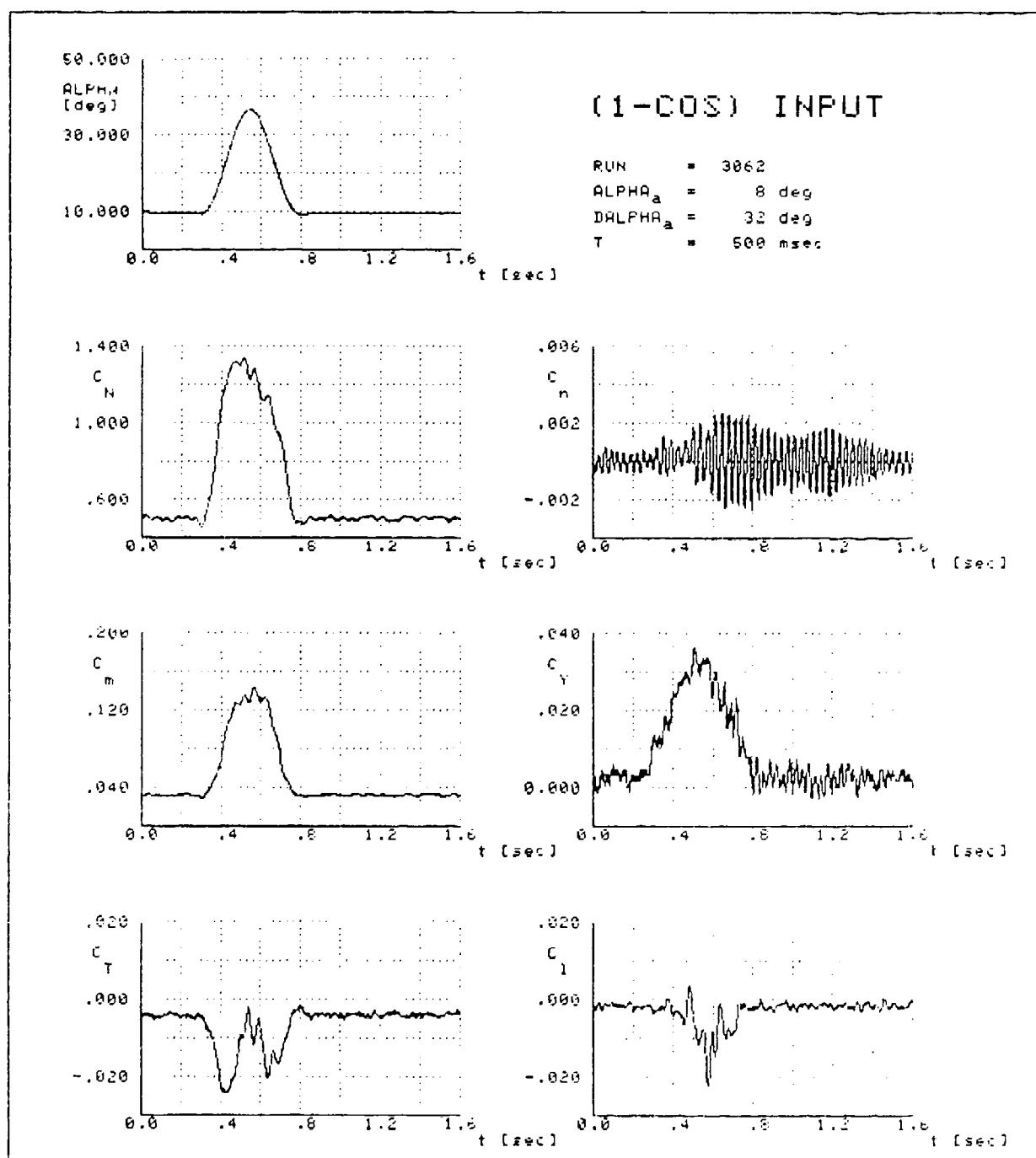


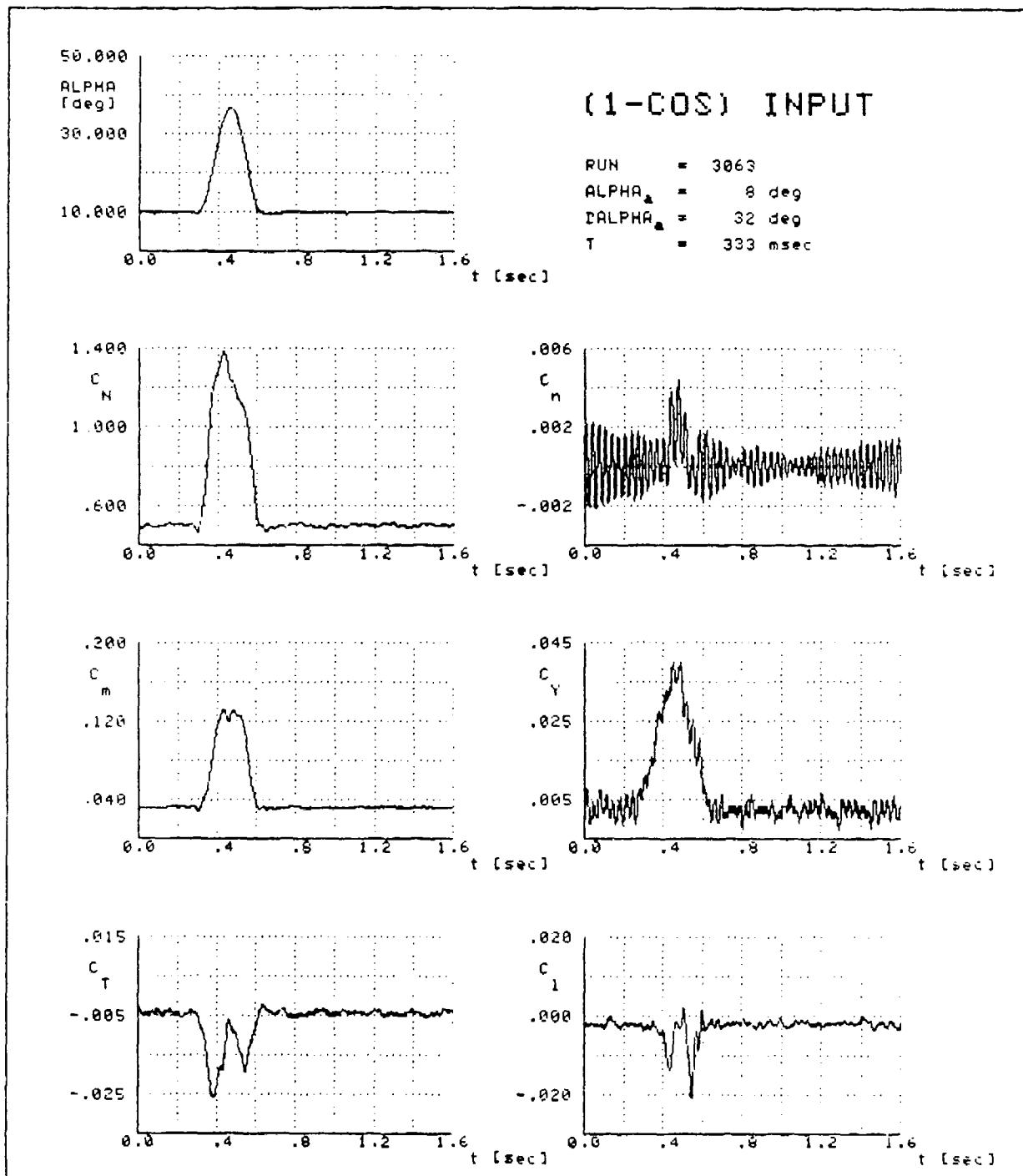


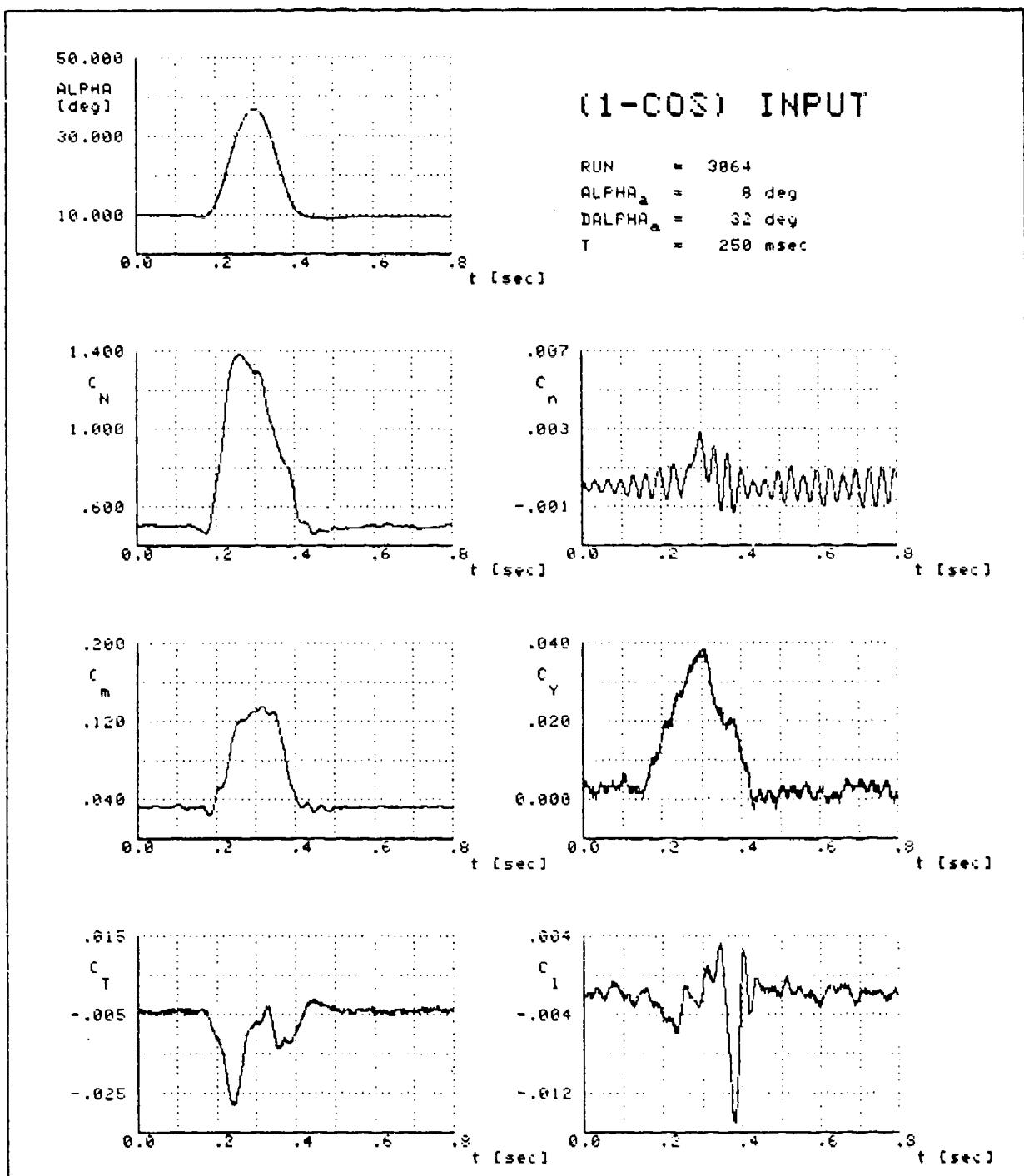


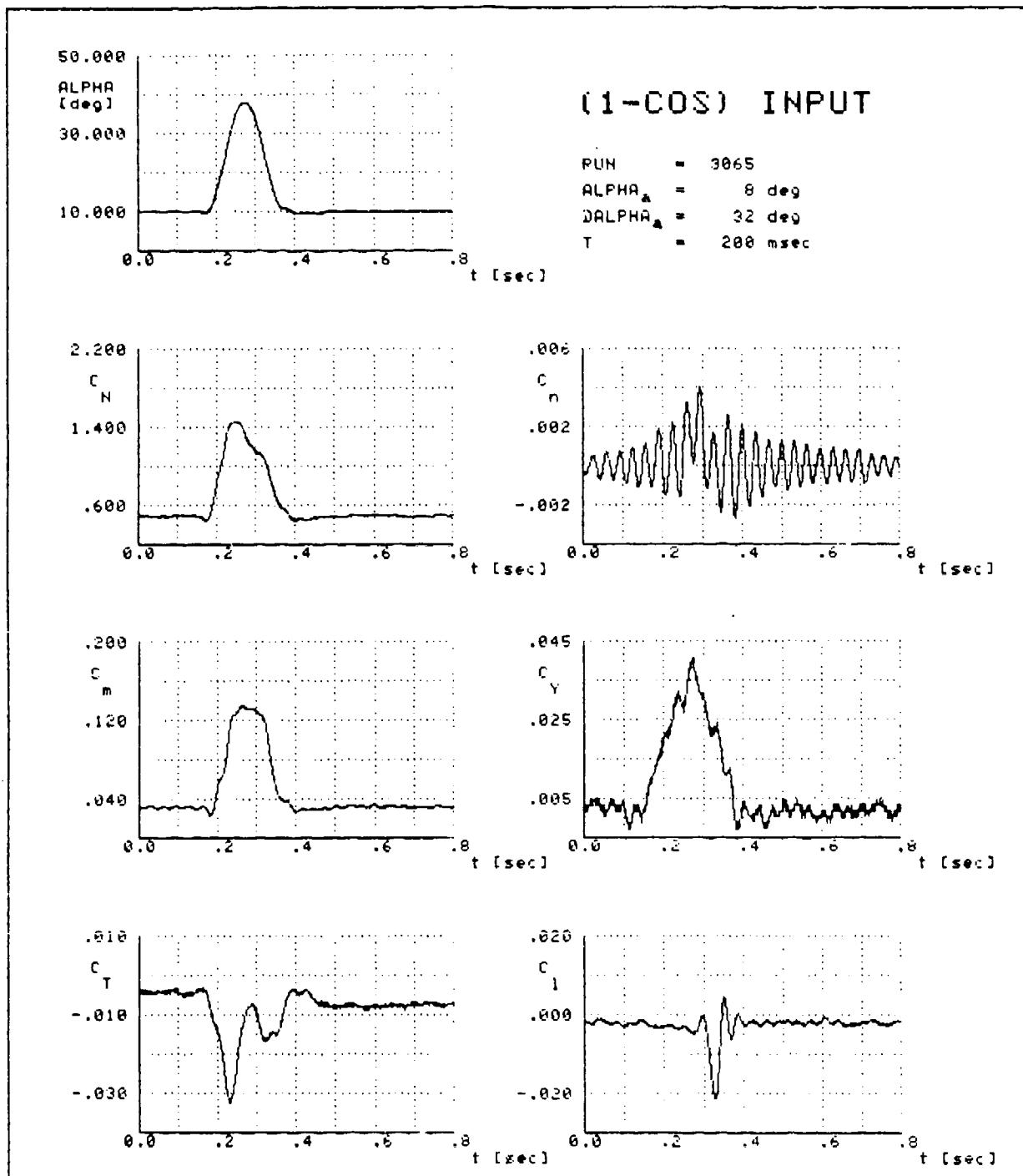


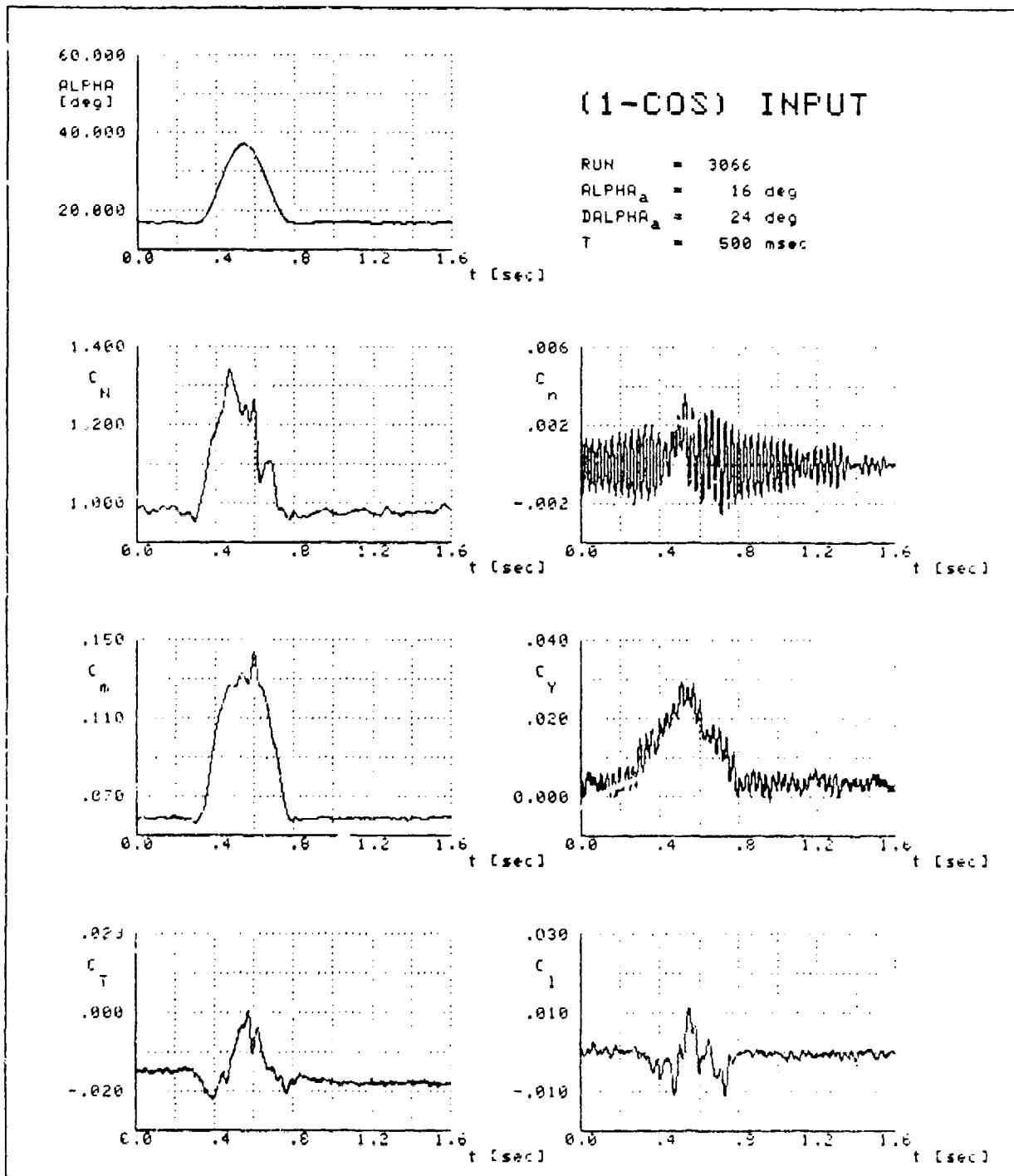


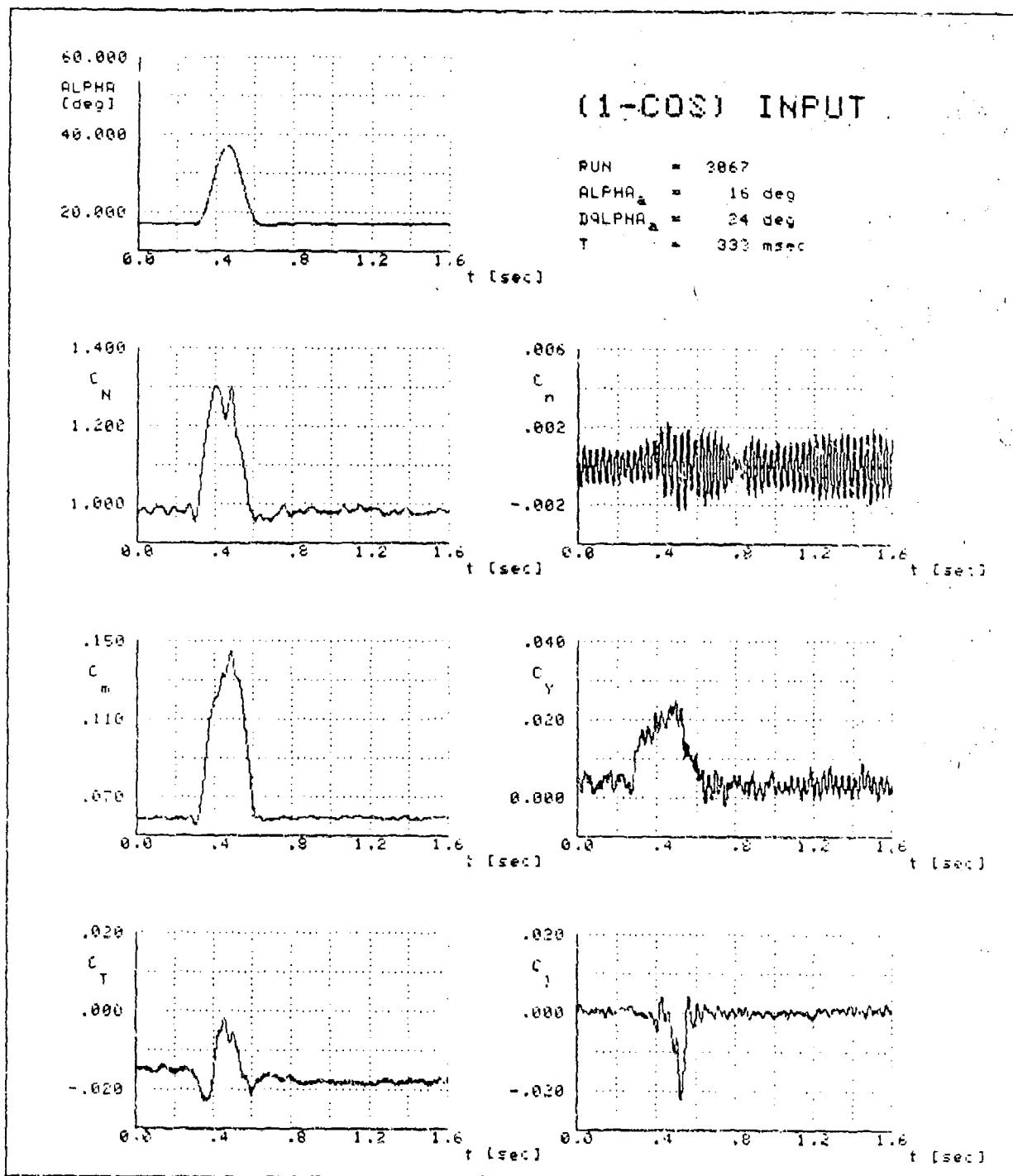


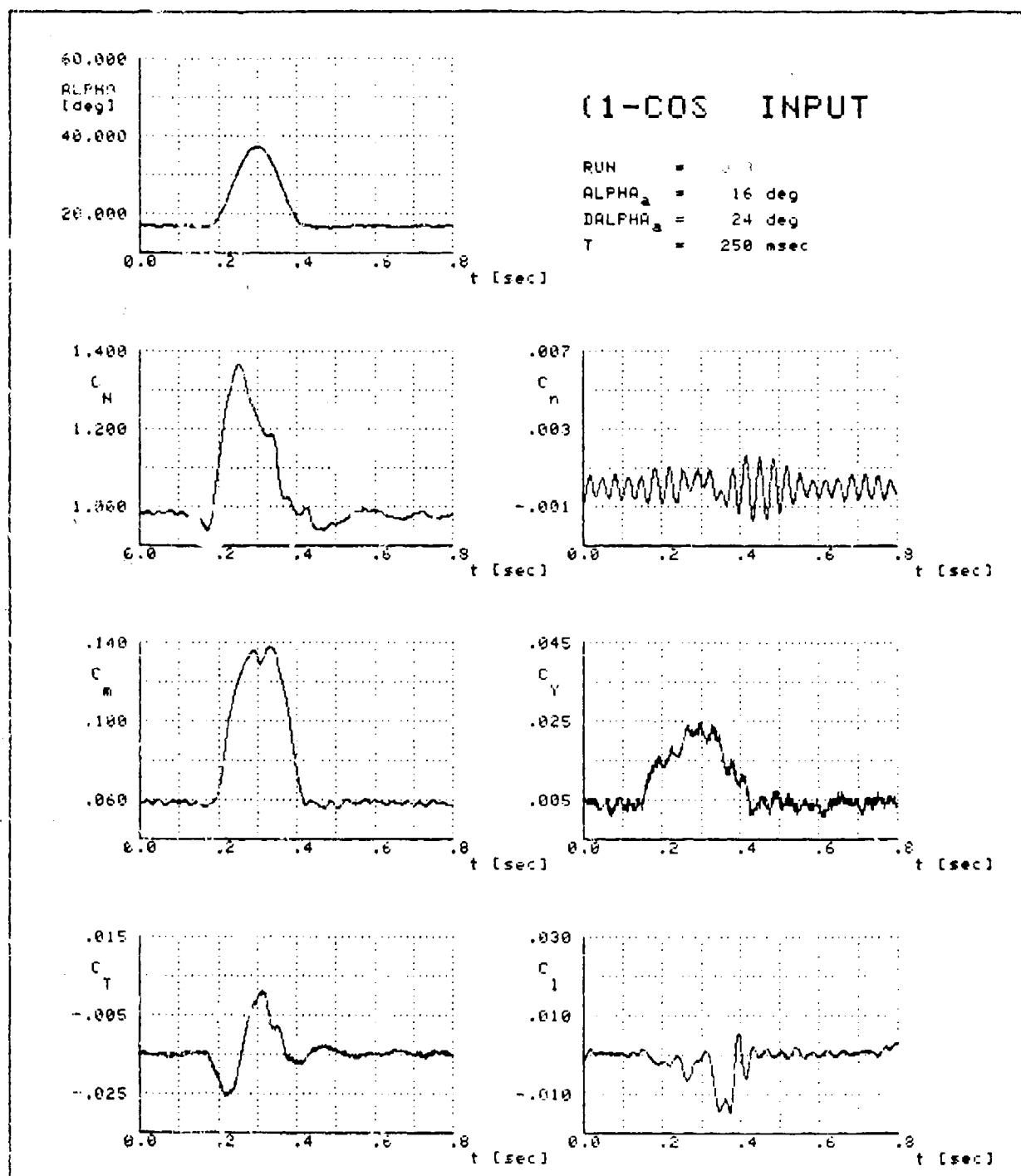


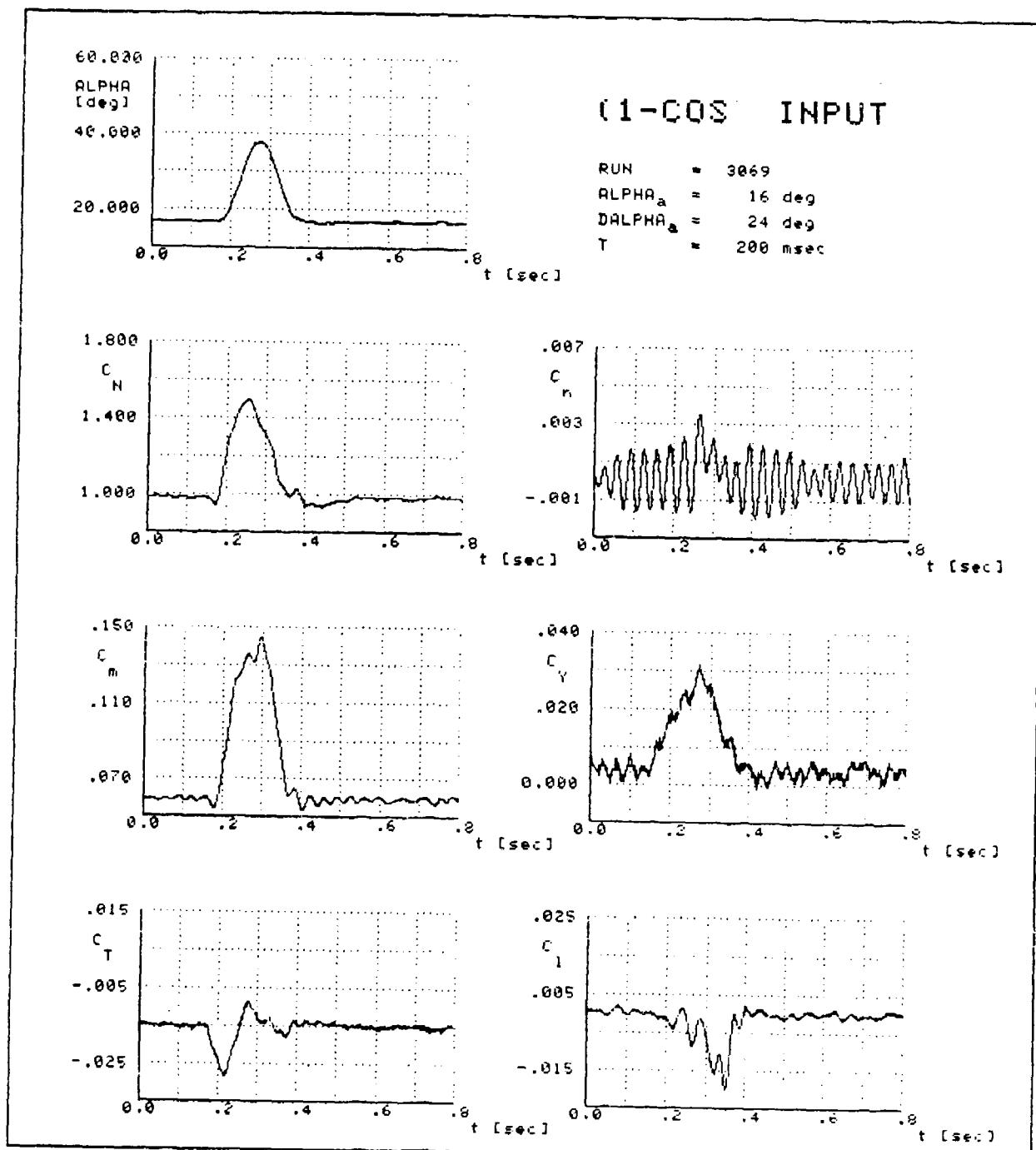


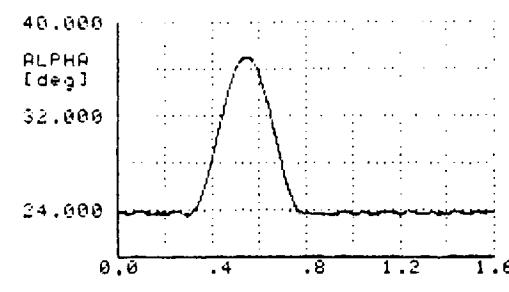






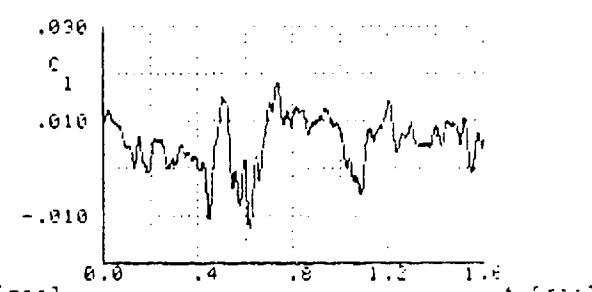
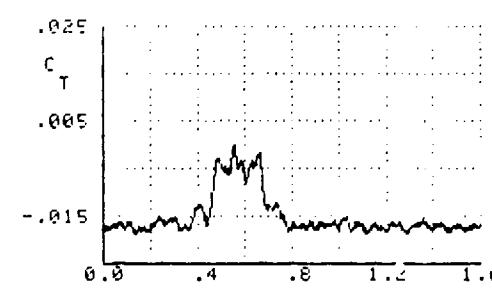
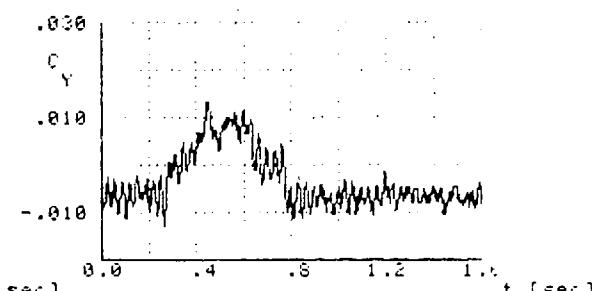
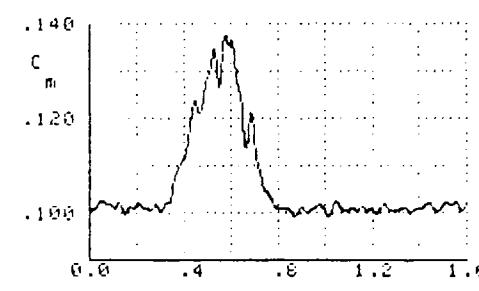
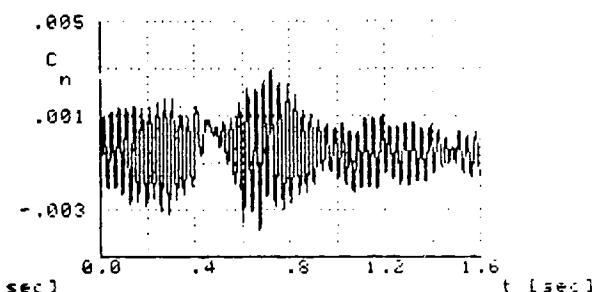
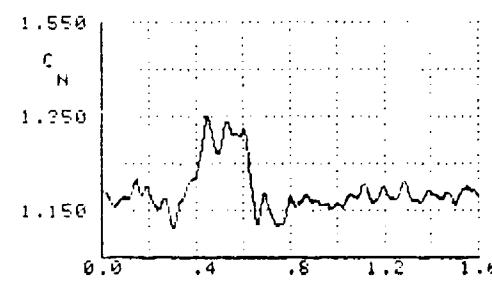


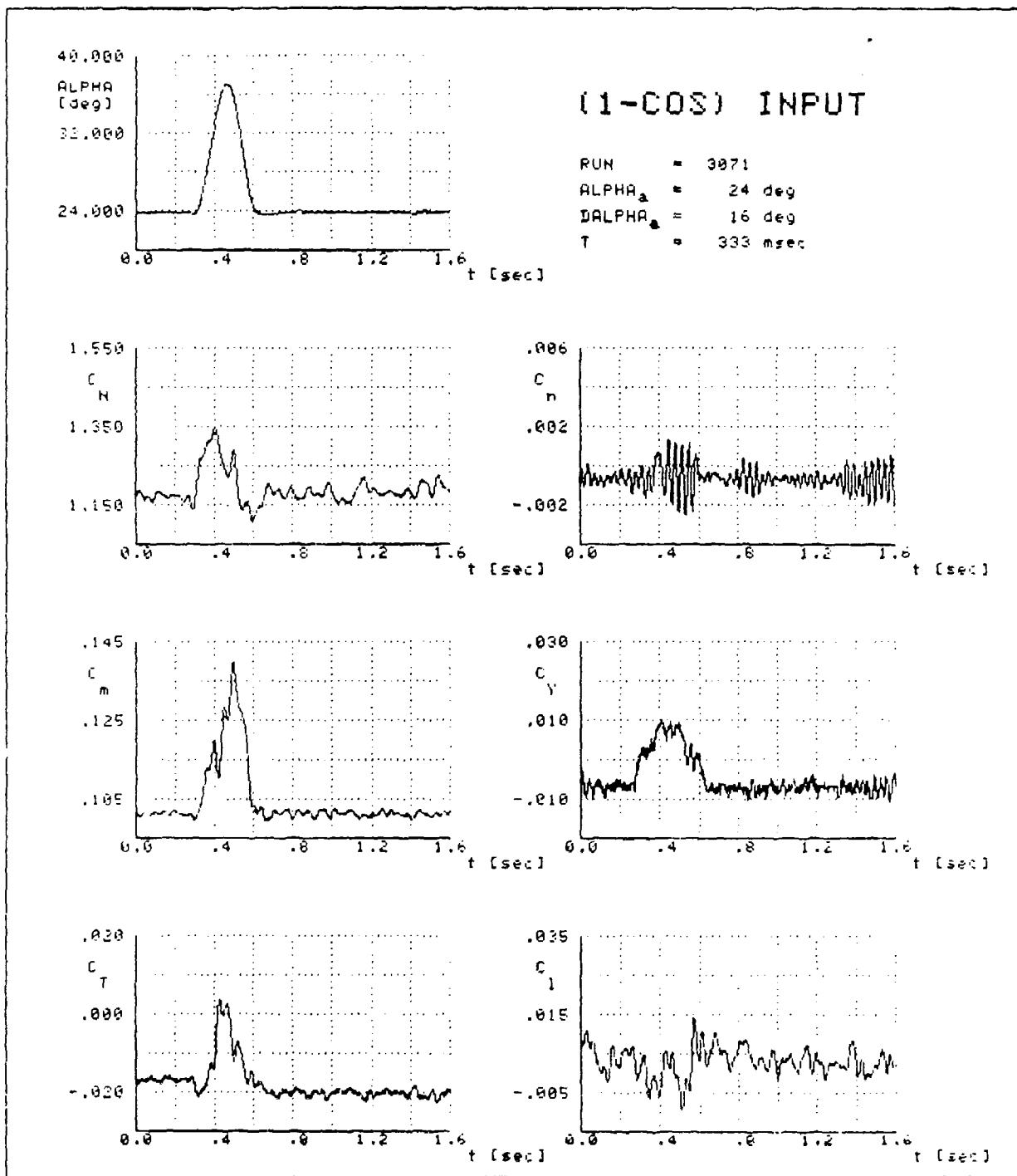


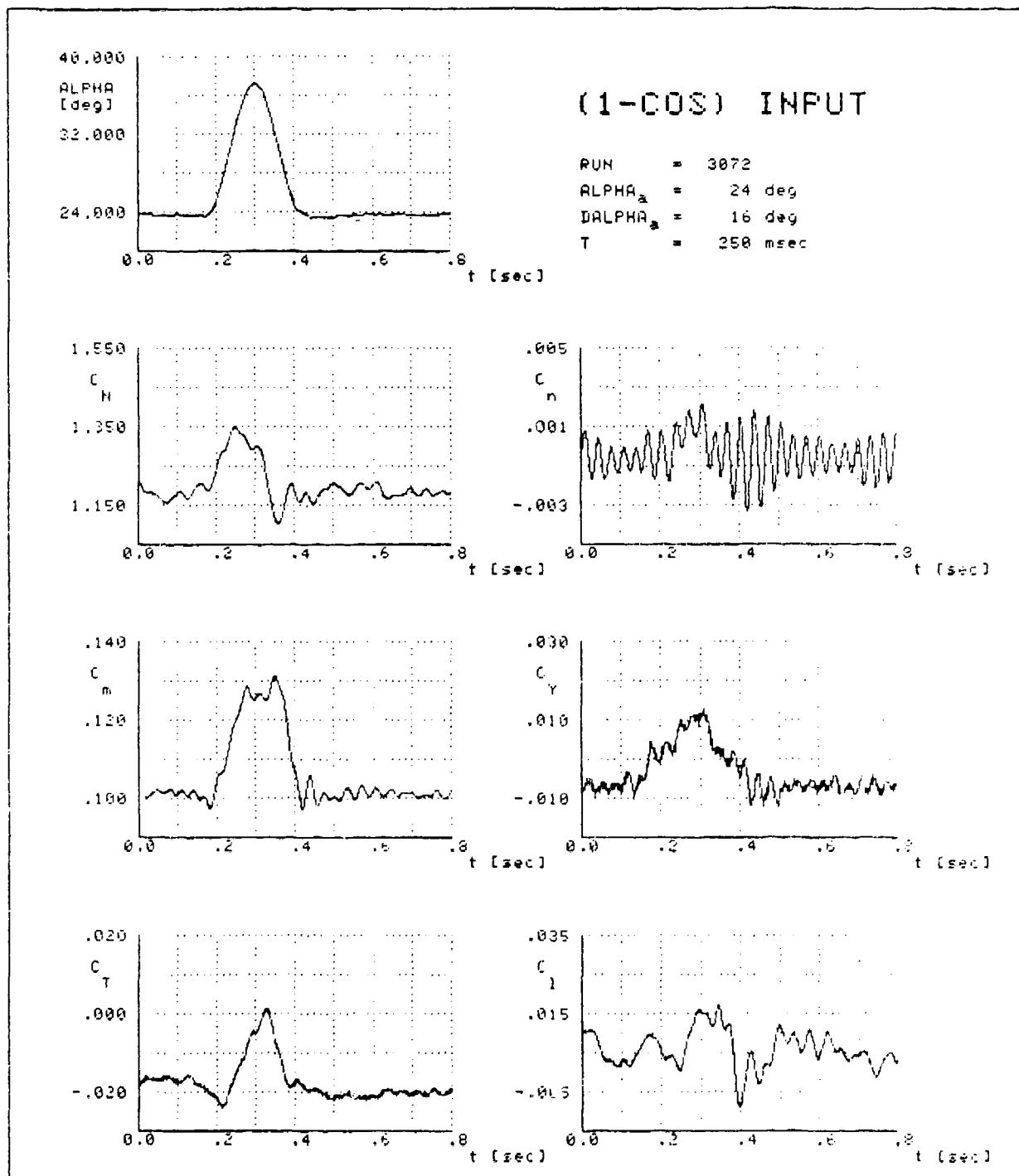


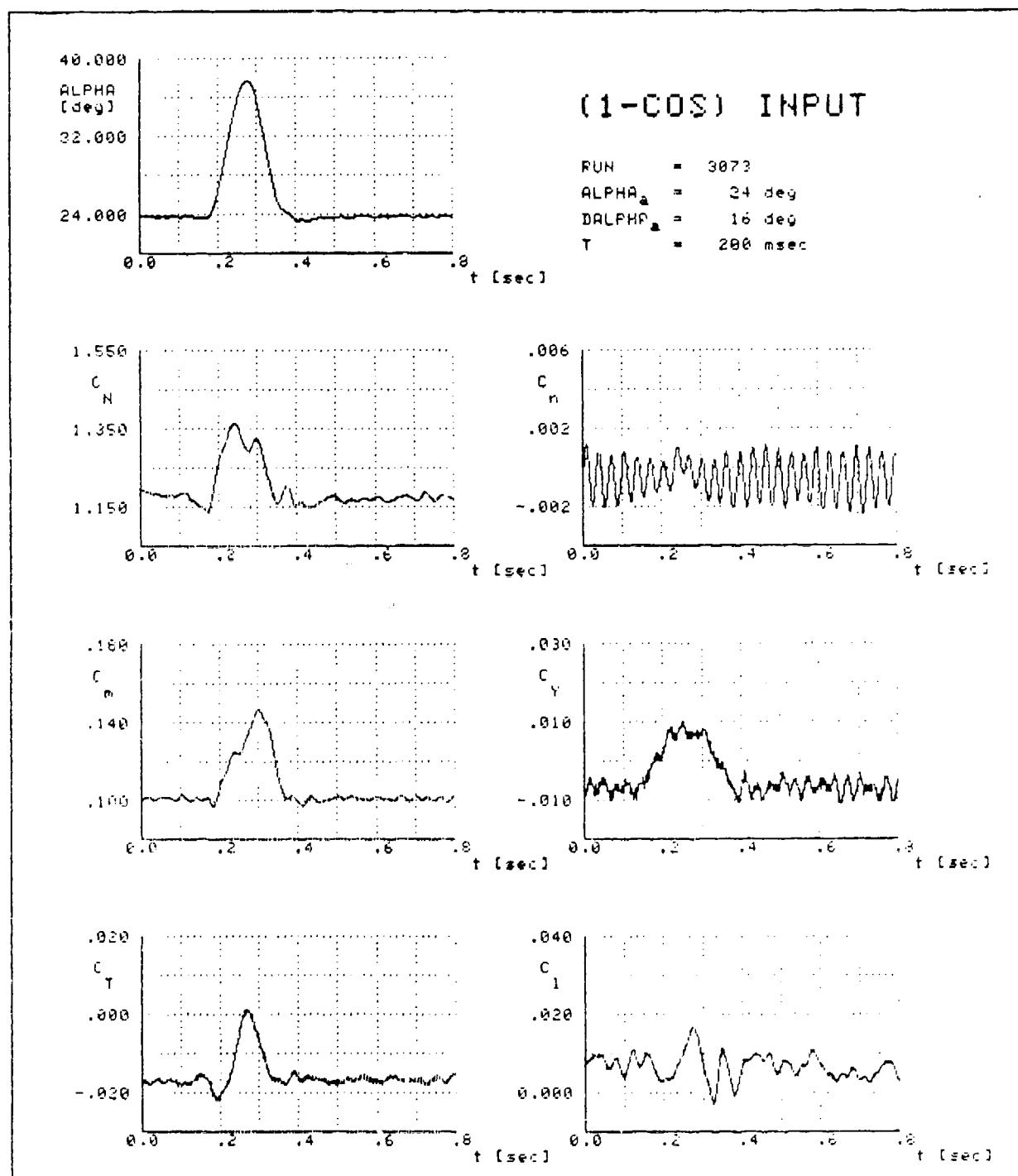
(1-COS) INPUT

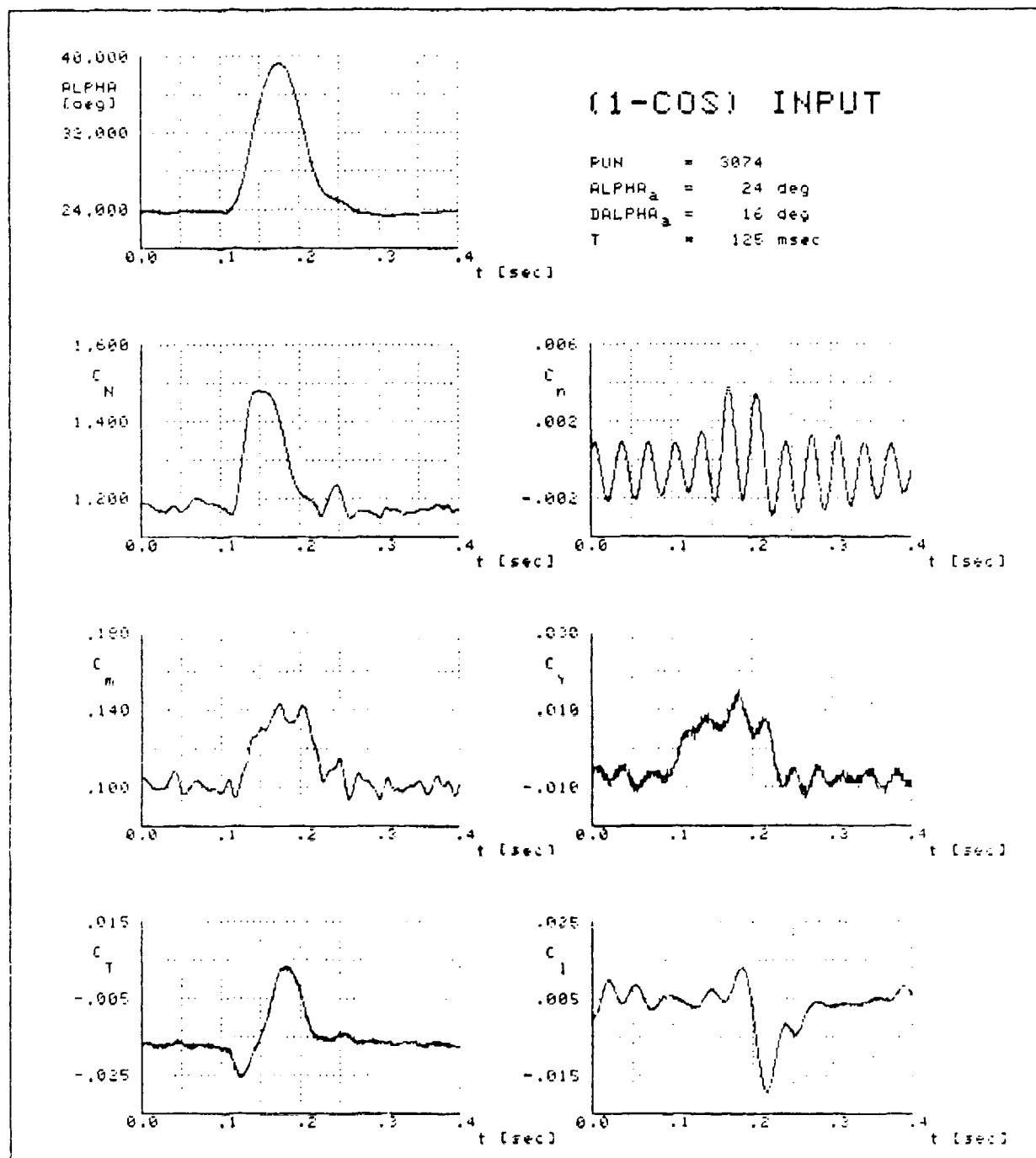
RUN = 3070
ALPHA_a = 24 deg
DALPHA_a = 16 deg
T = 500 msec

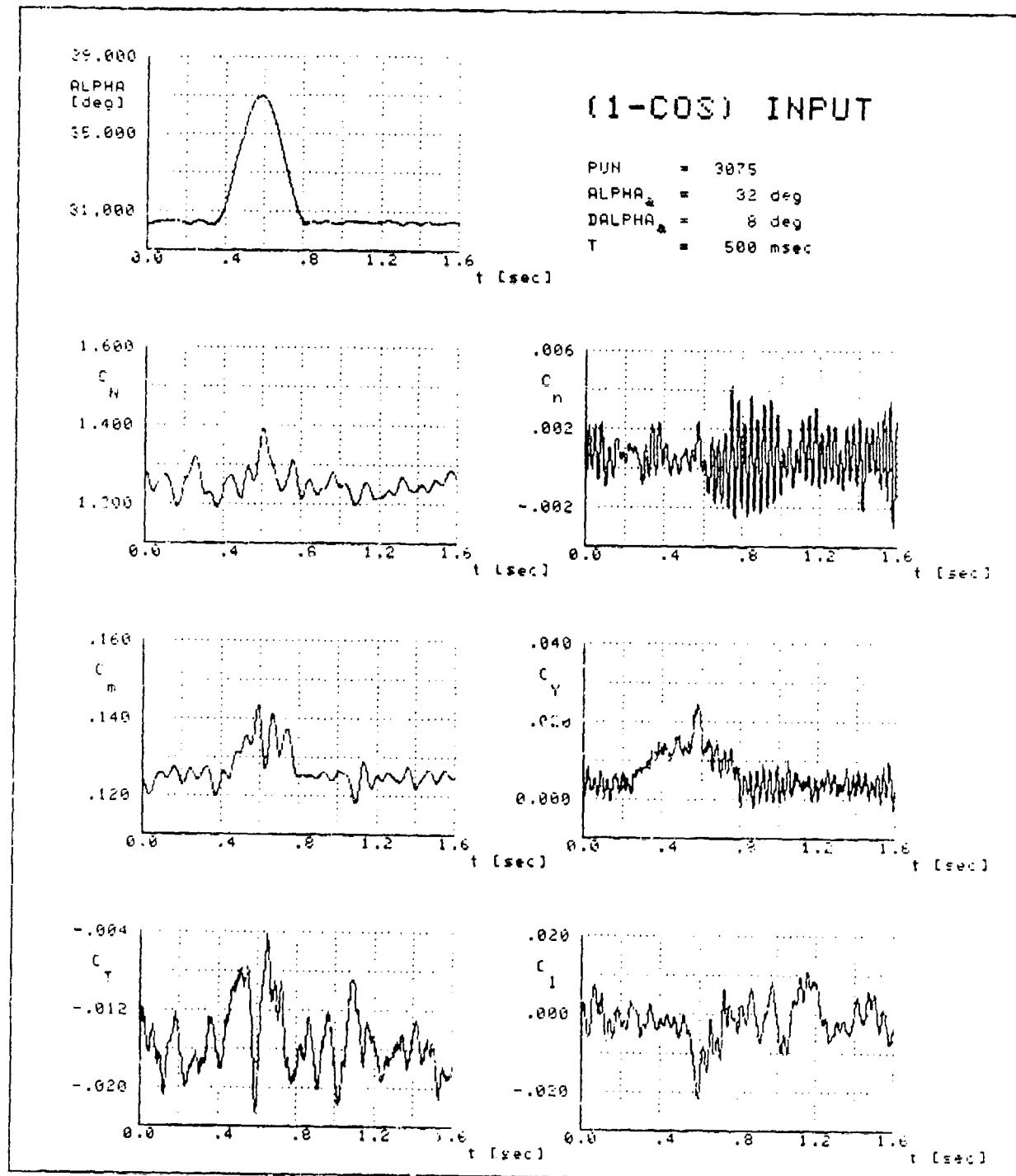


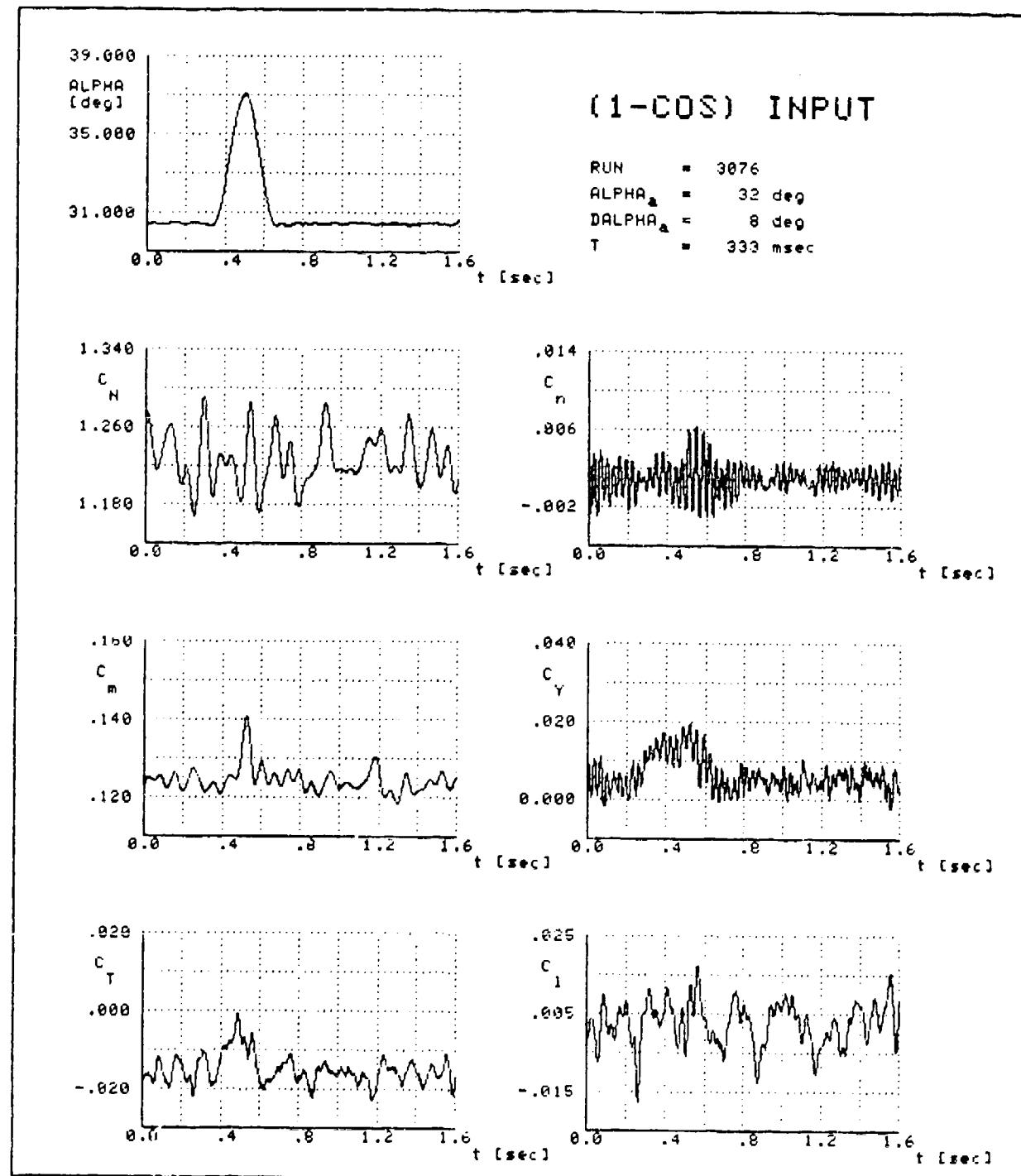


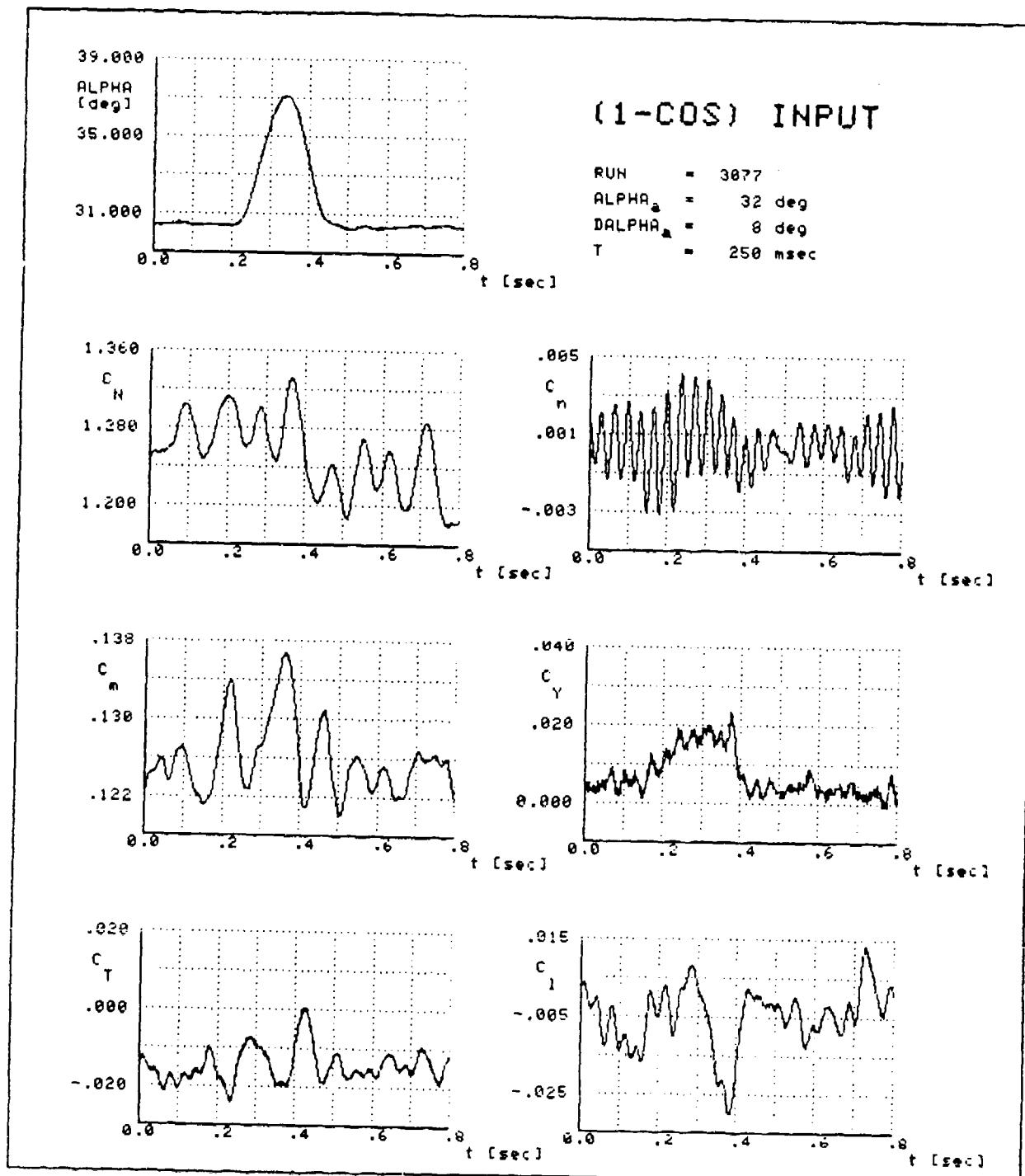


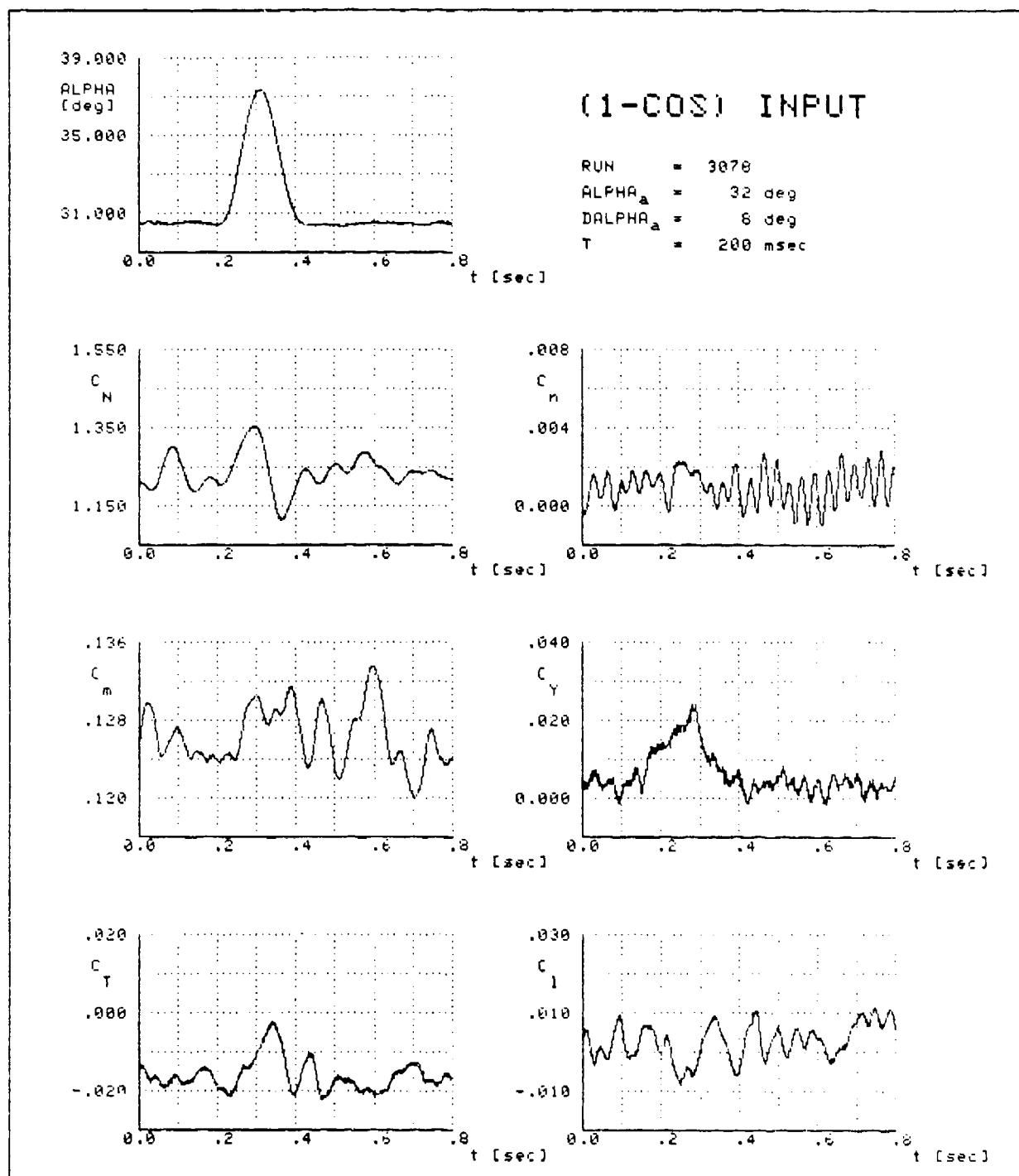


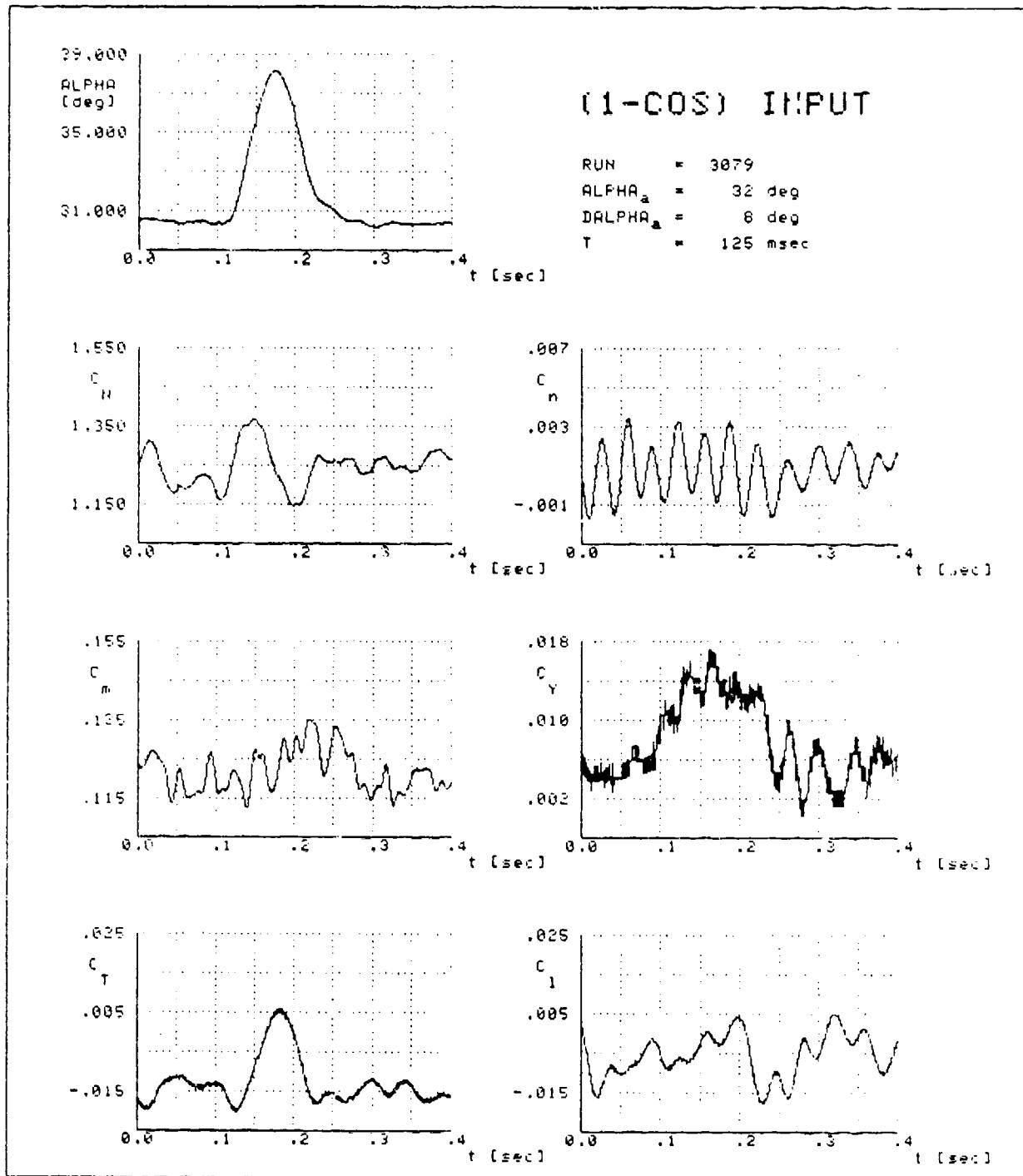


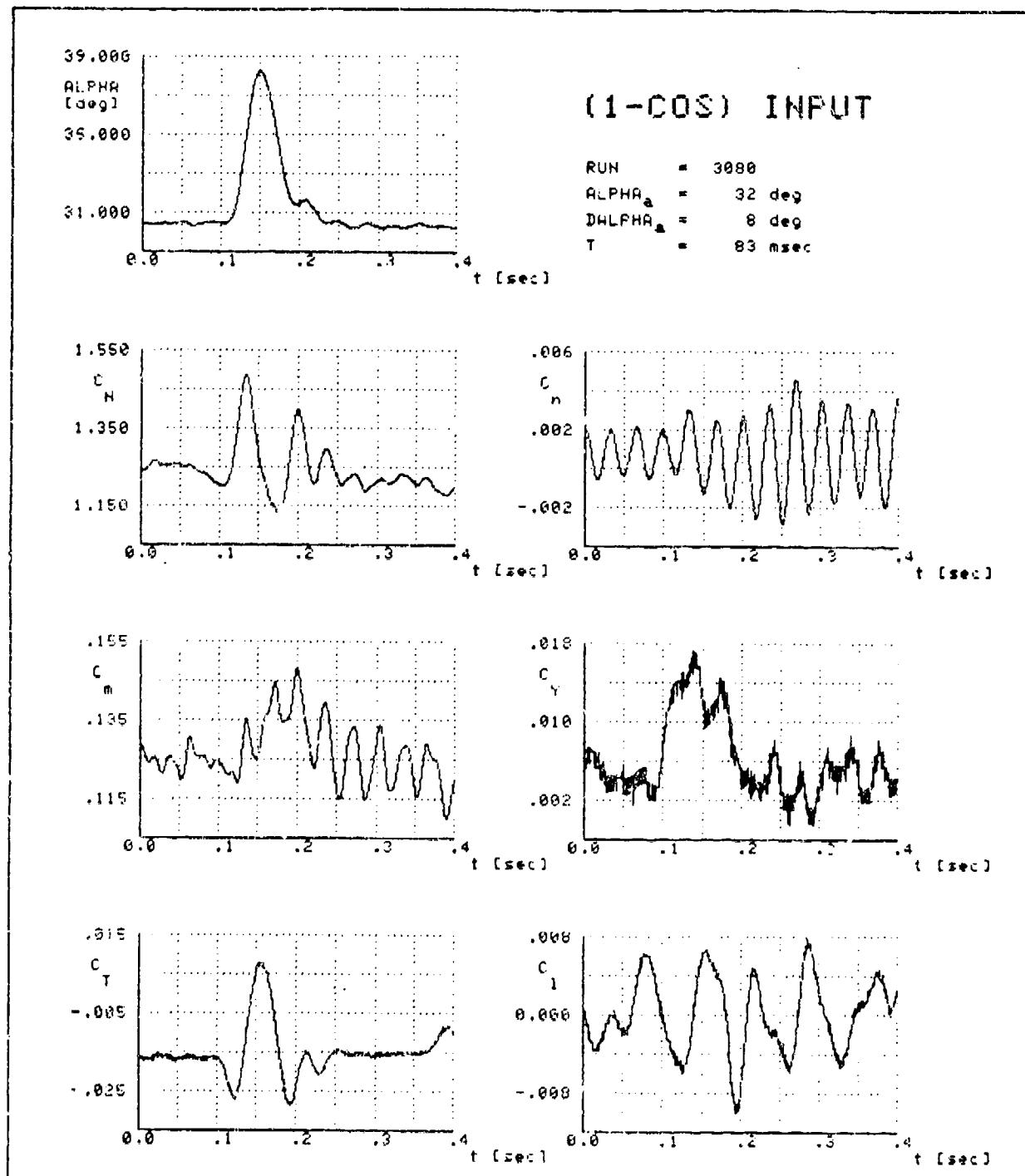


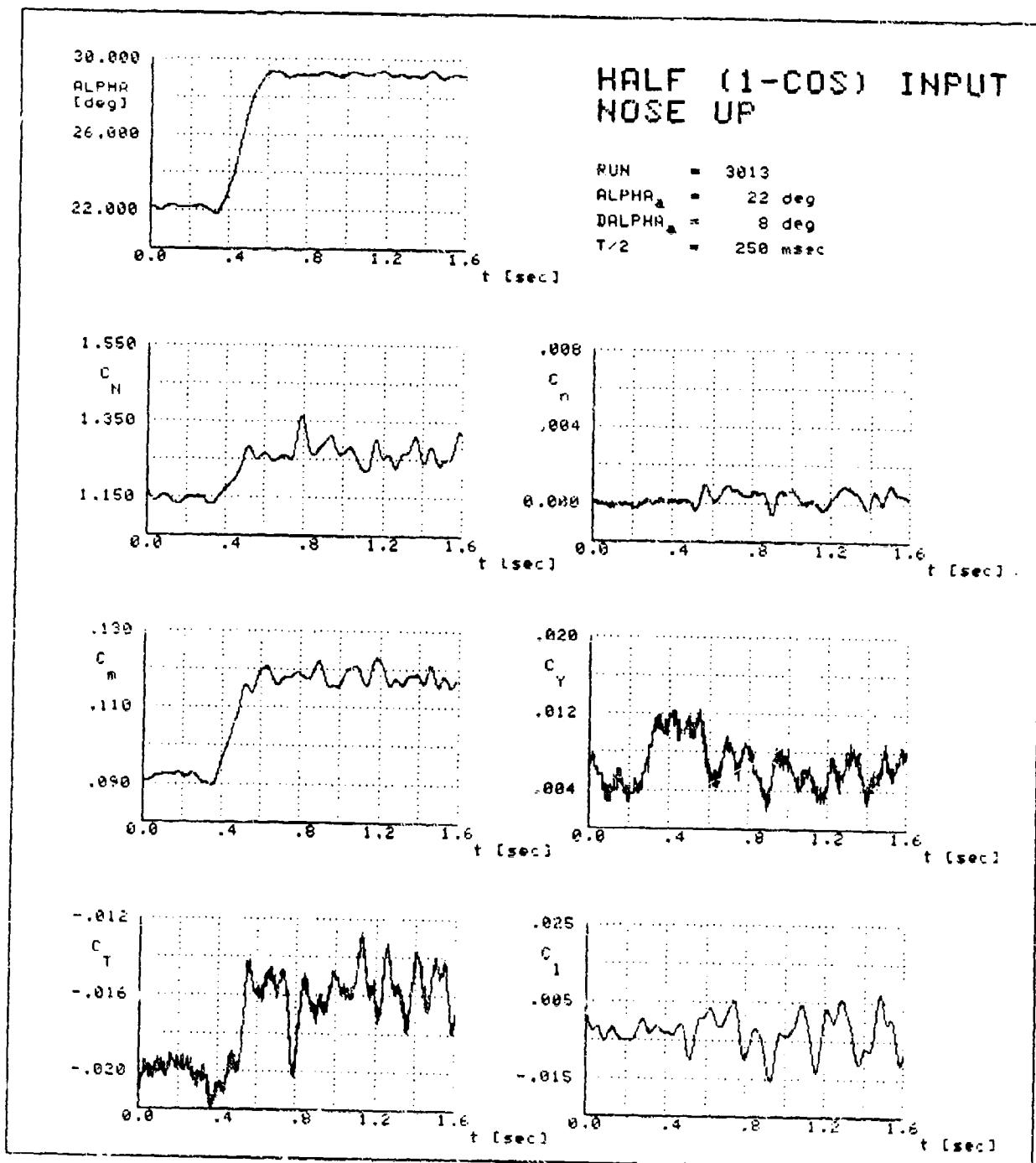


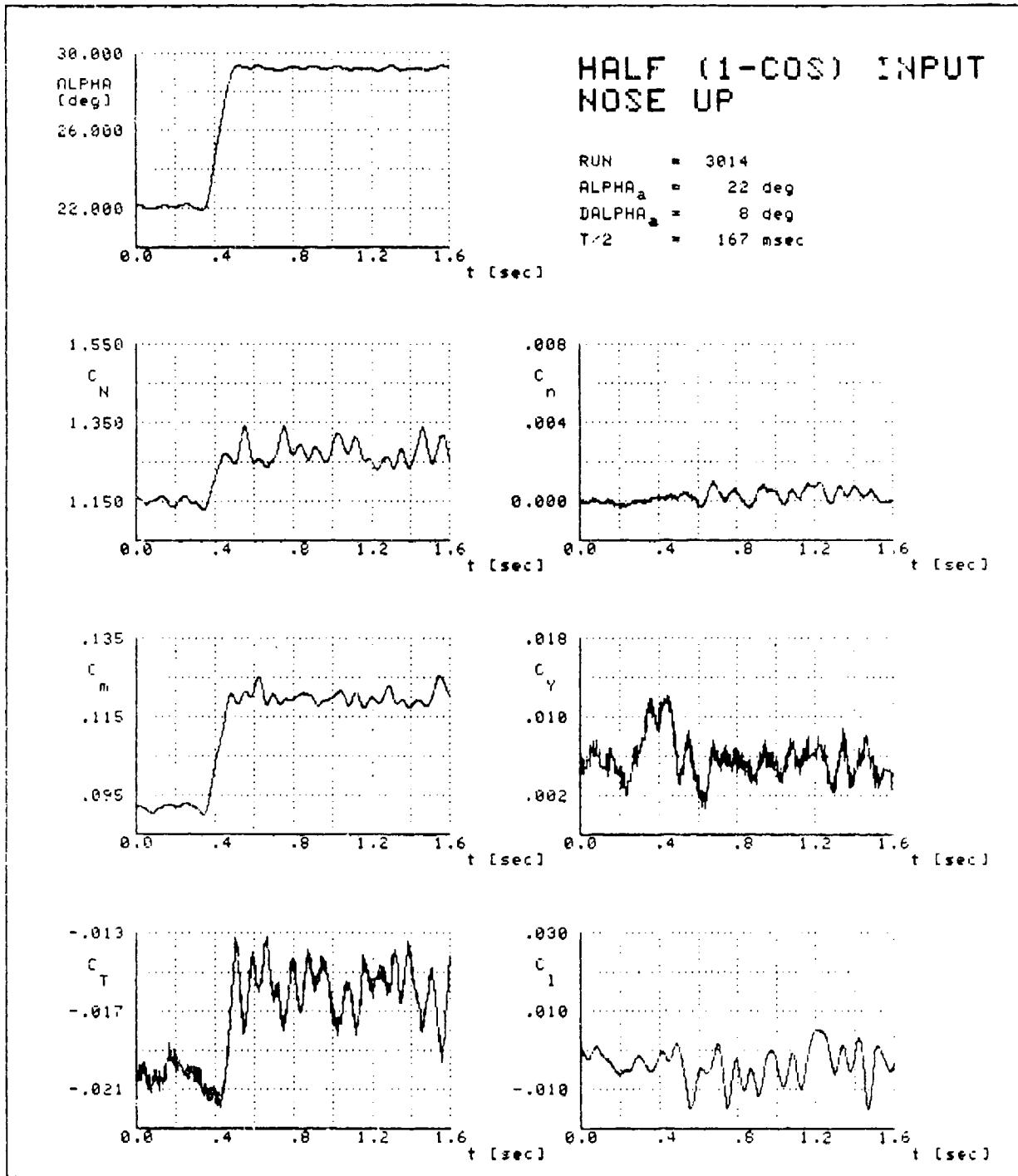


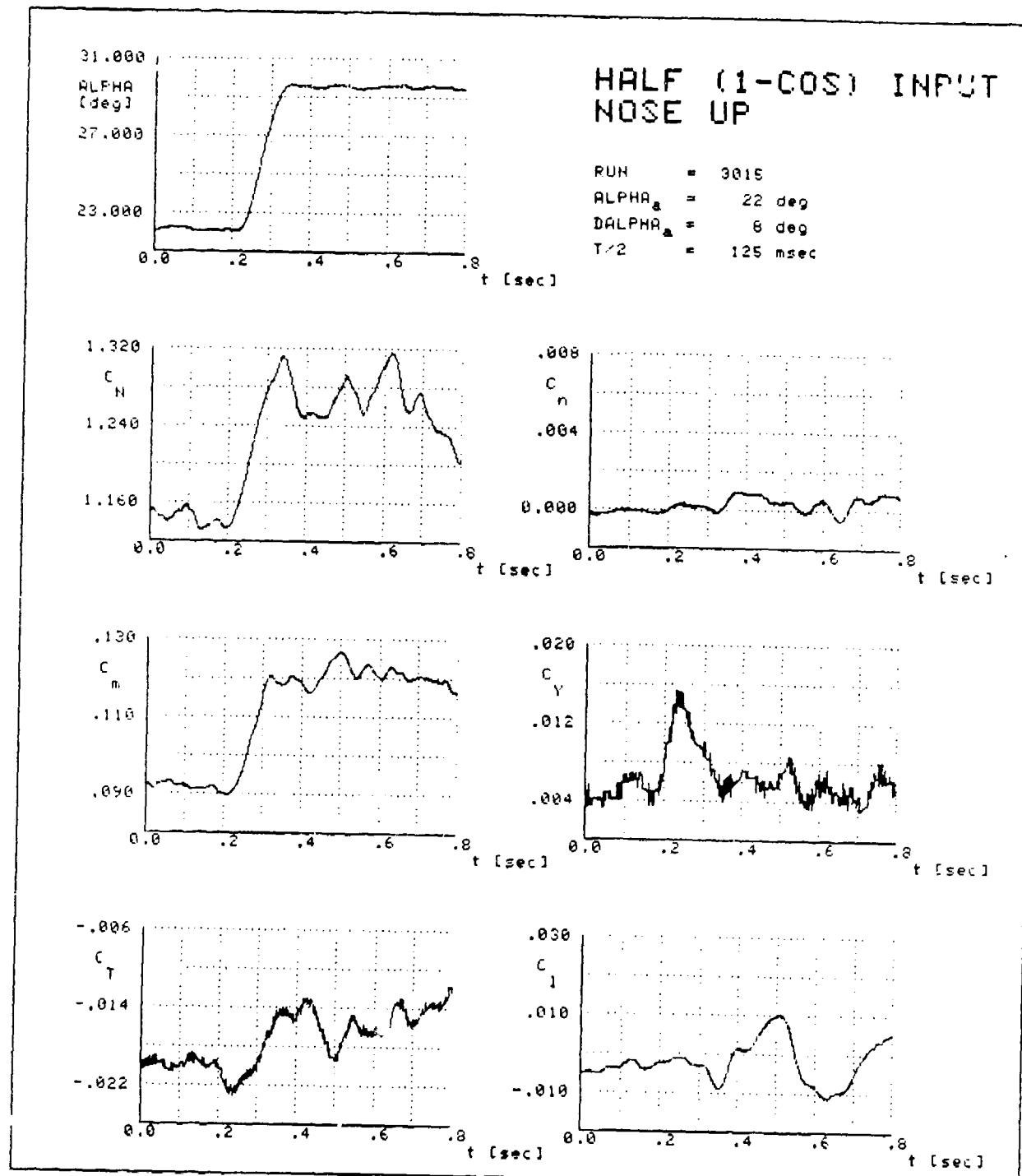


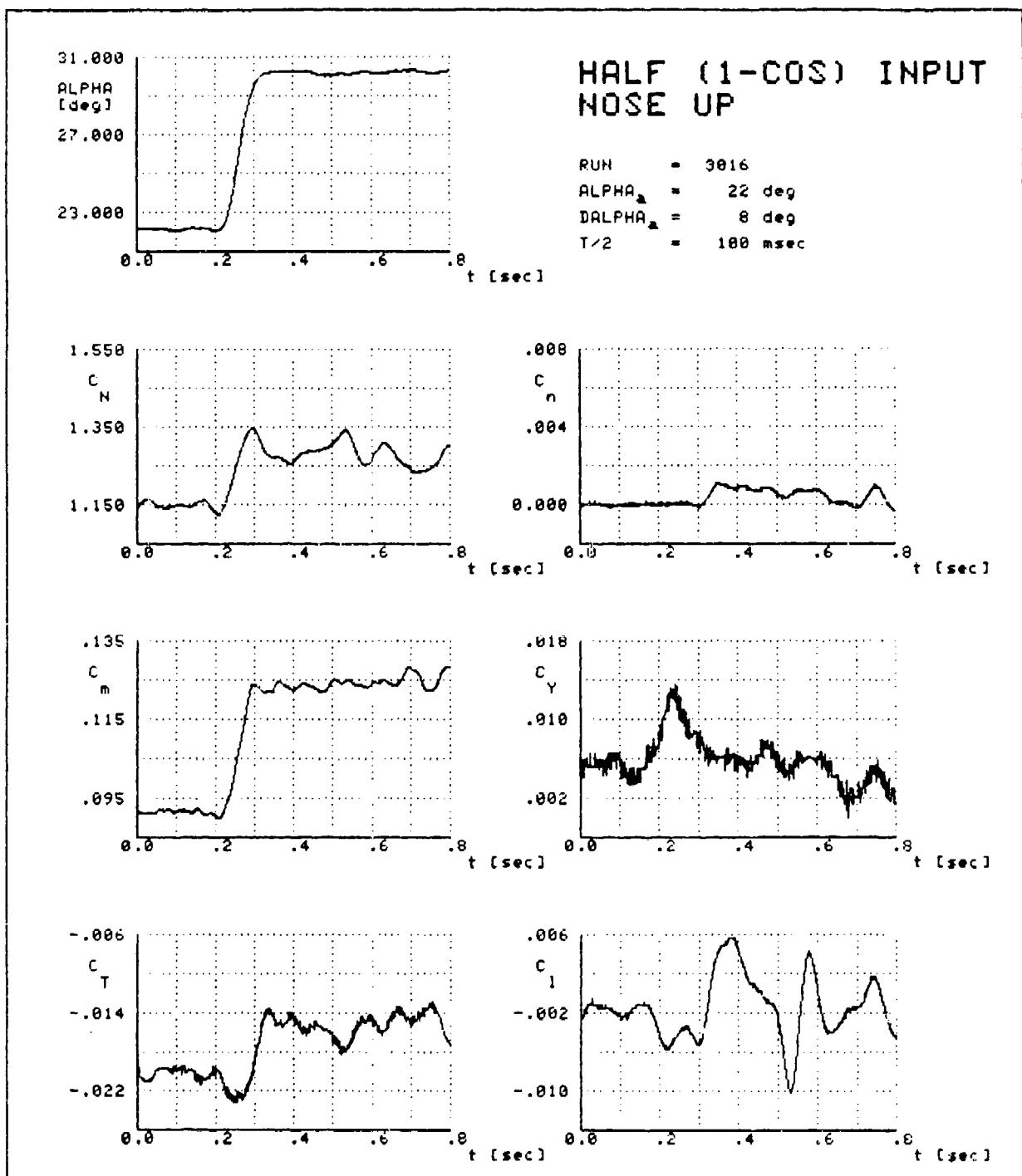


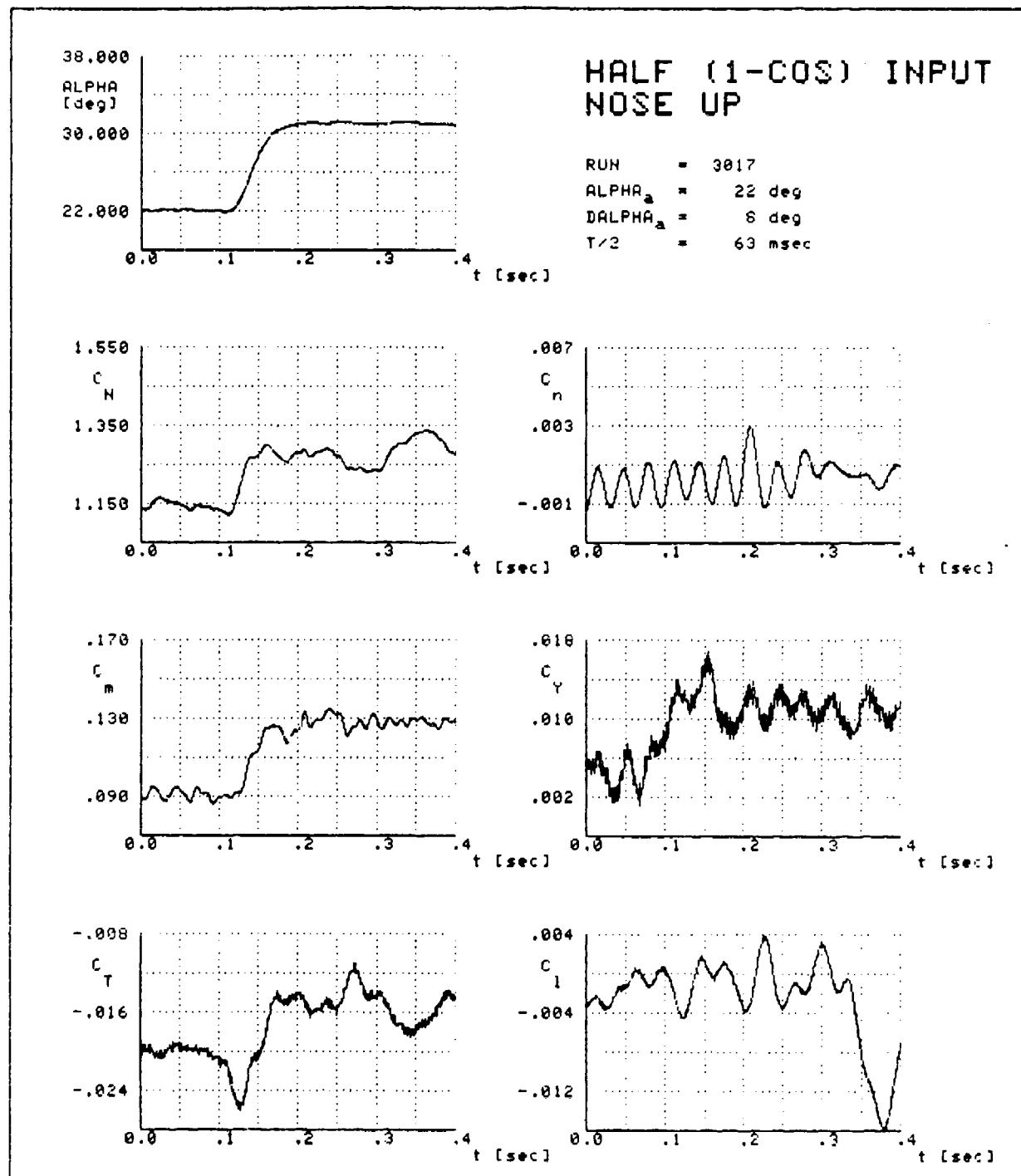


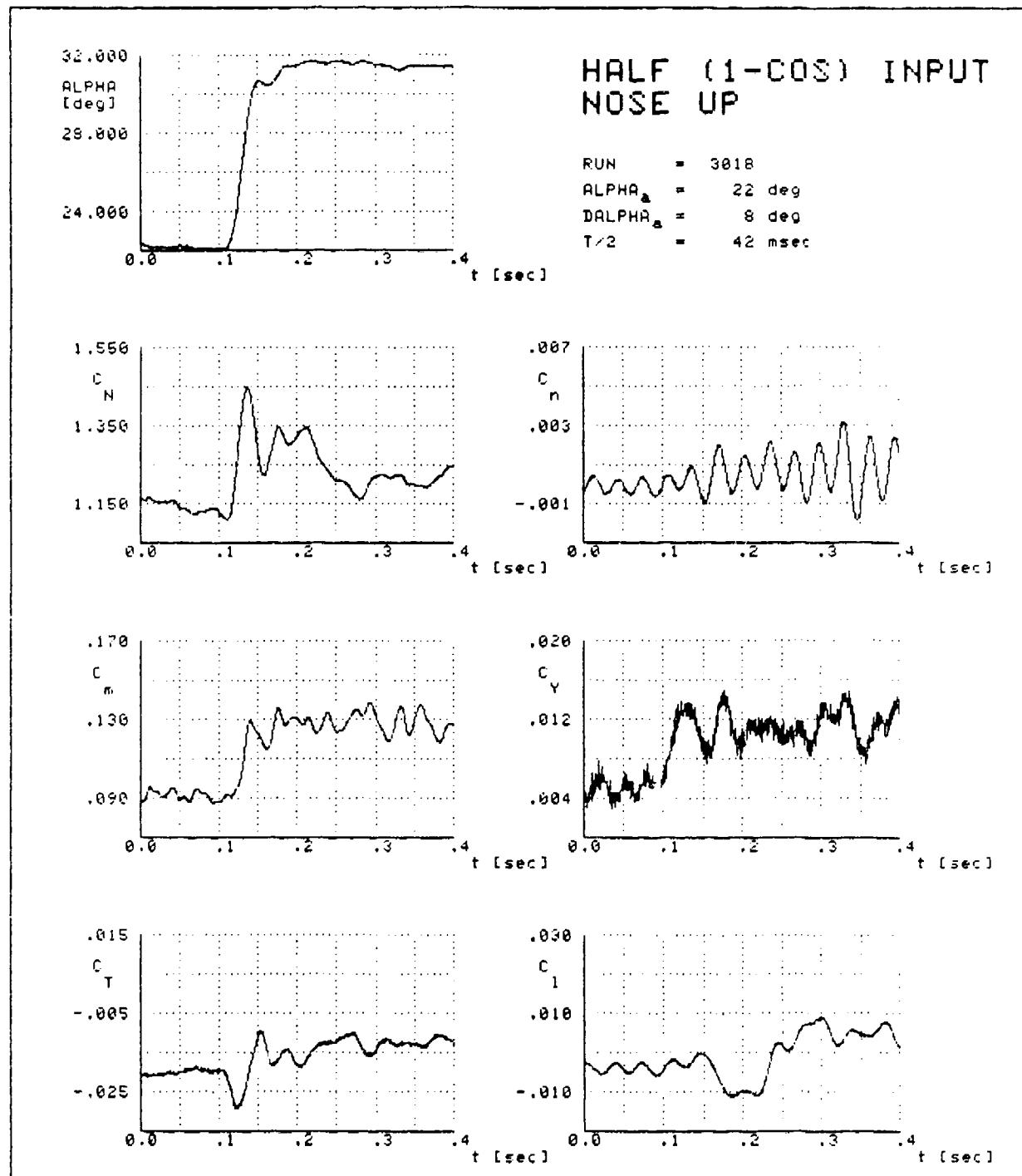


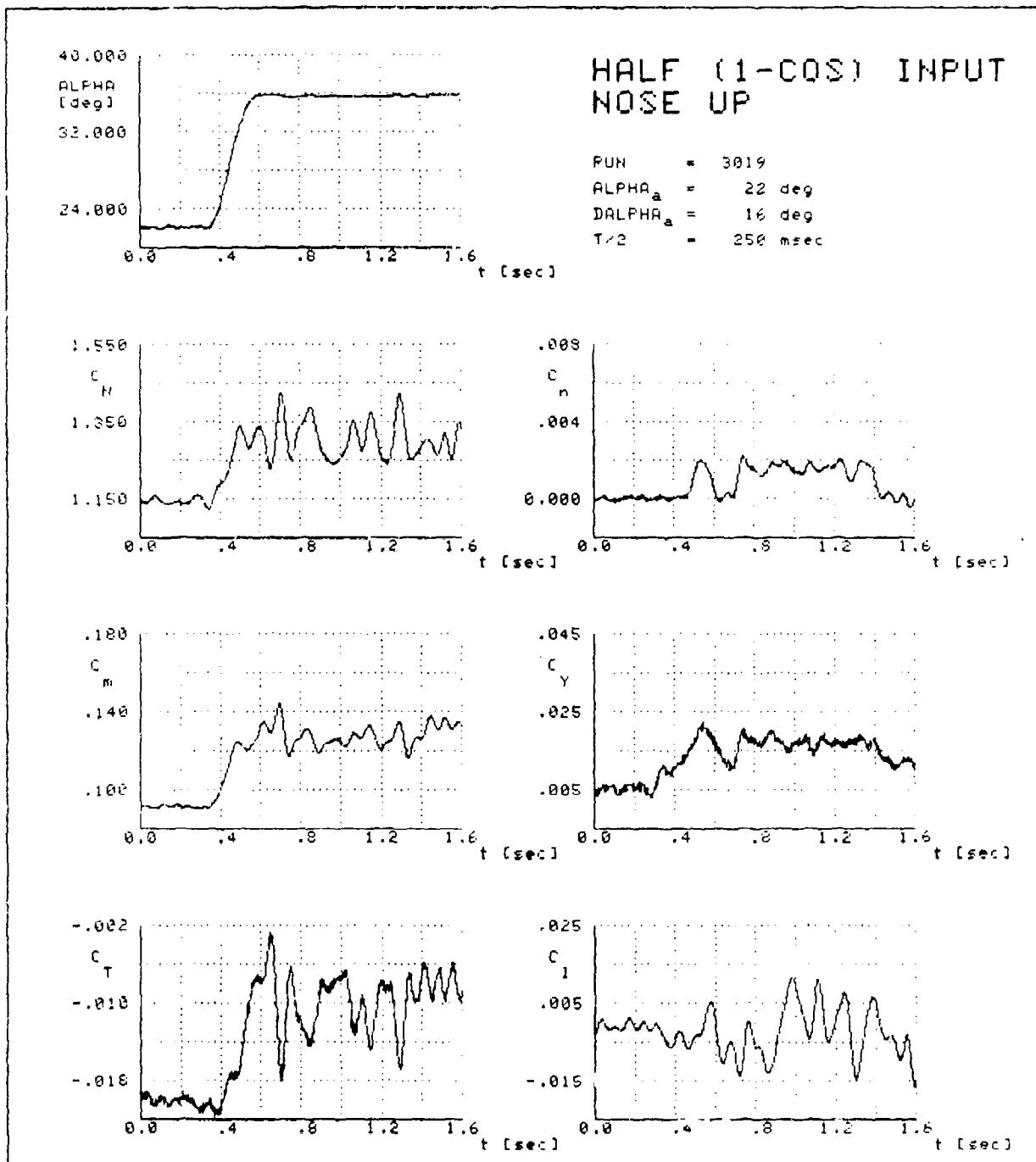


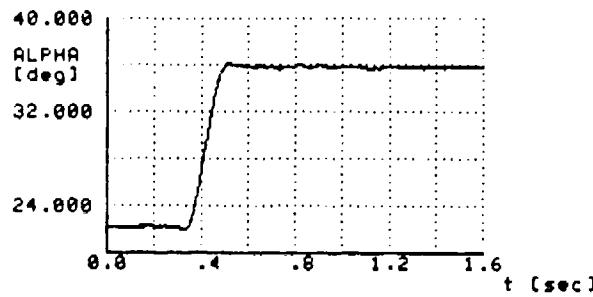






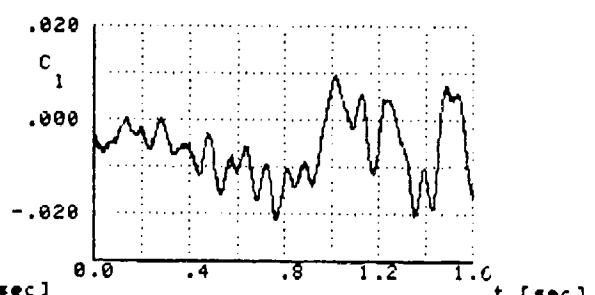
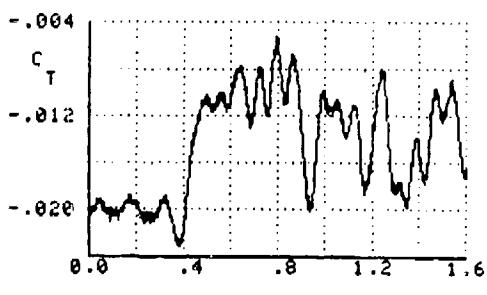
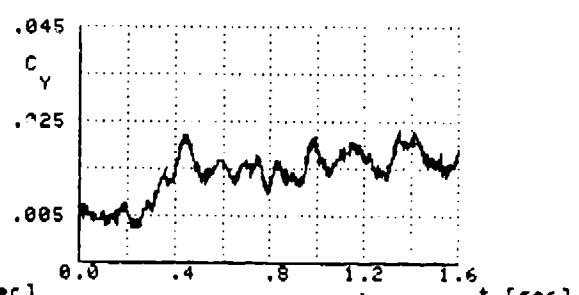
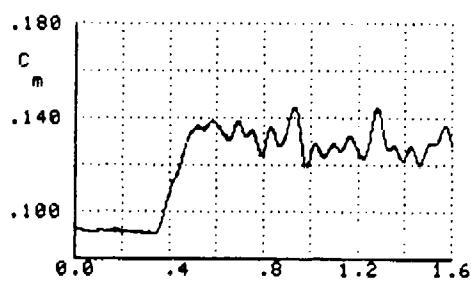
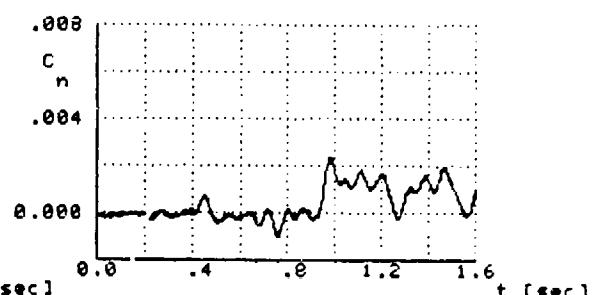
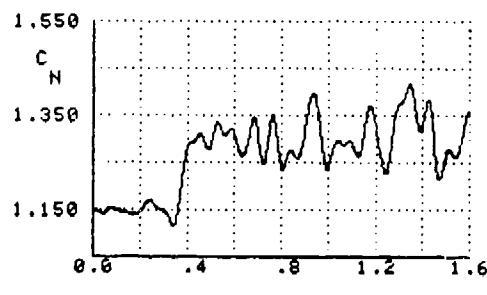


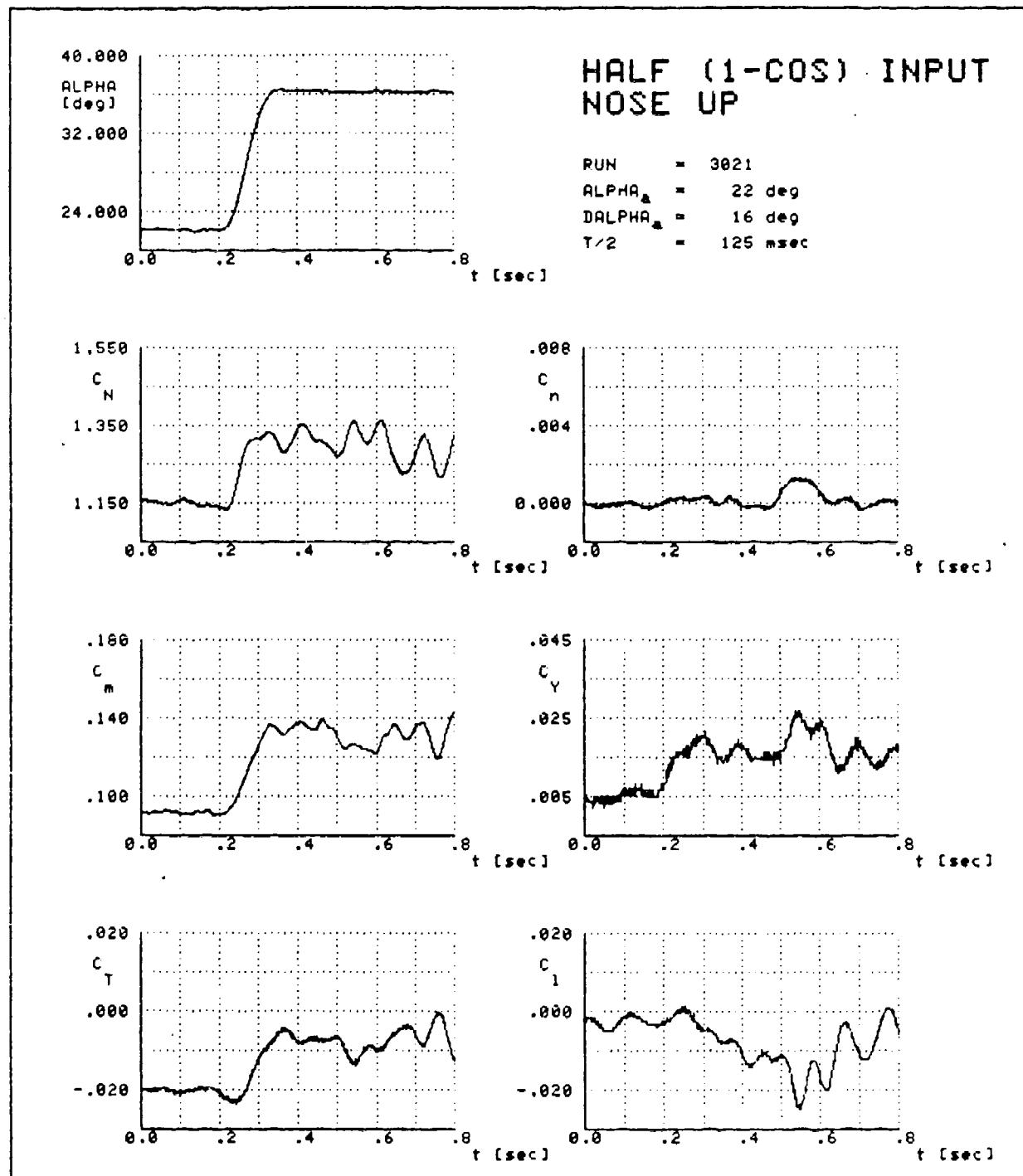


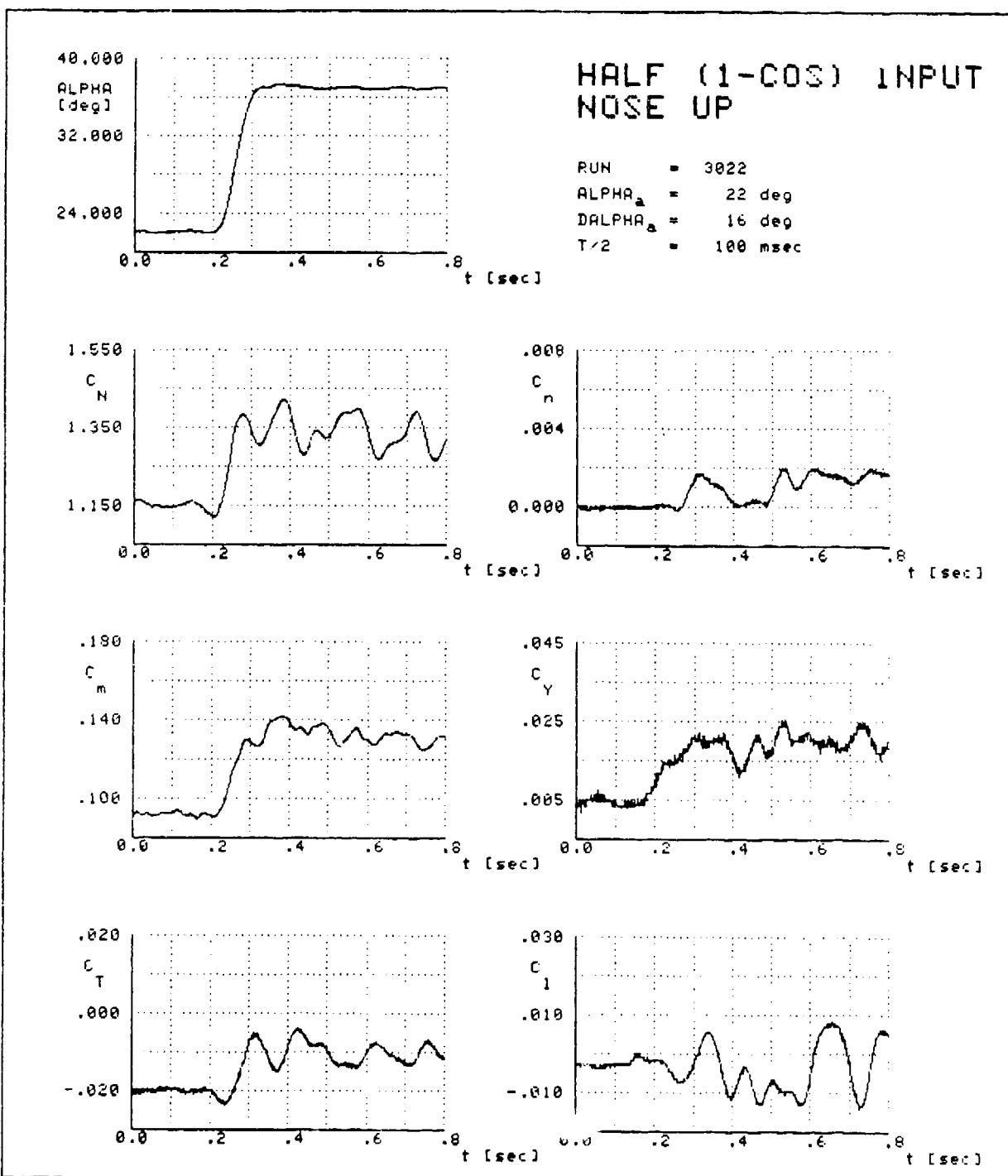


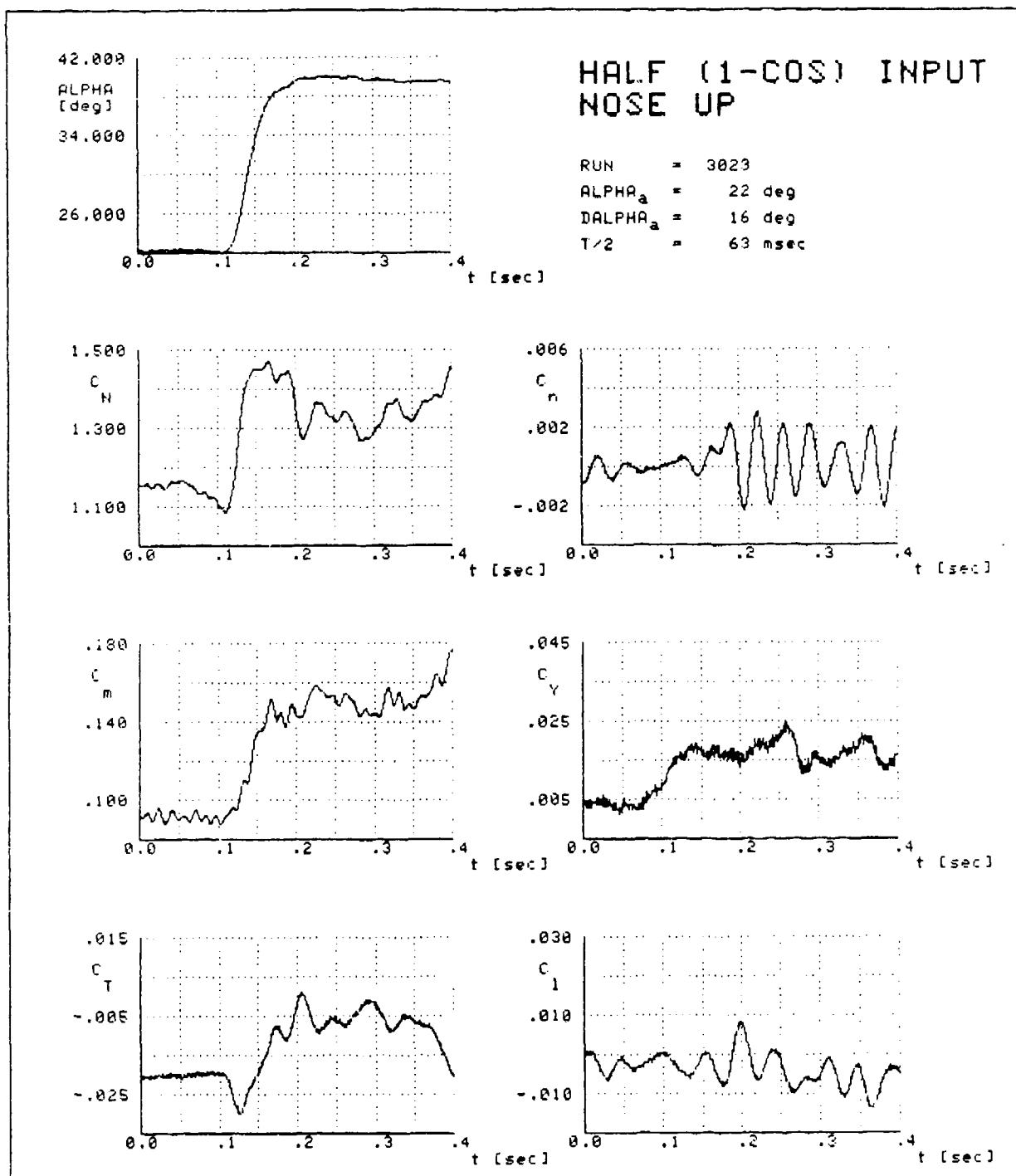
HALF (1-COS) INPUT NOSE UP

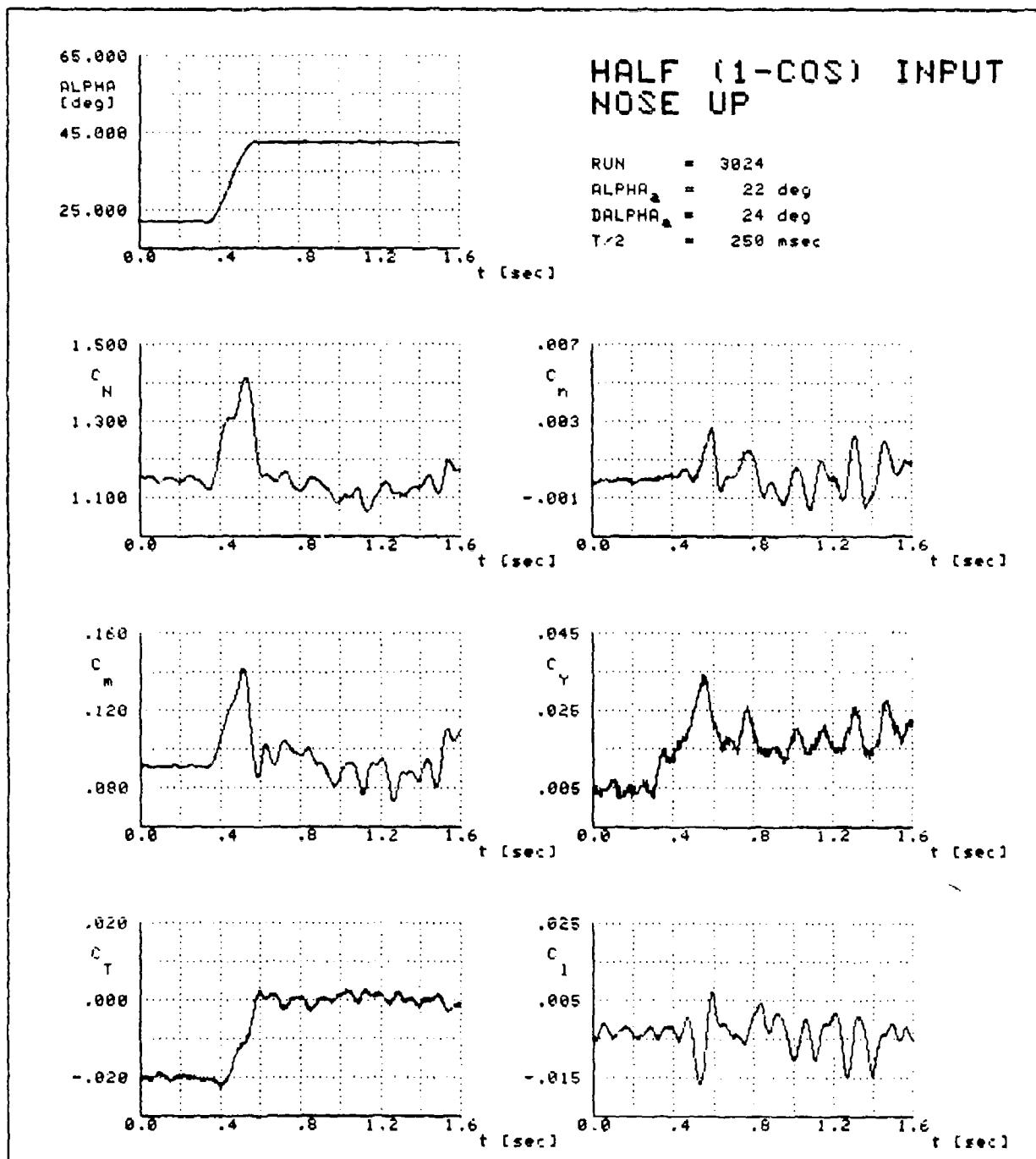
RUN = 3020
 ALPHA_a = 22 deg
 DALPHA_a = 16 deg
 $T/2$ = 167 msec

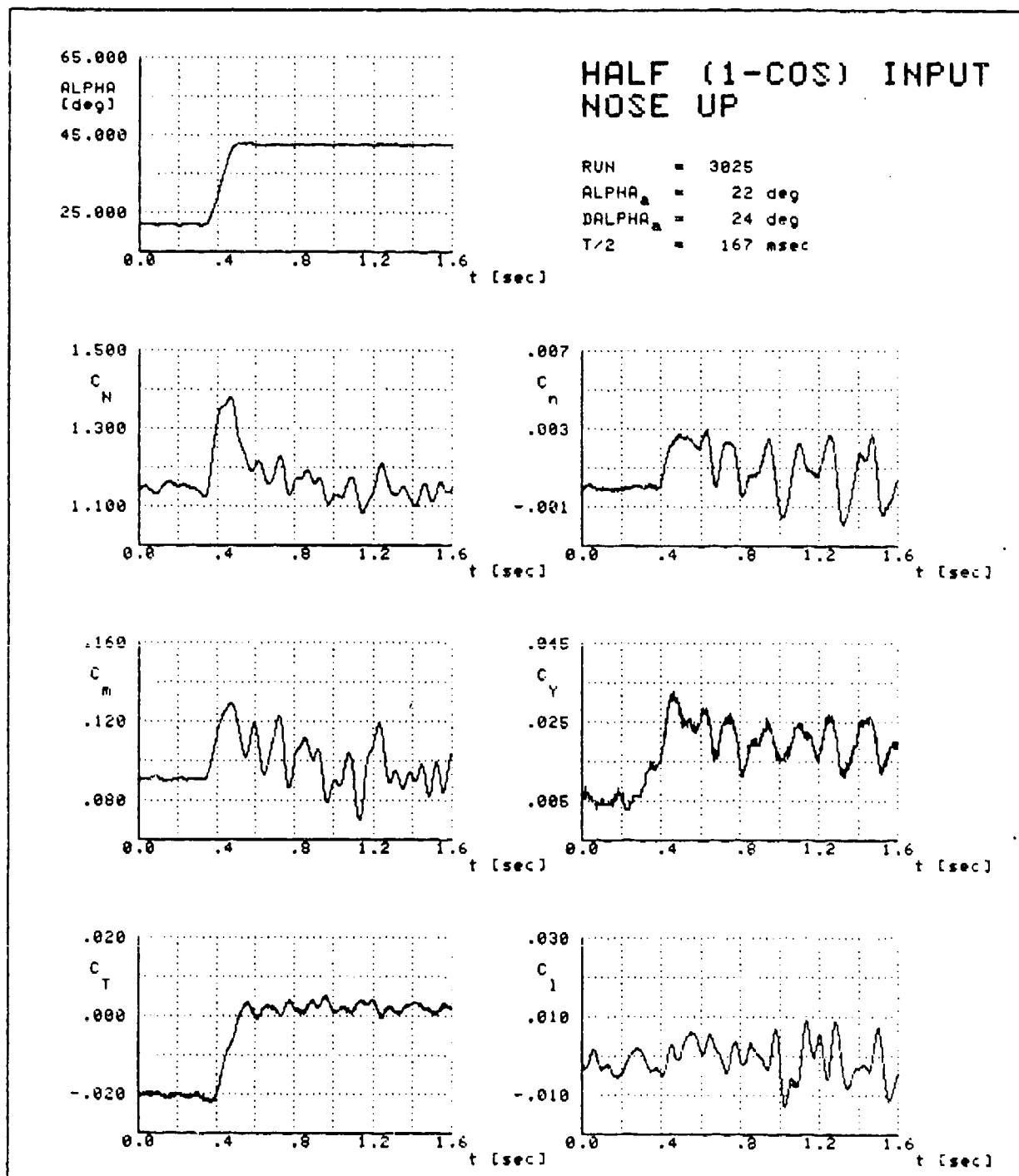


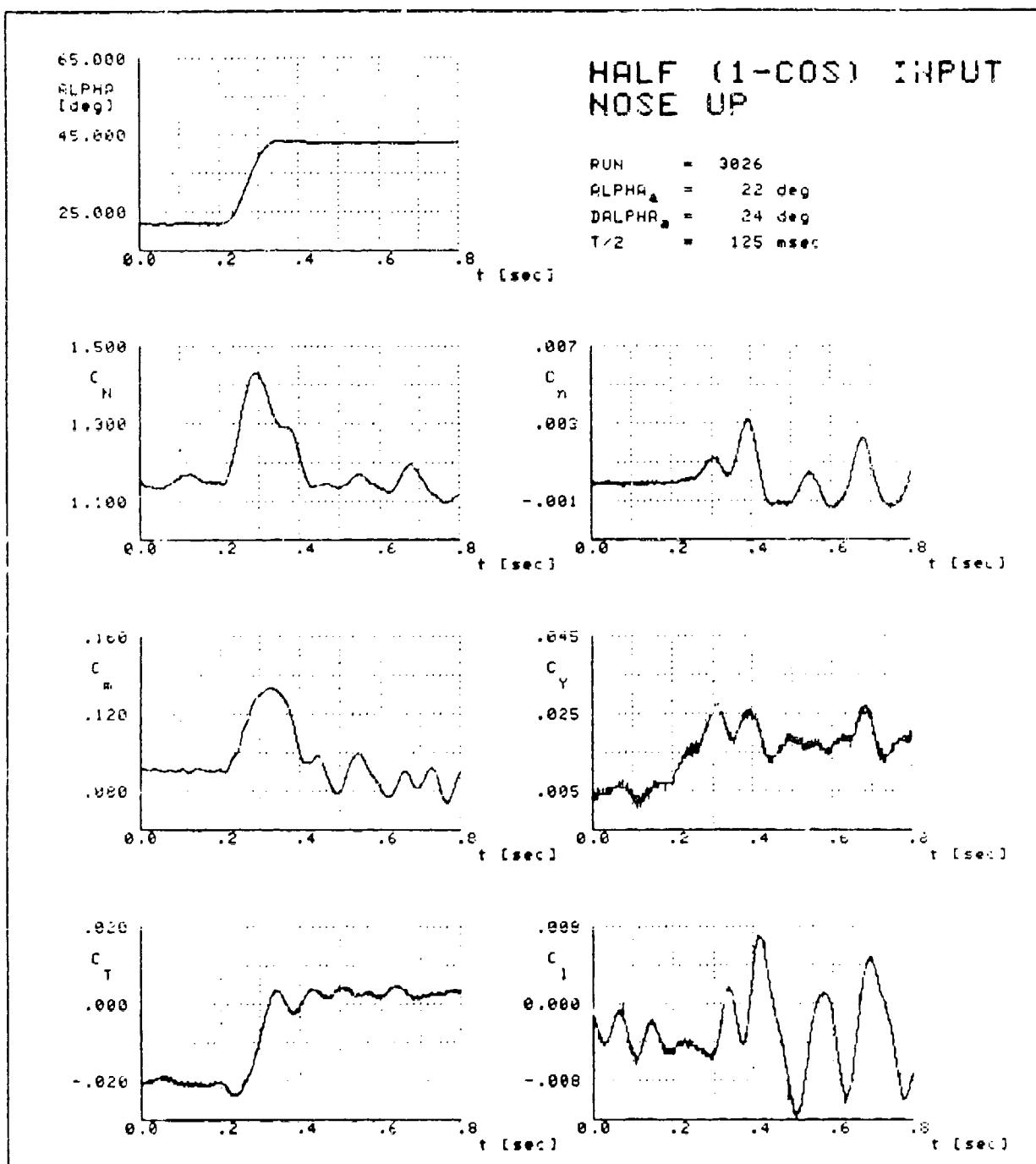


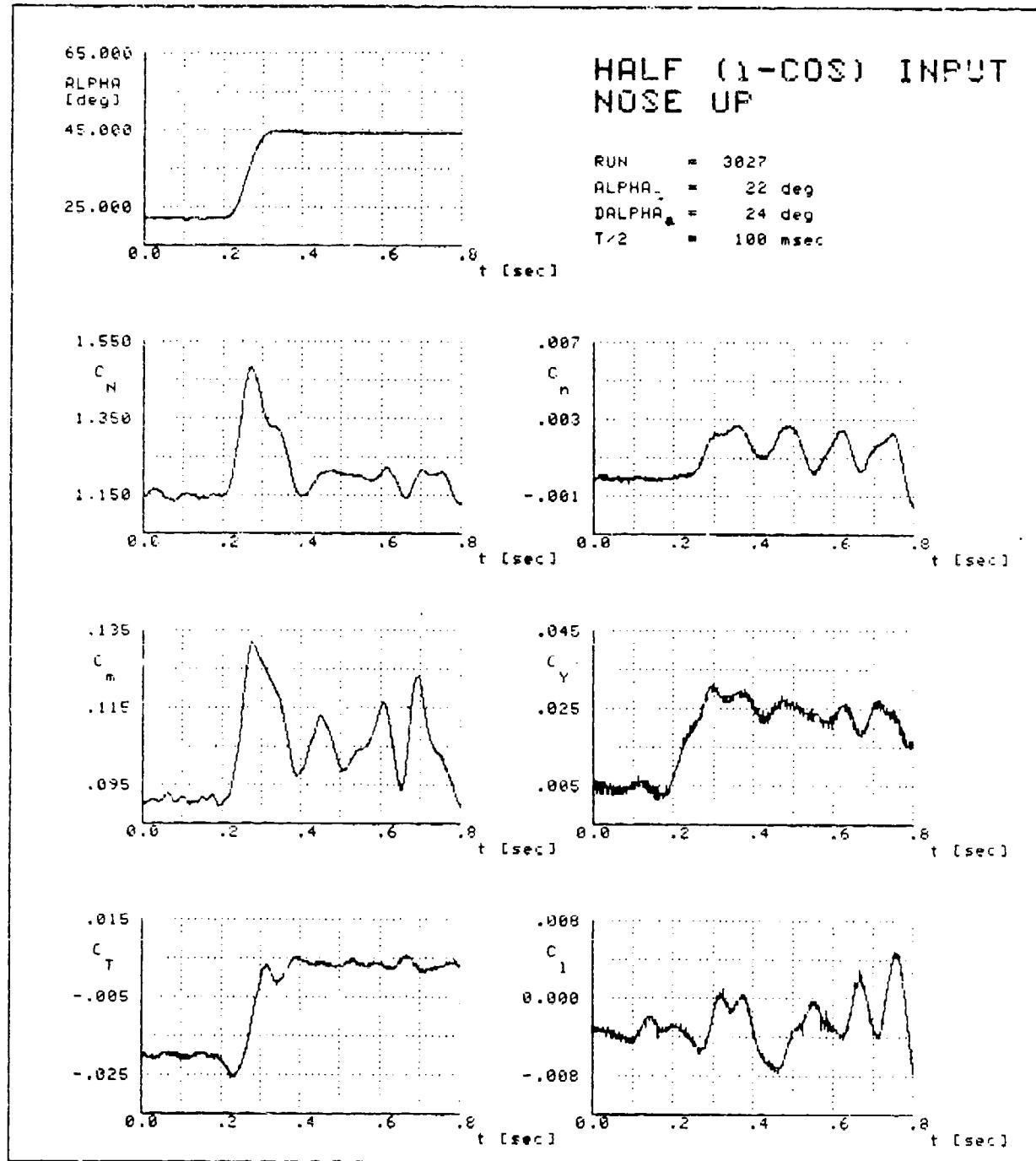


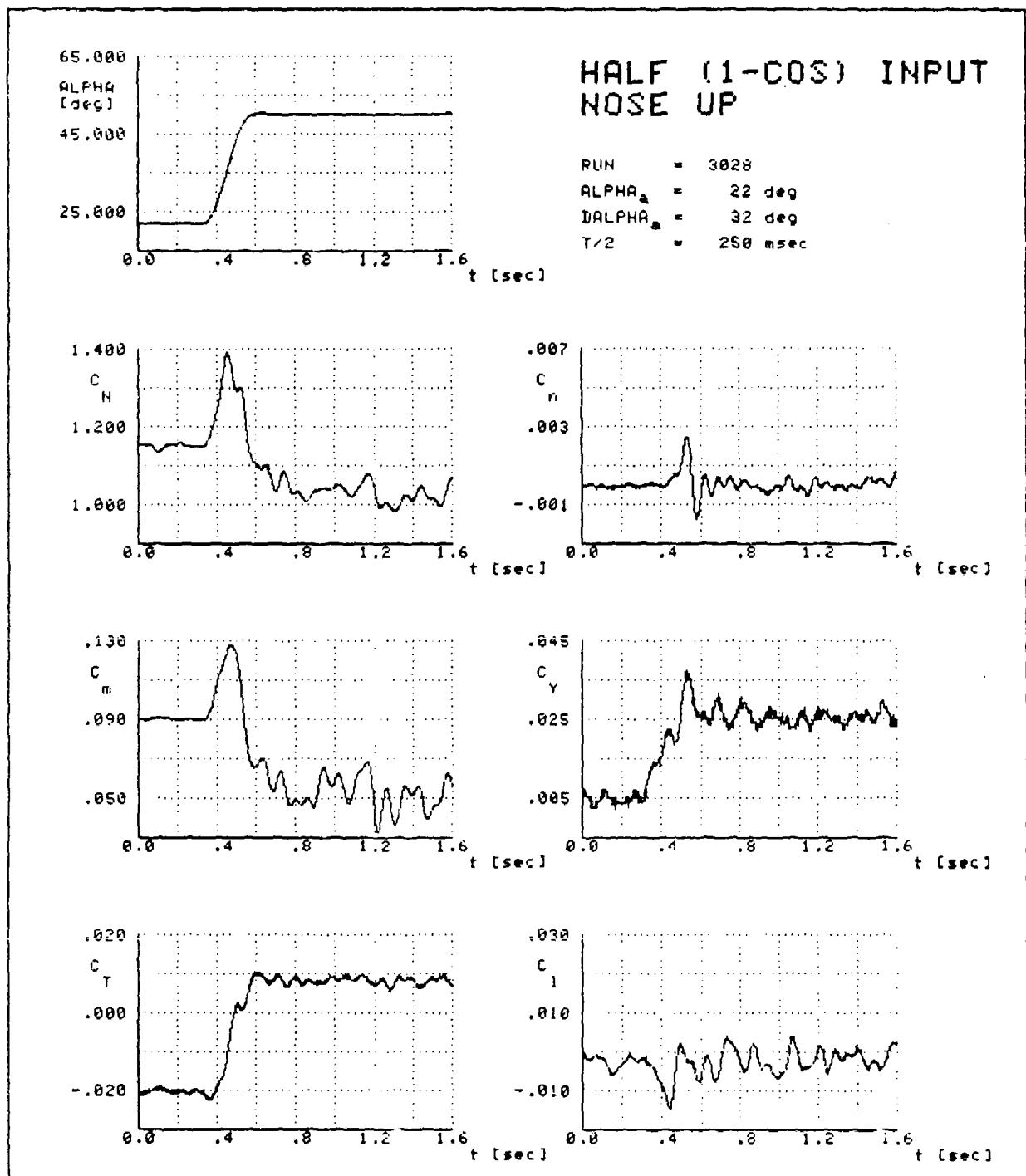


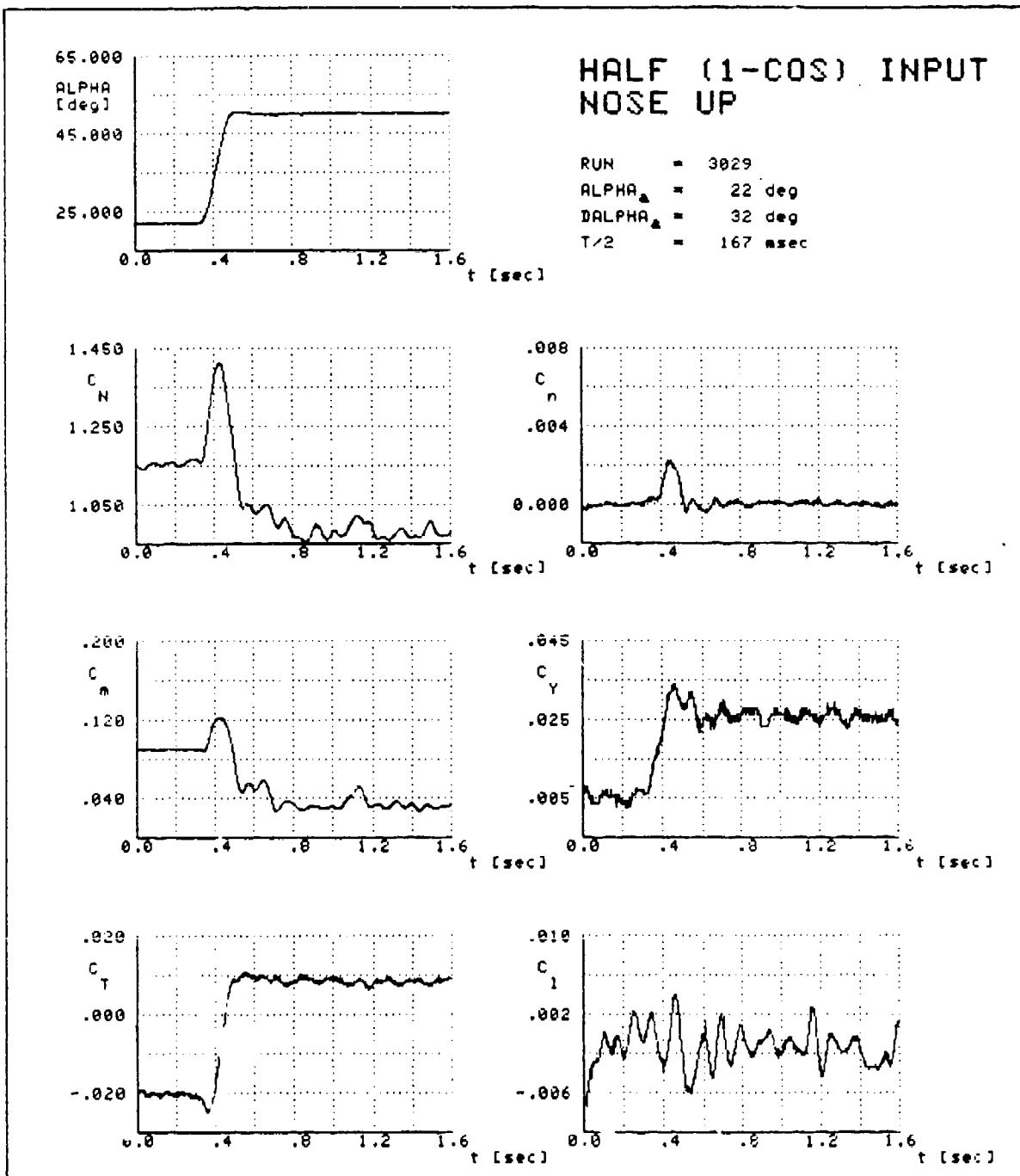


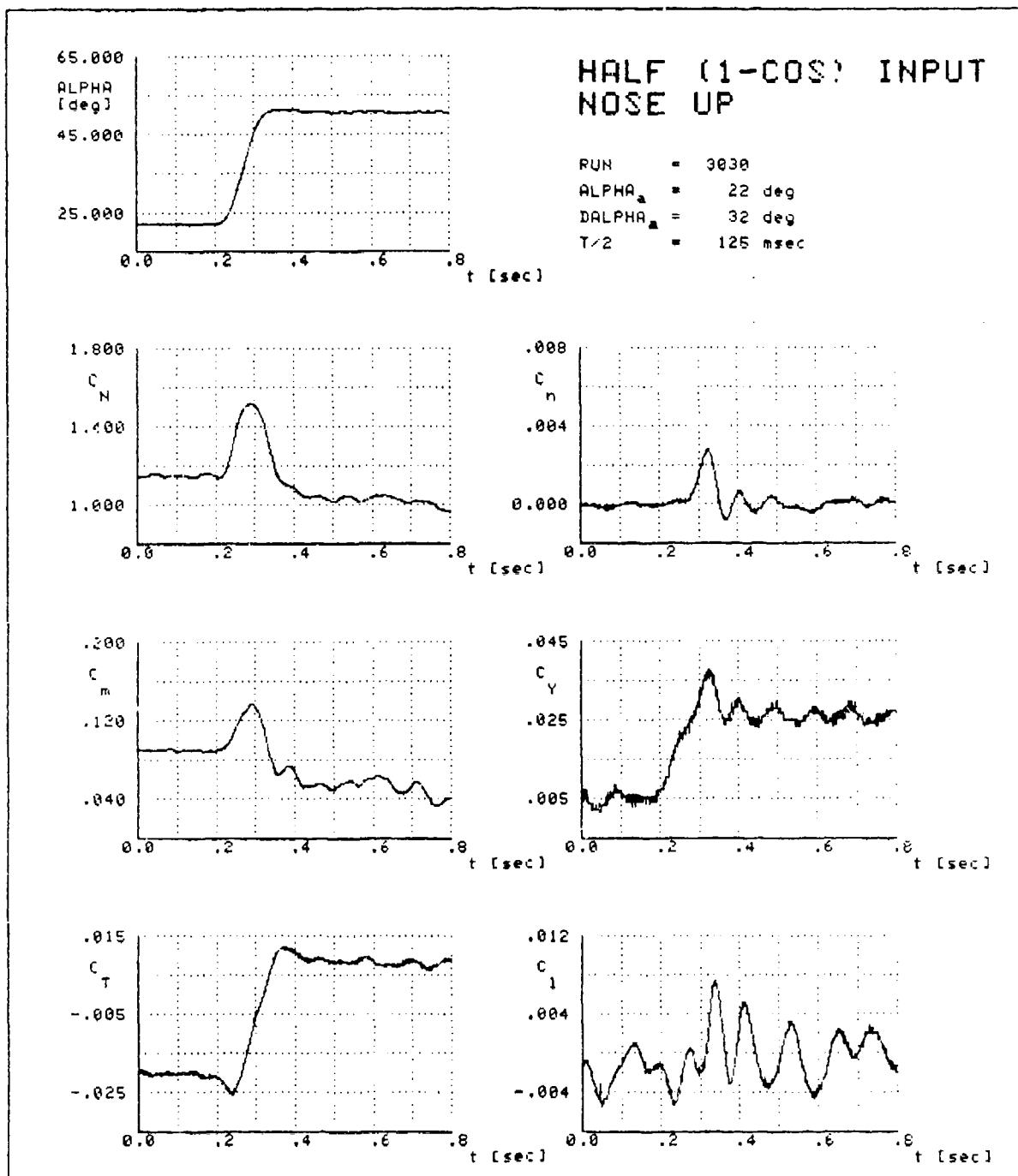




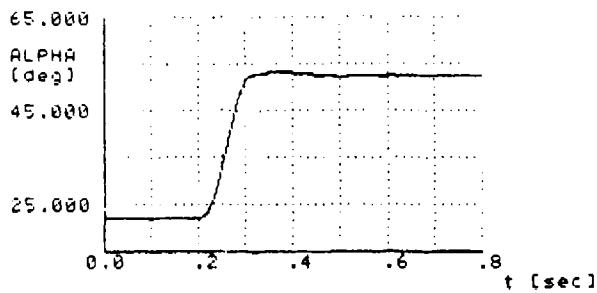




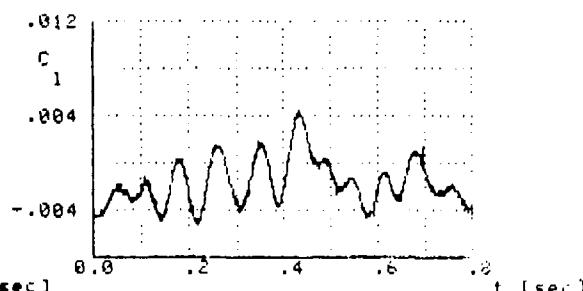
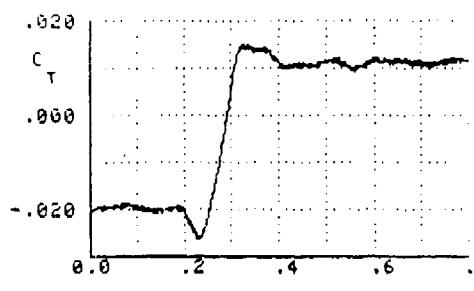
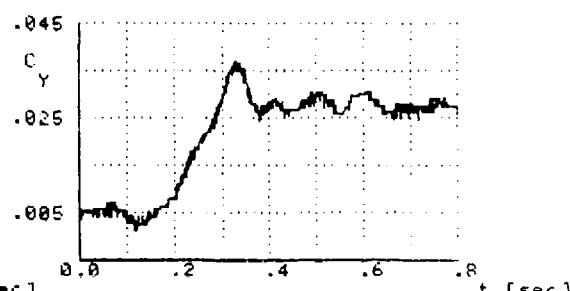
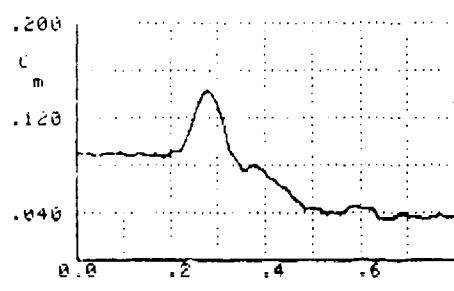
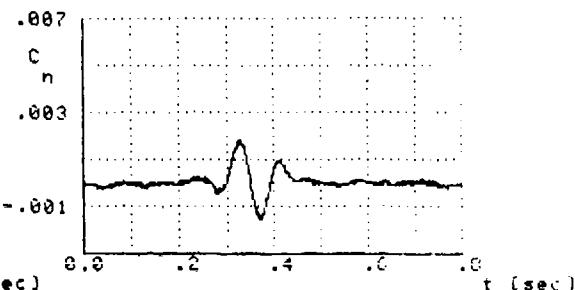
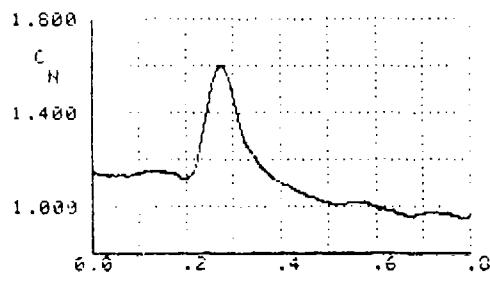


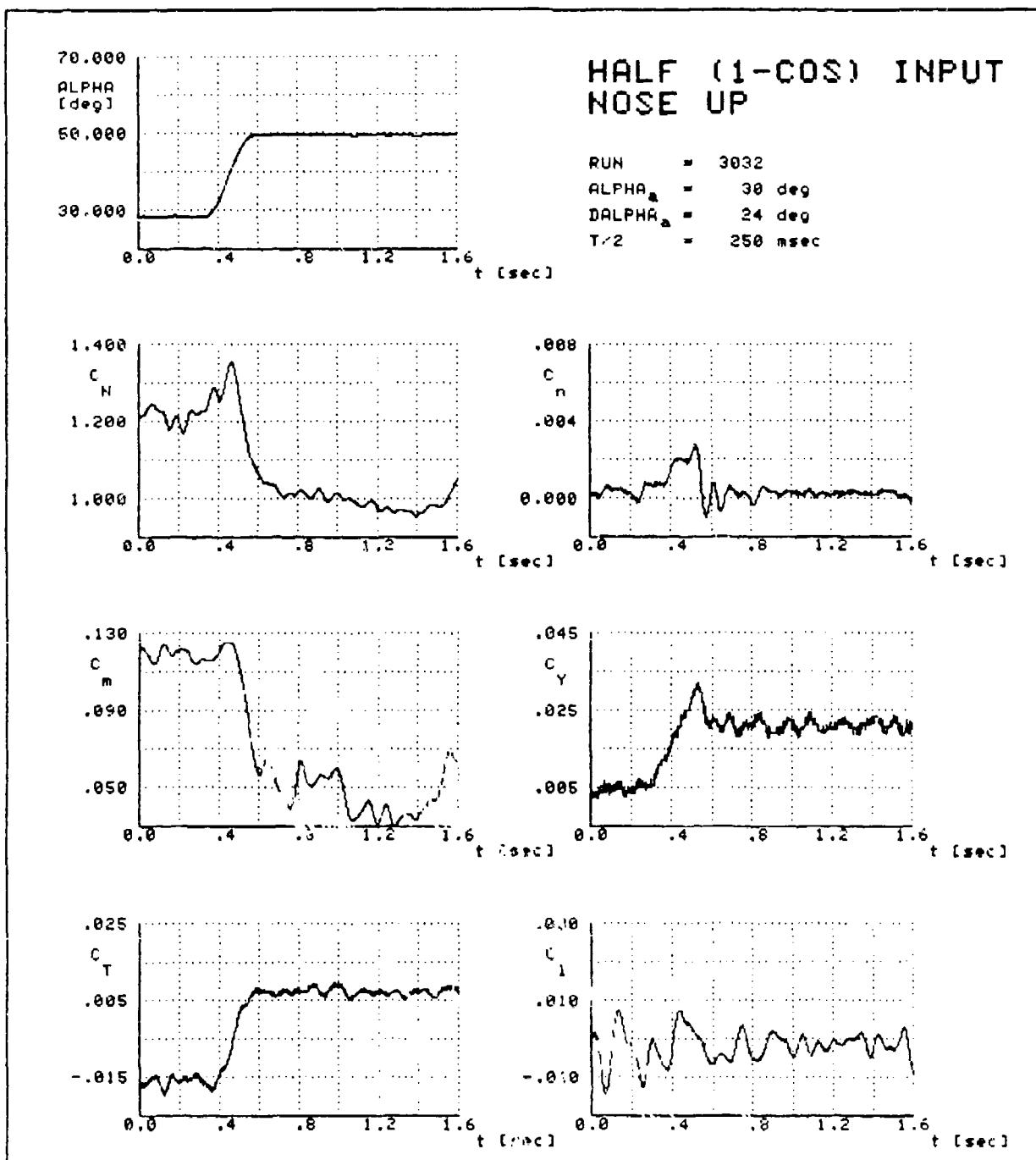


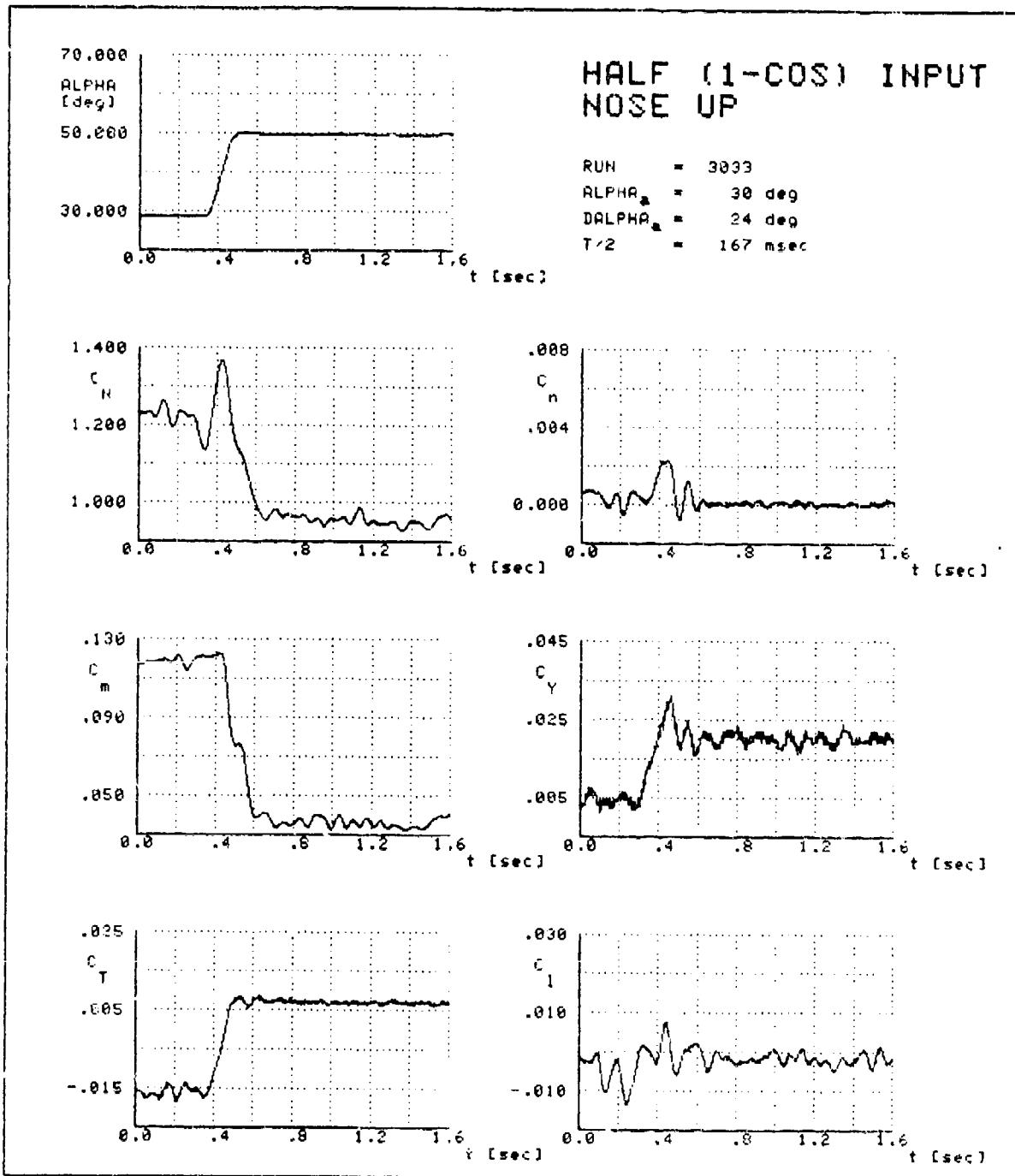
HALF (1-COS) INPUT
NOSE UP

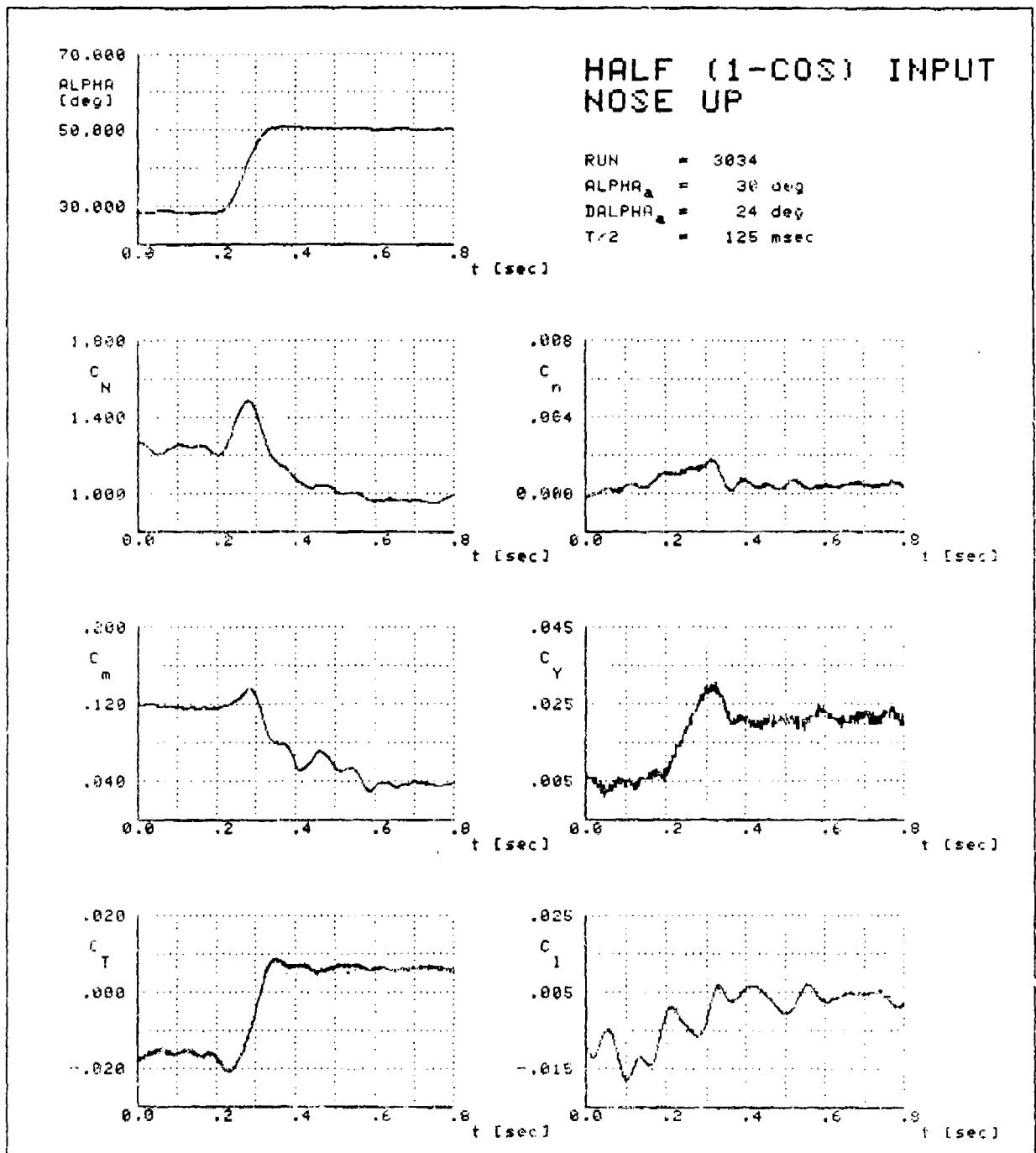


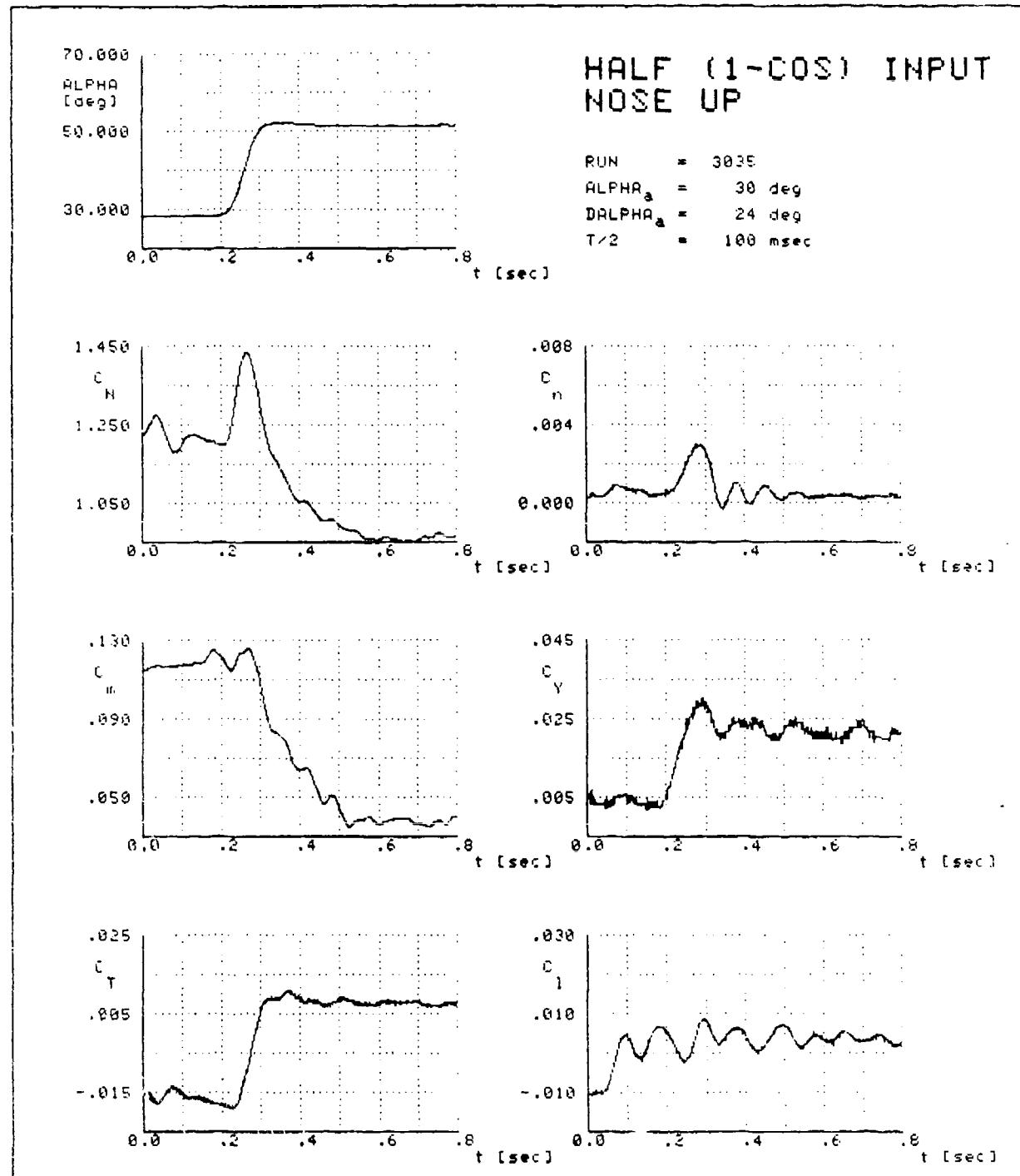
RUN = 3031
ALPHA_a = 22 deg
DALPHA_a = 32 deg
T/2 = 100 msec

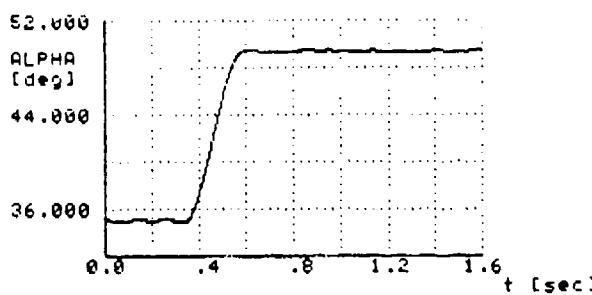






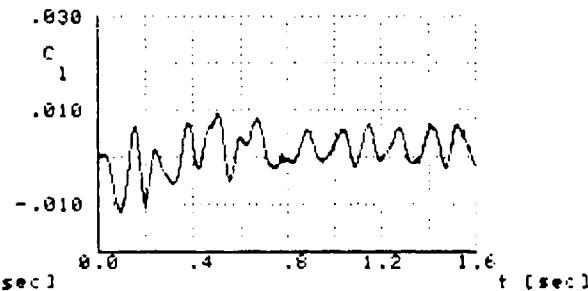
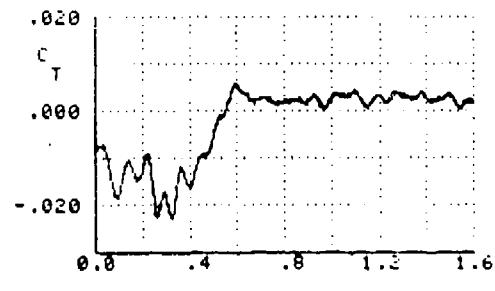
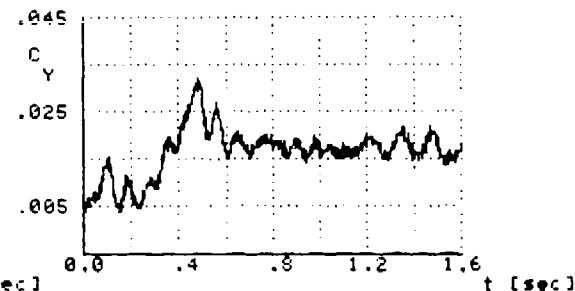
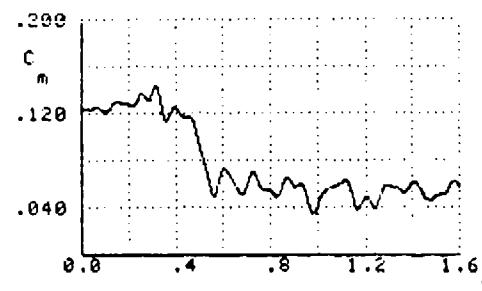
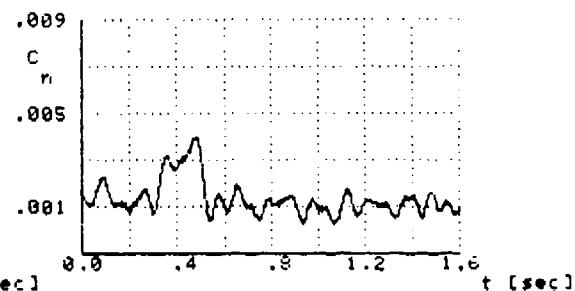
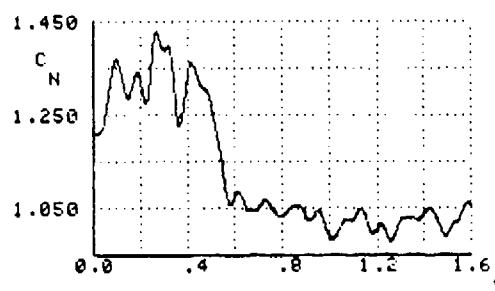


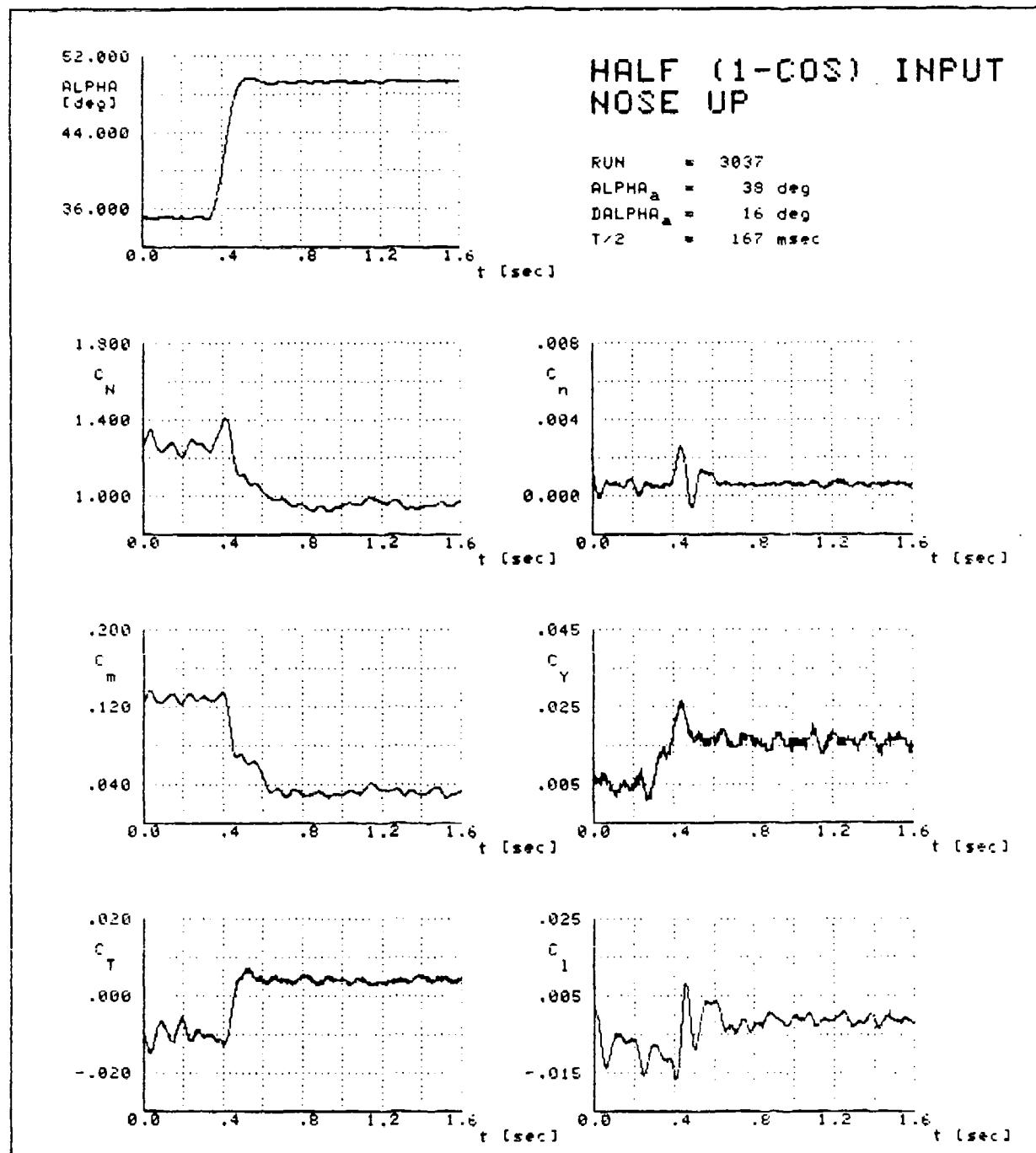


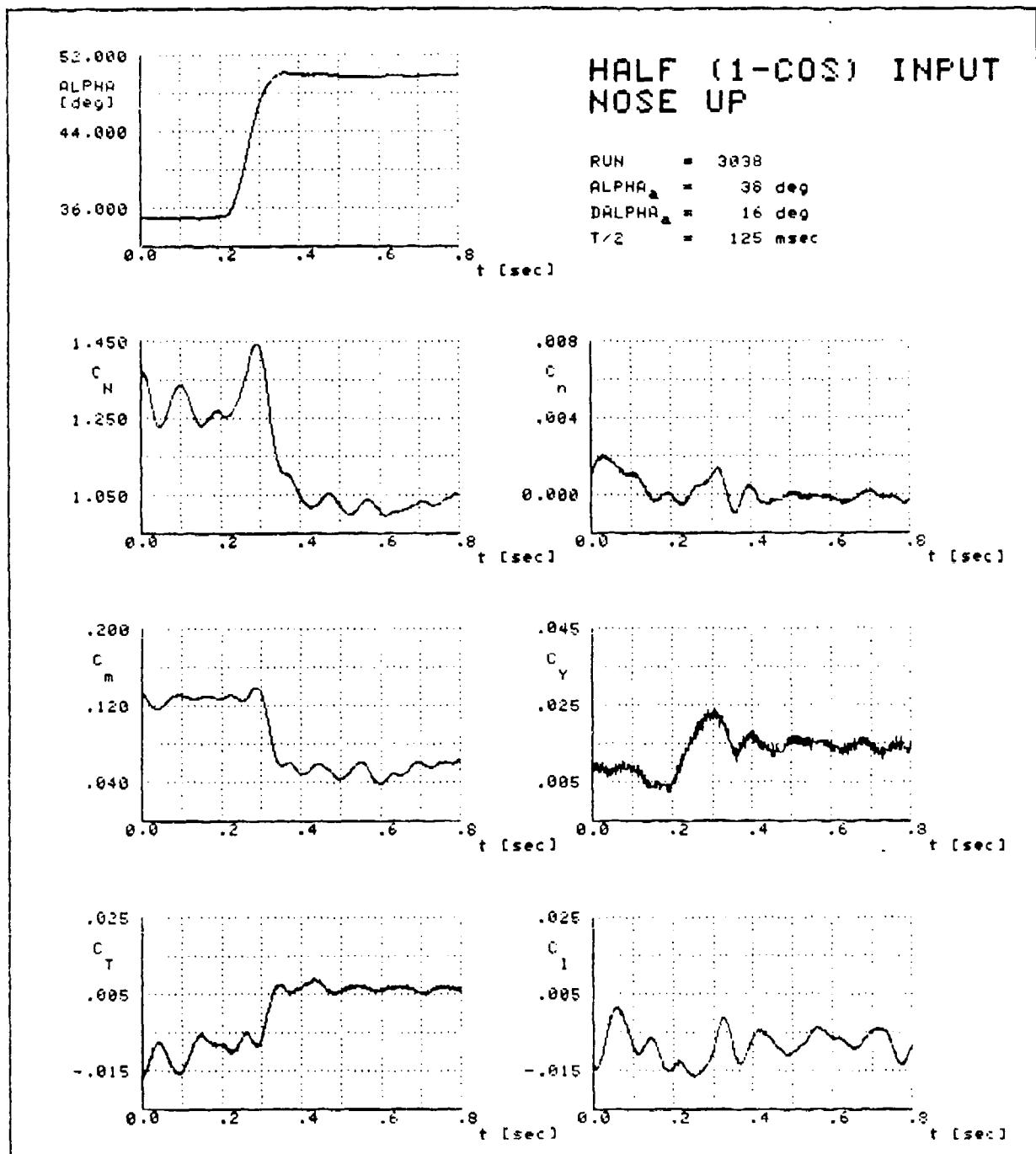


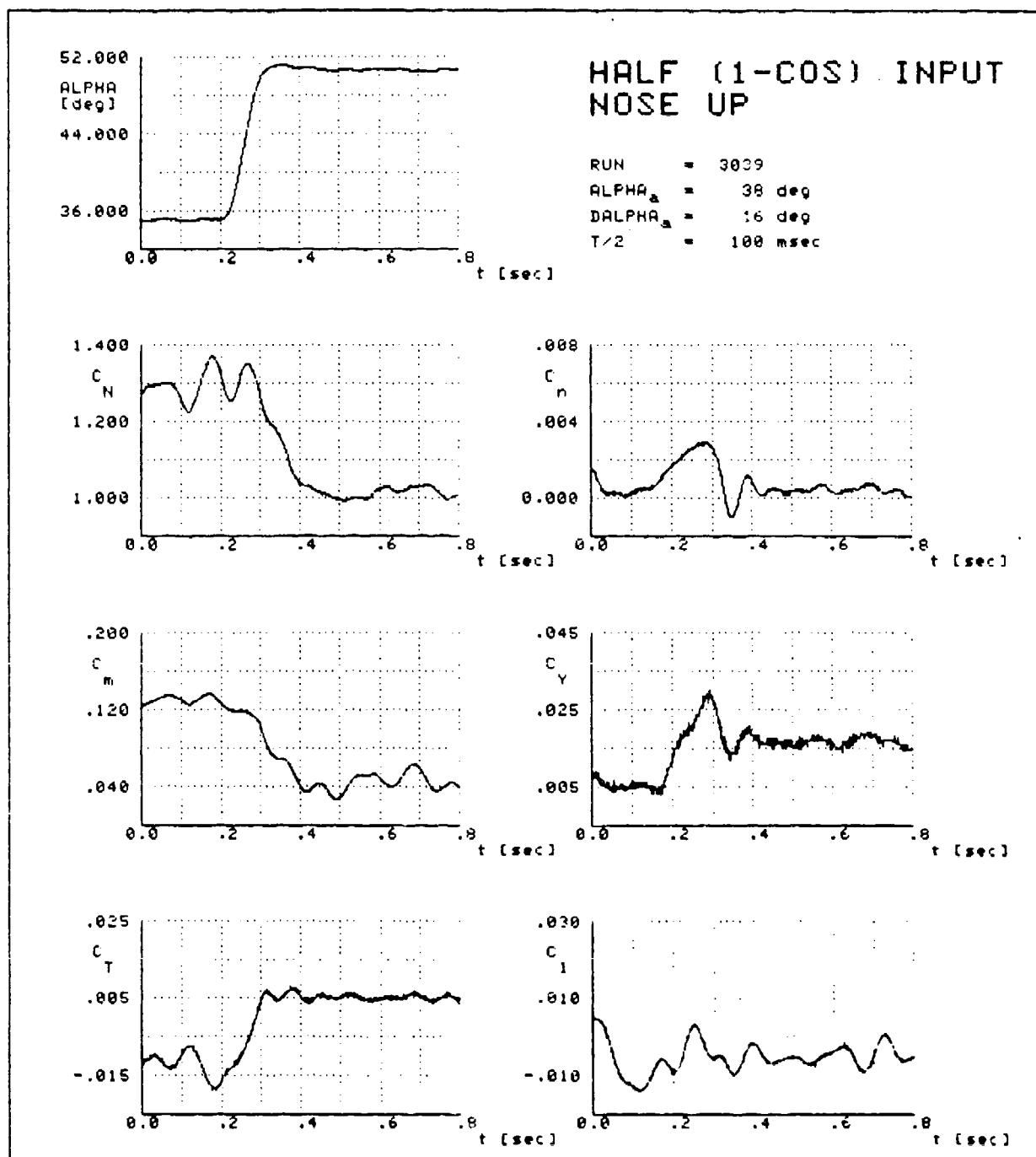
HALF (1-COS) INPUT NOSE UP

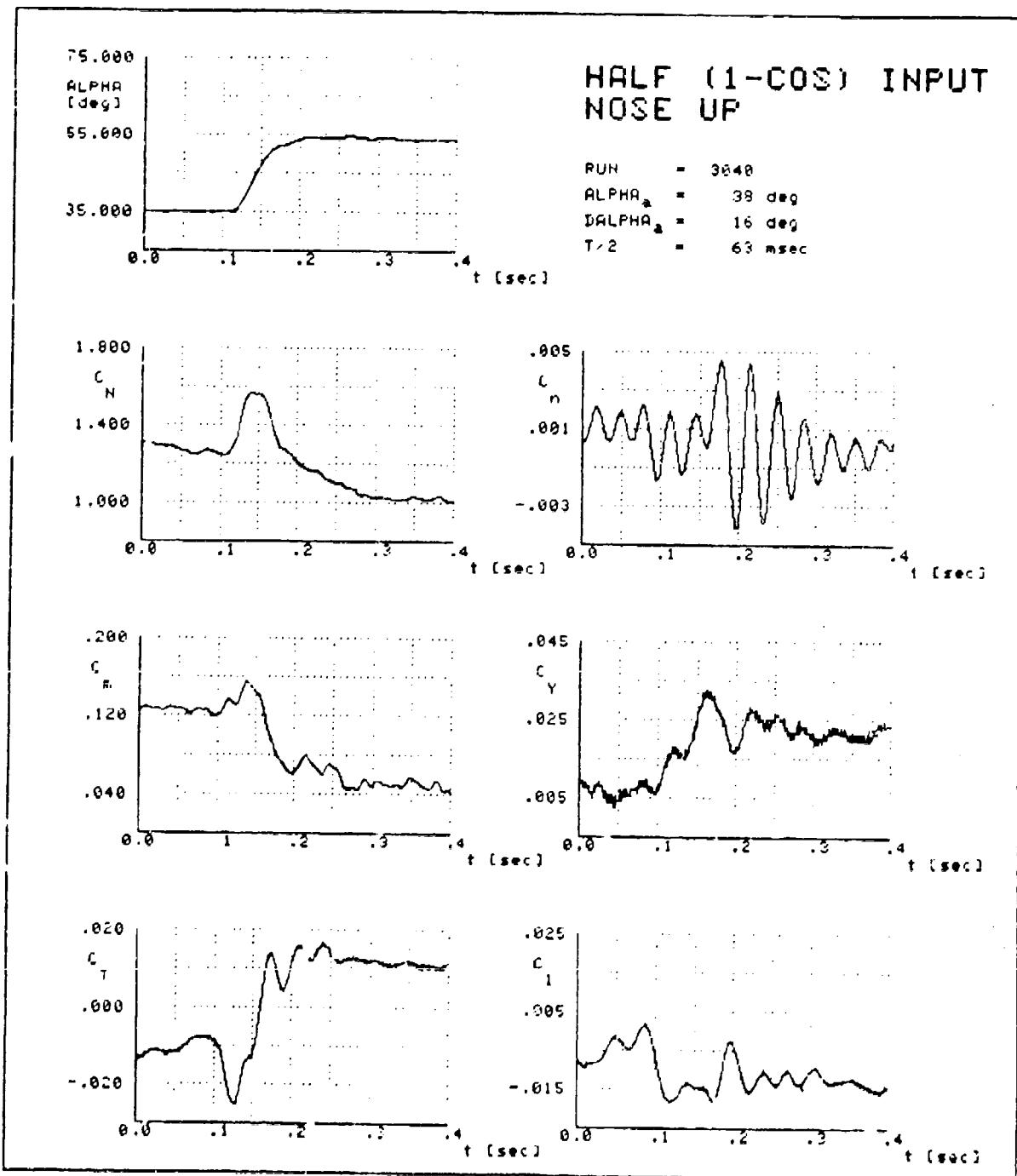
RUN = 3036
ALPHA_a = 38 deg
DALPHA_a = 16 deg
T/2 = 250 msec

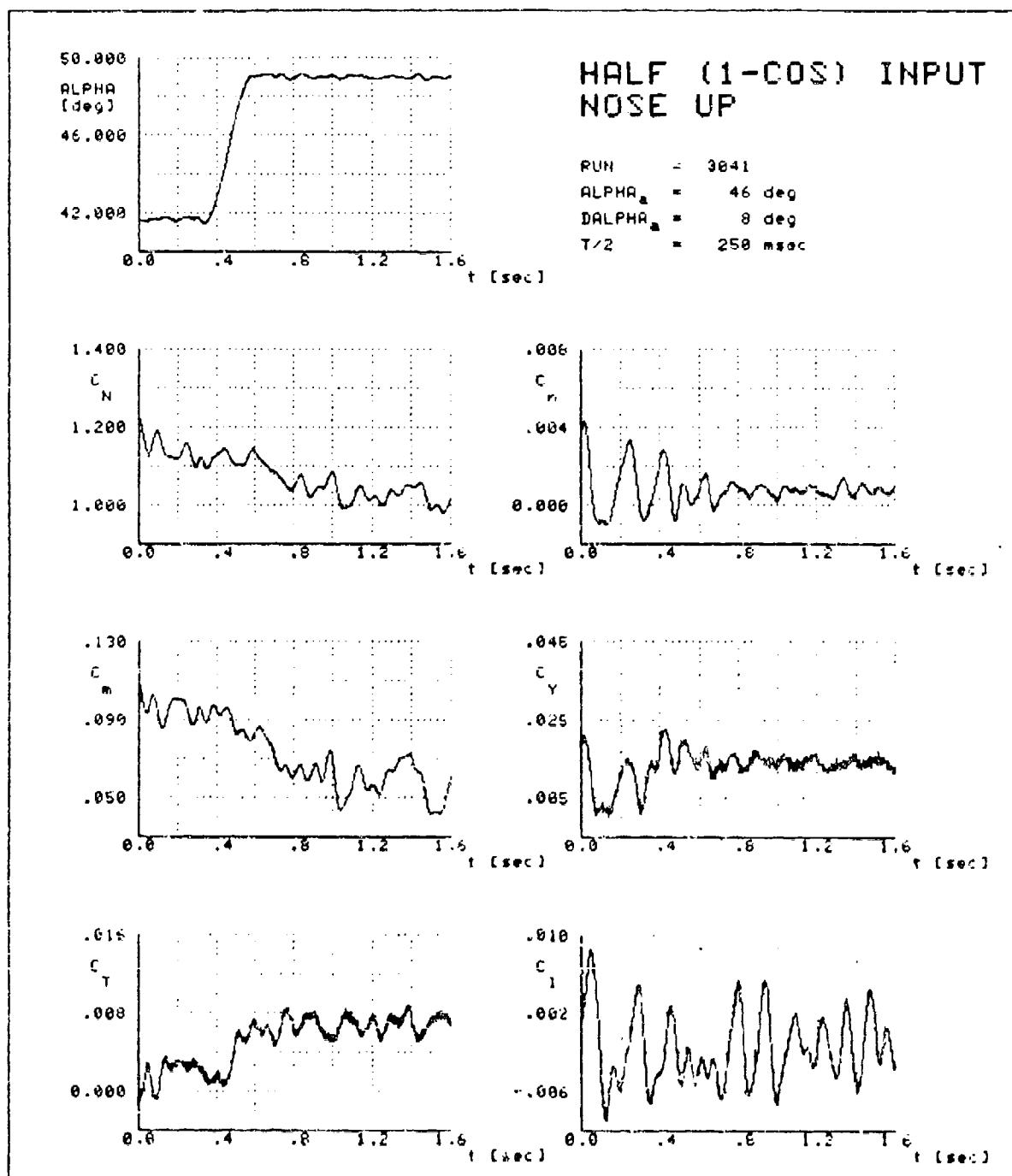


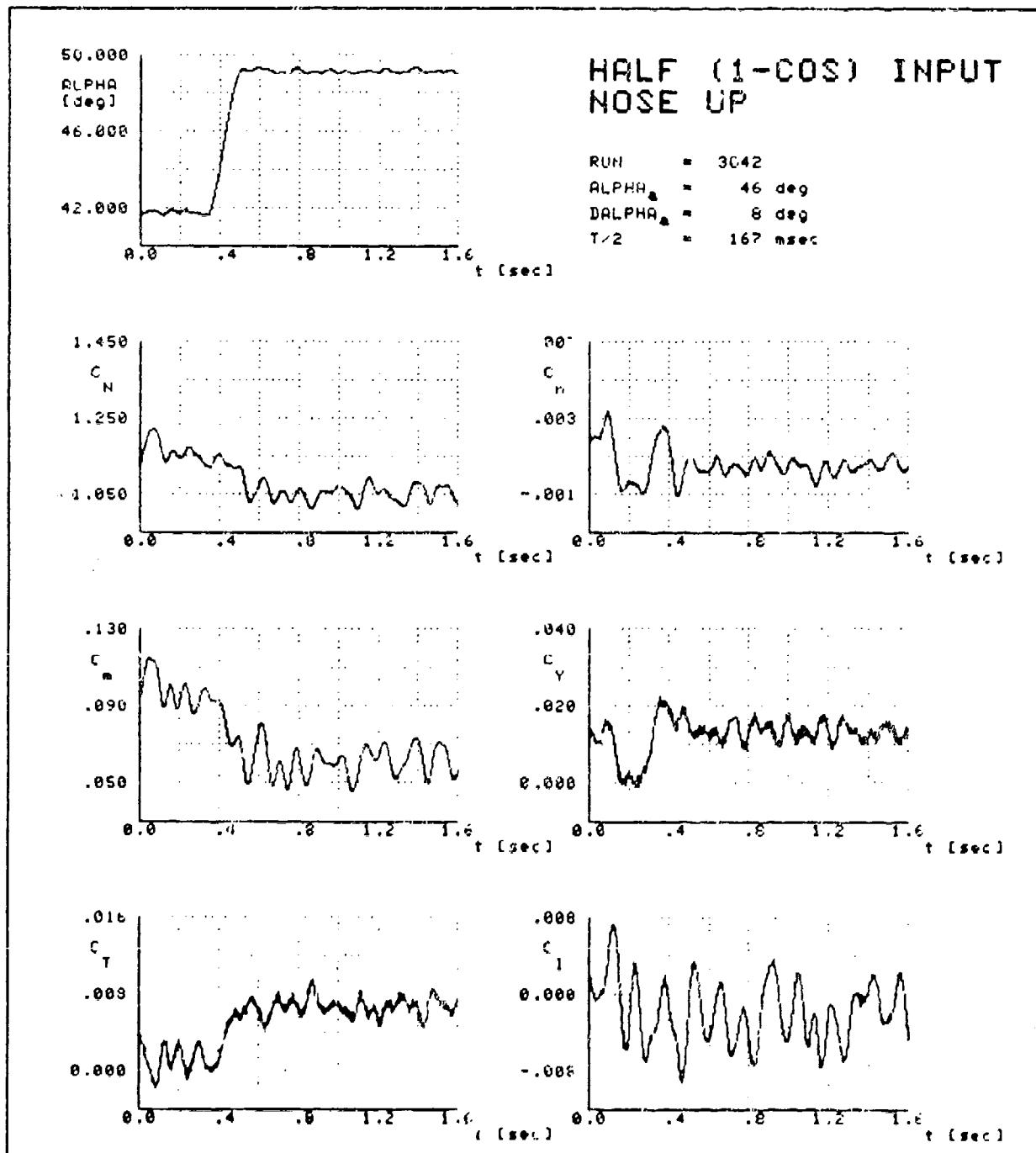


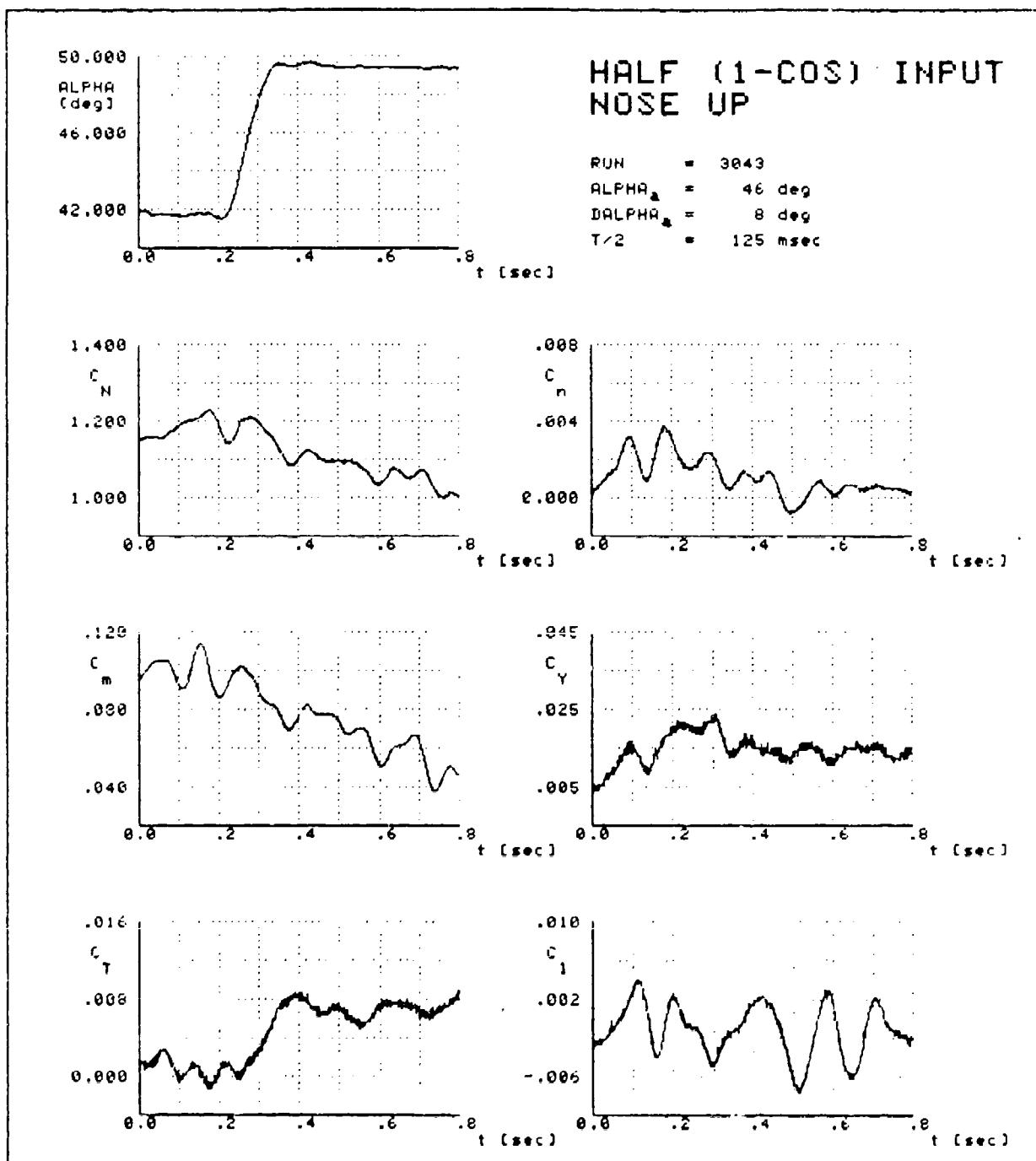


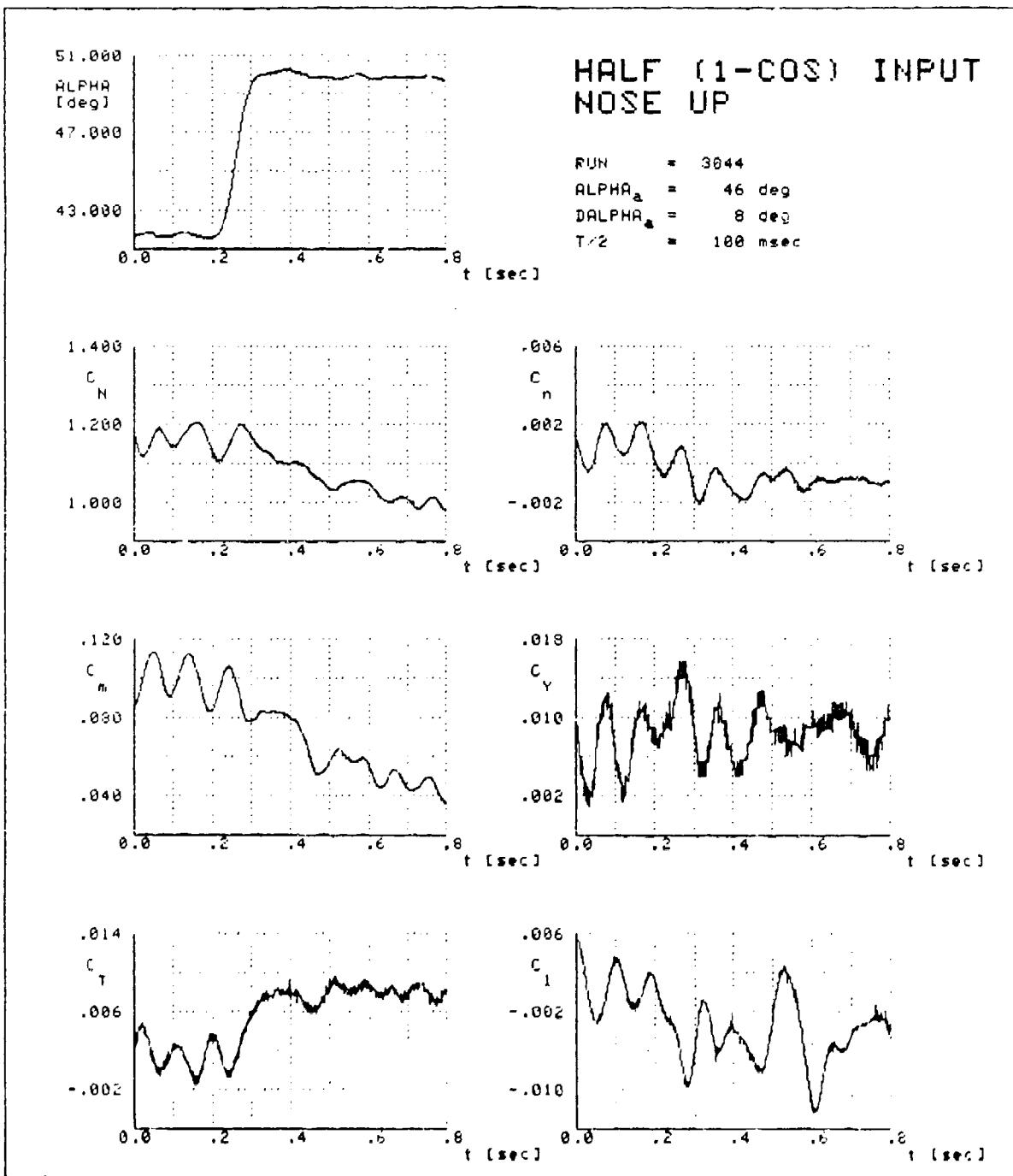


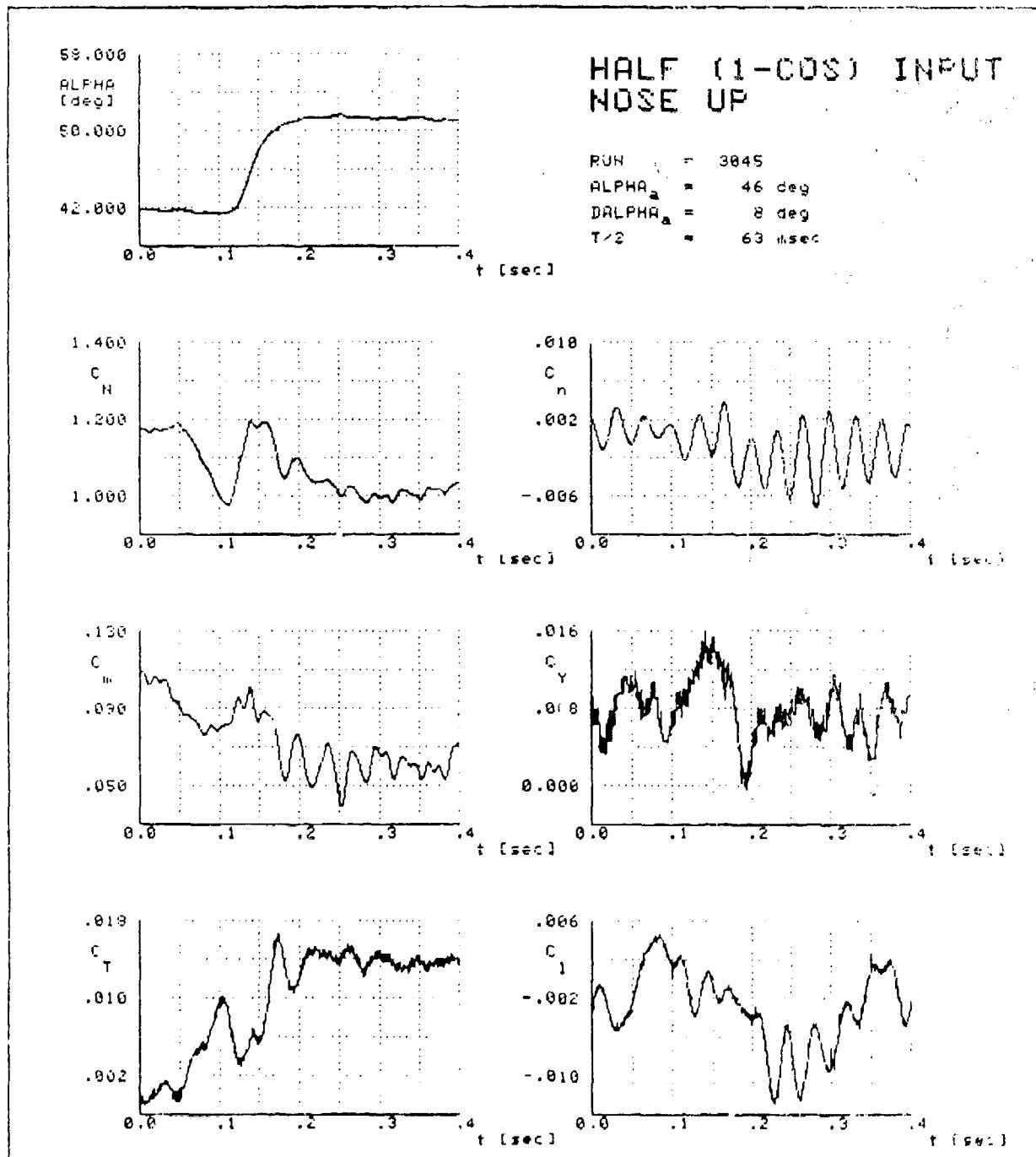


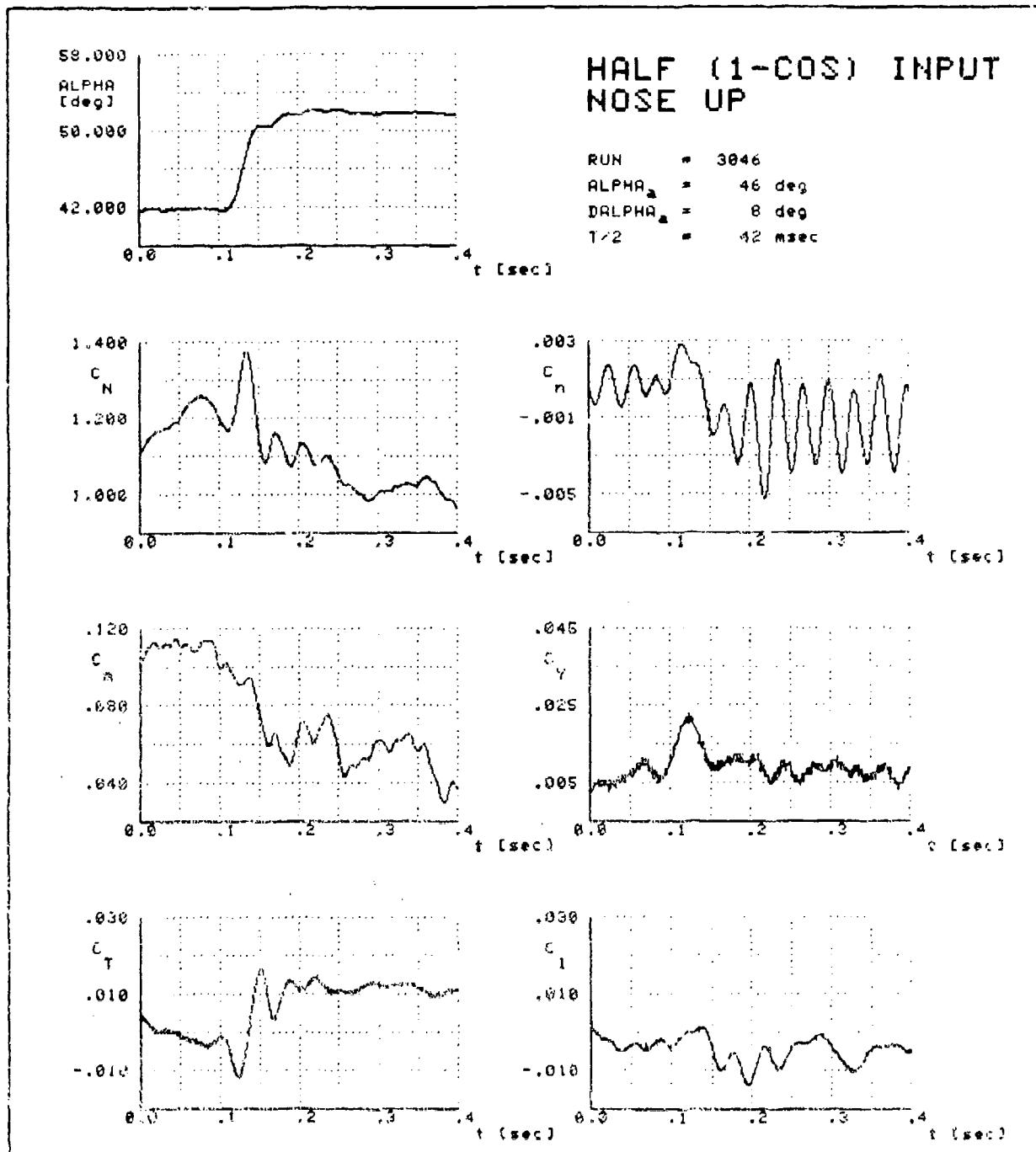


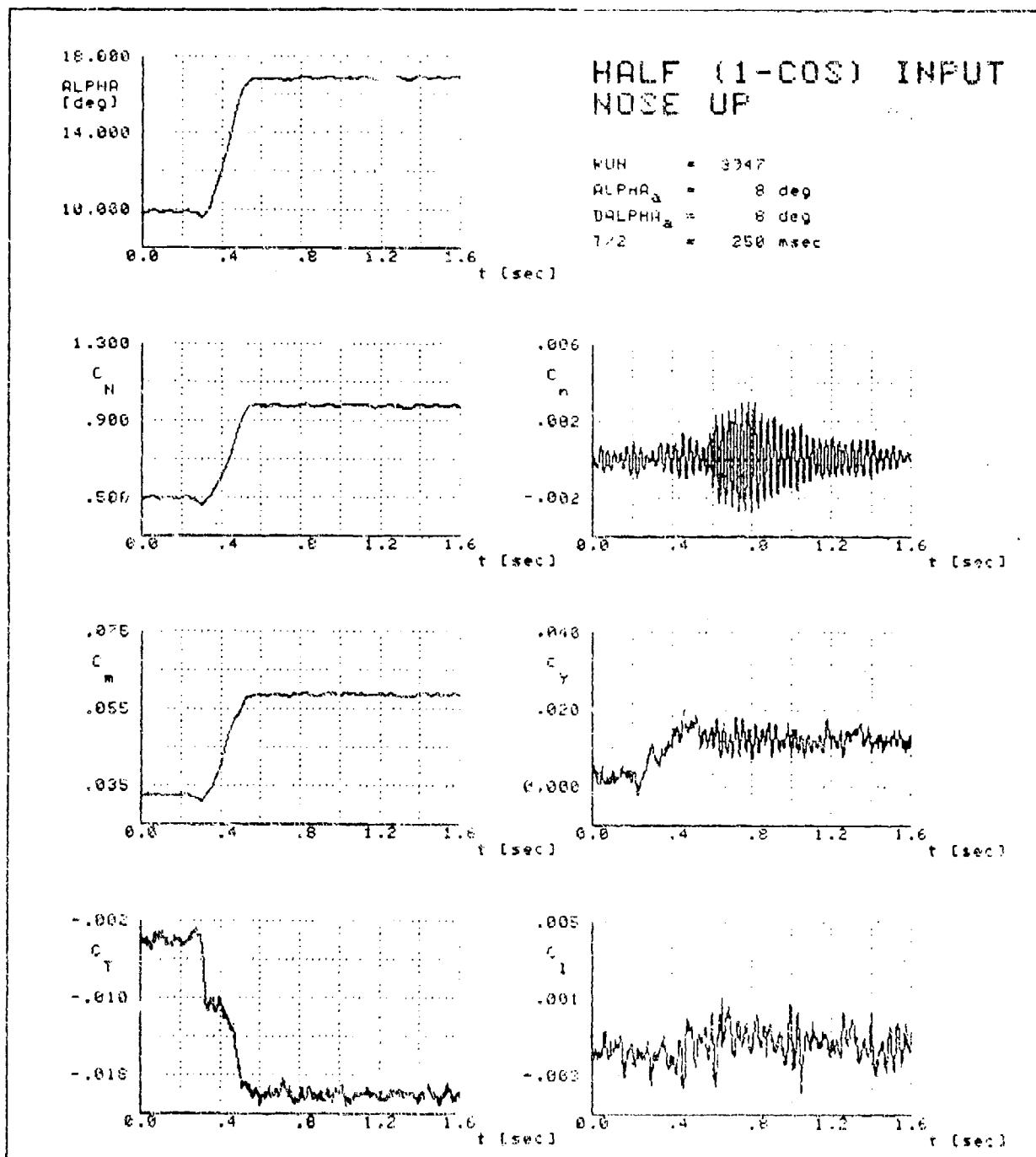


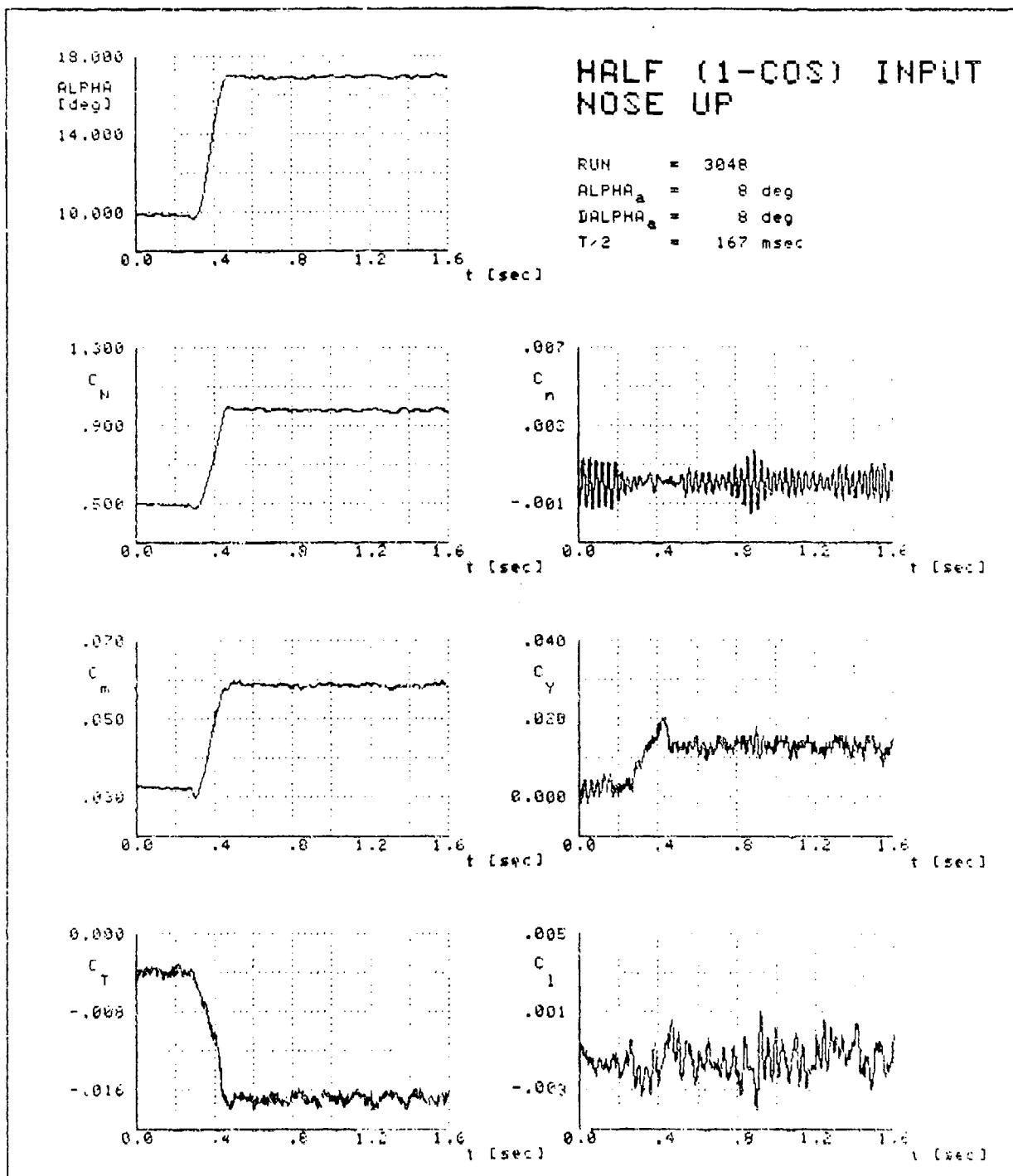


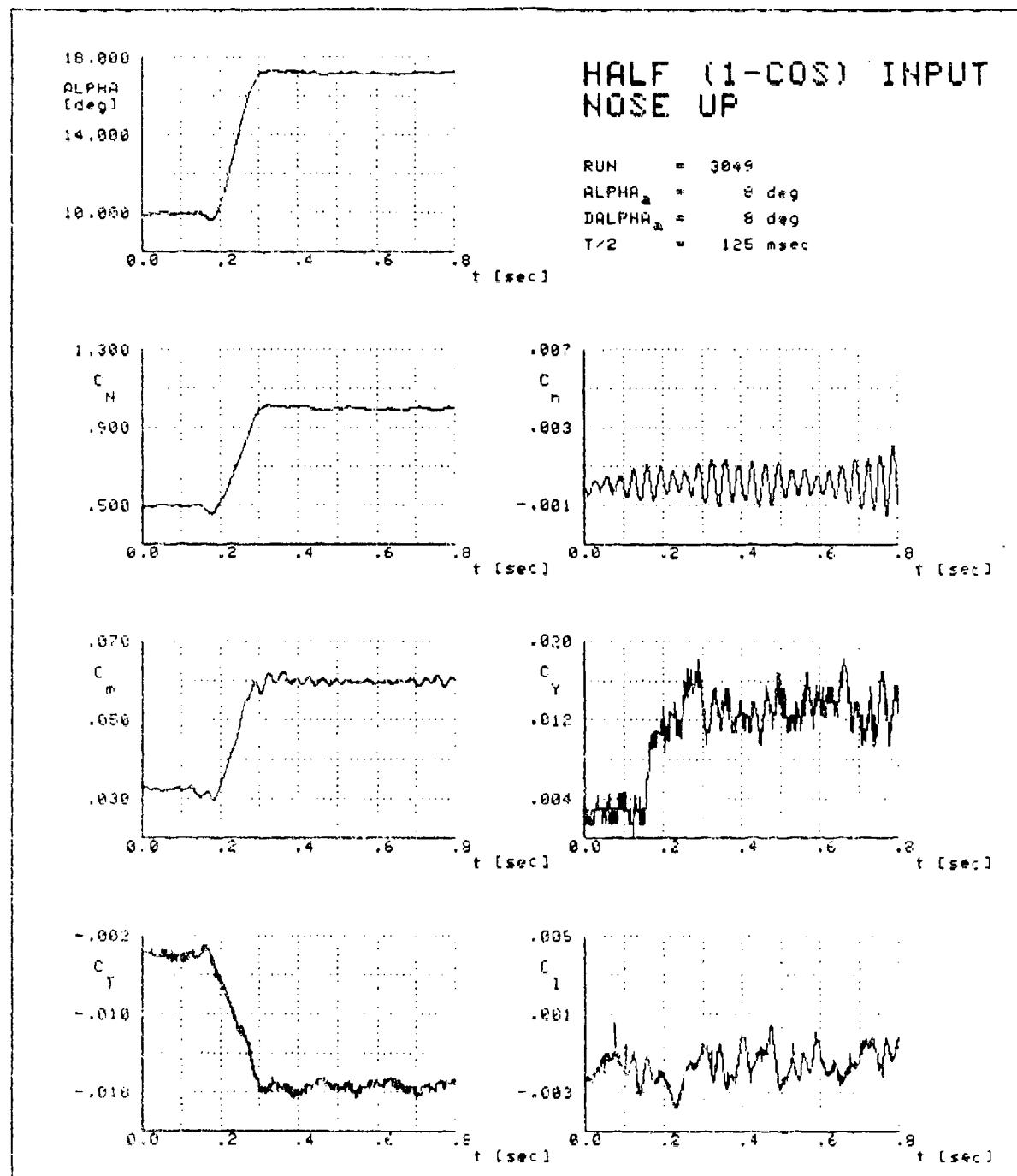


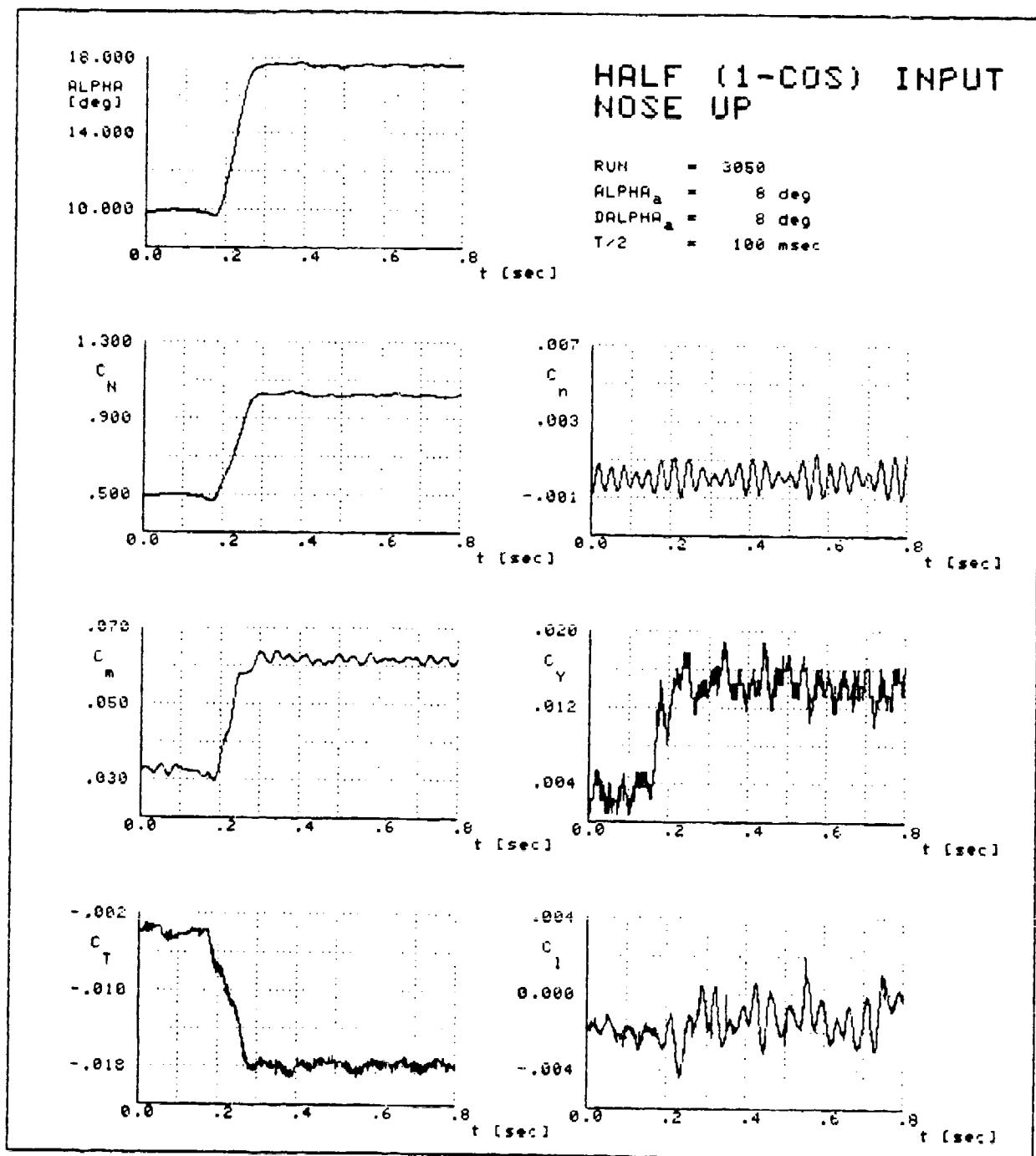


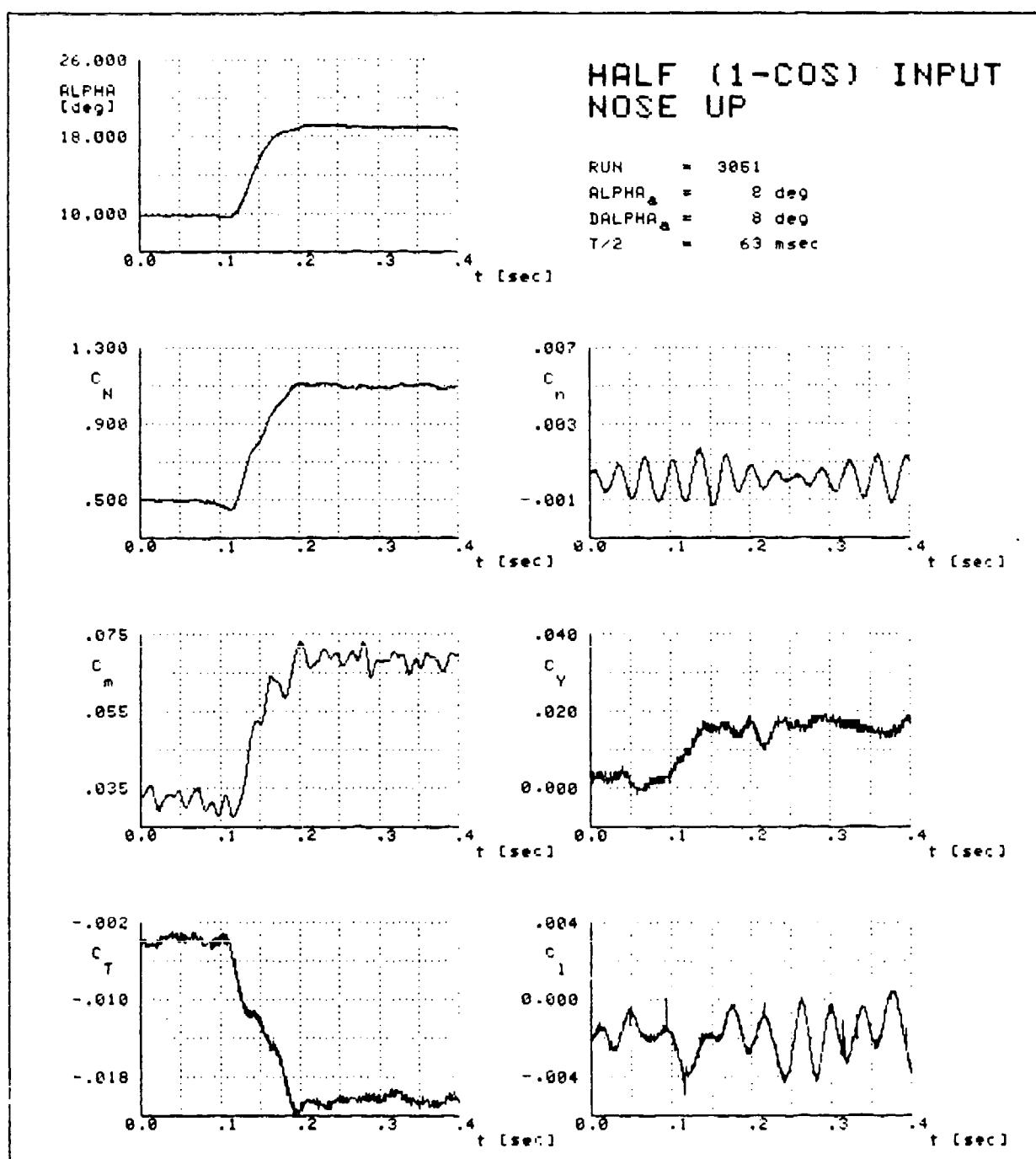


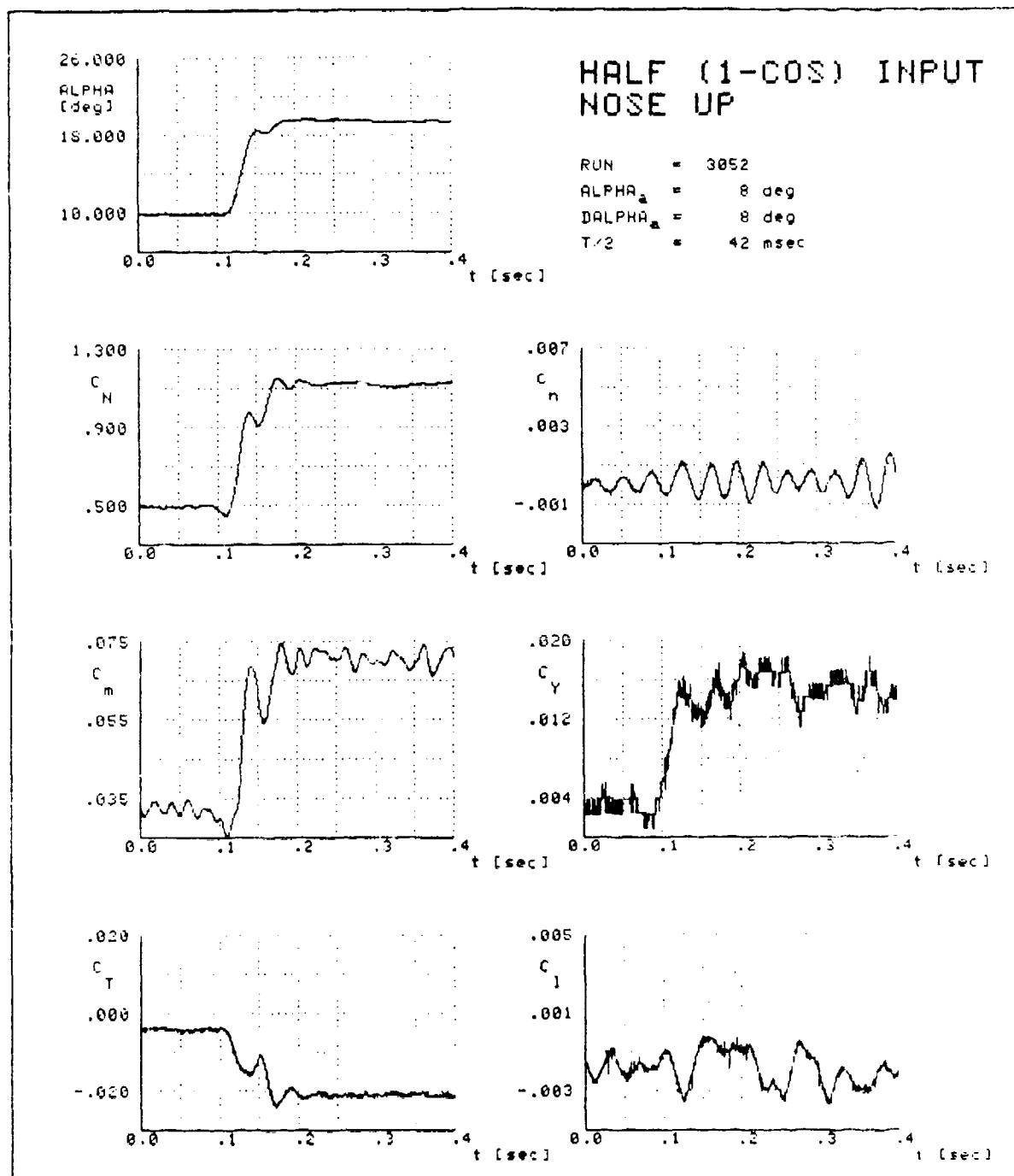


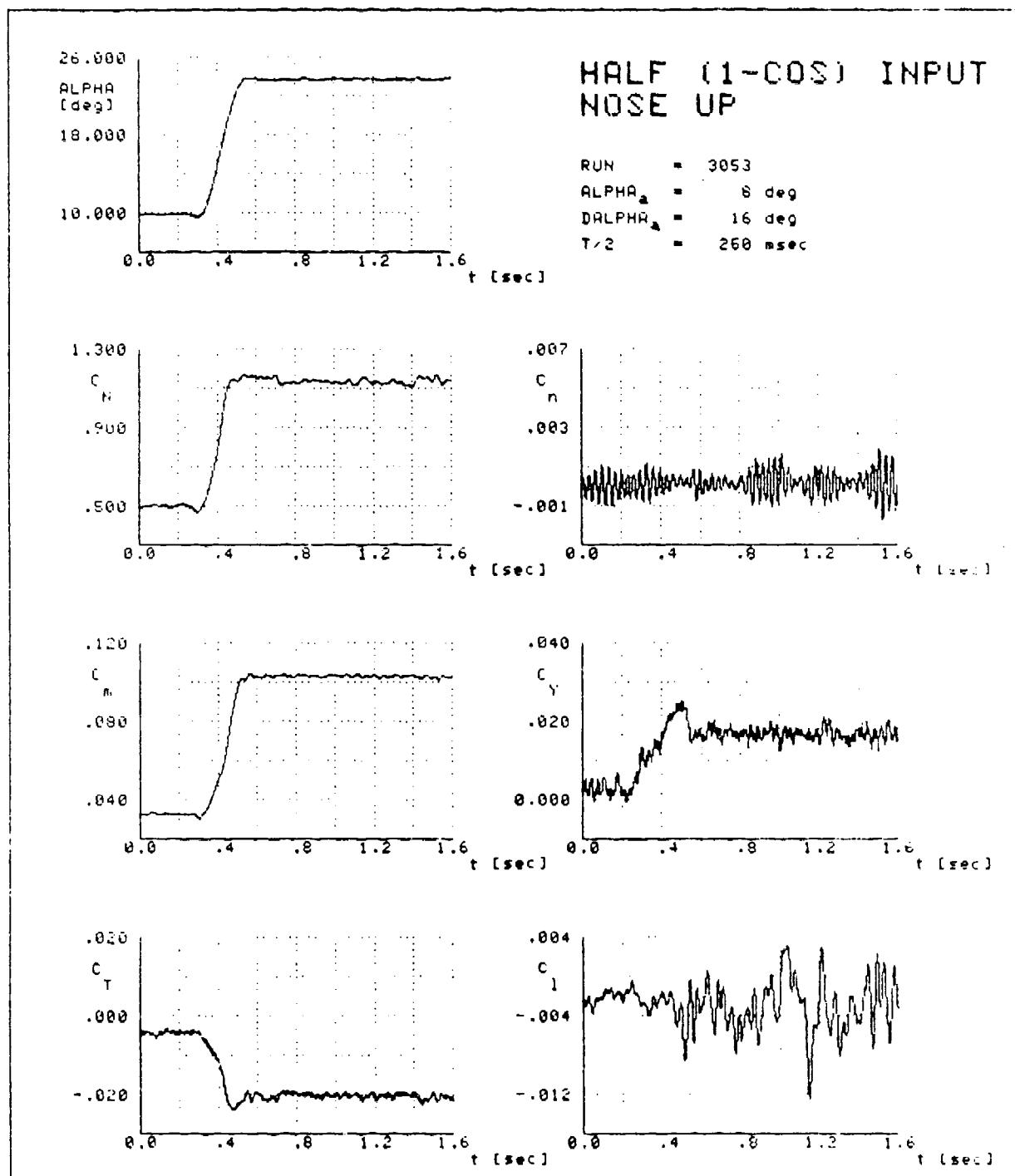


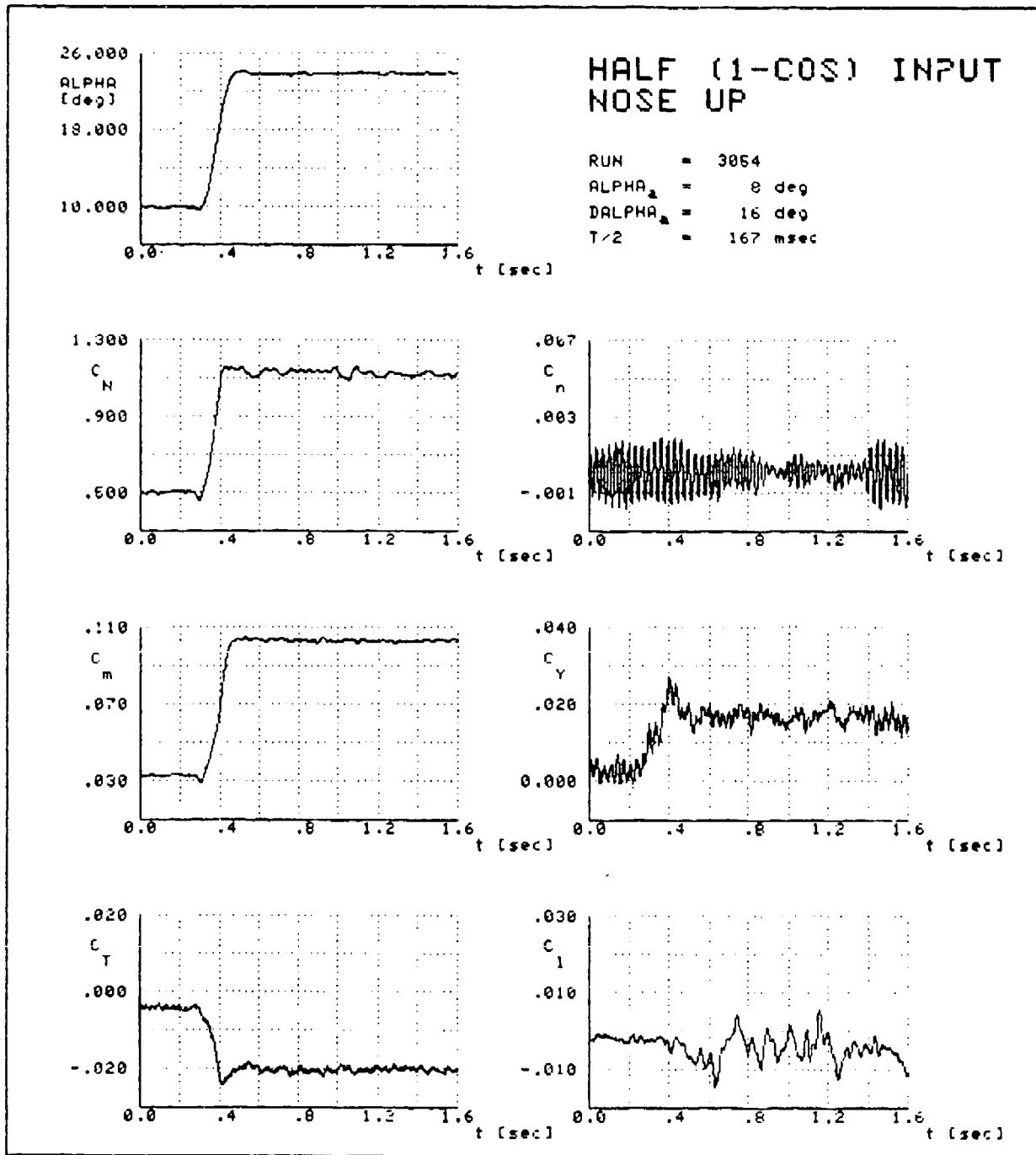


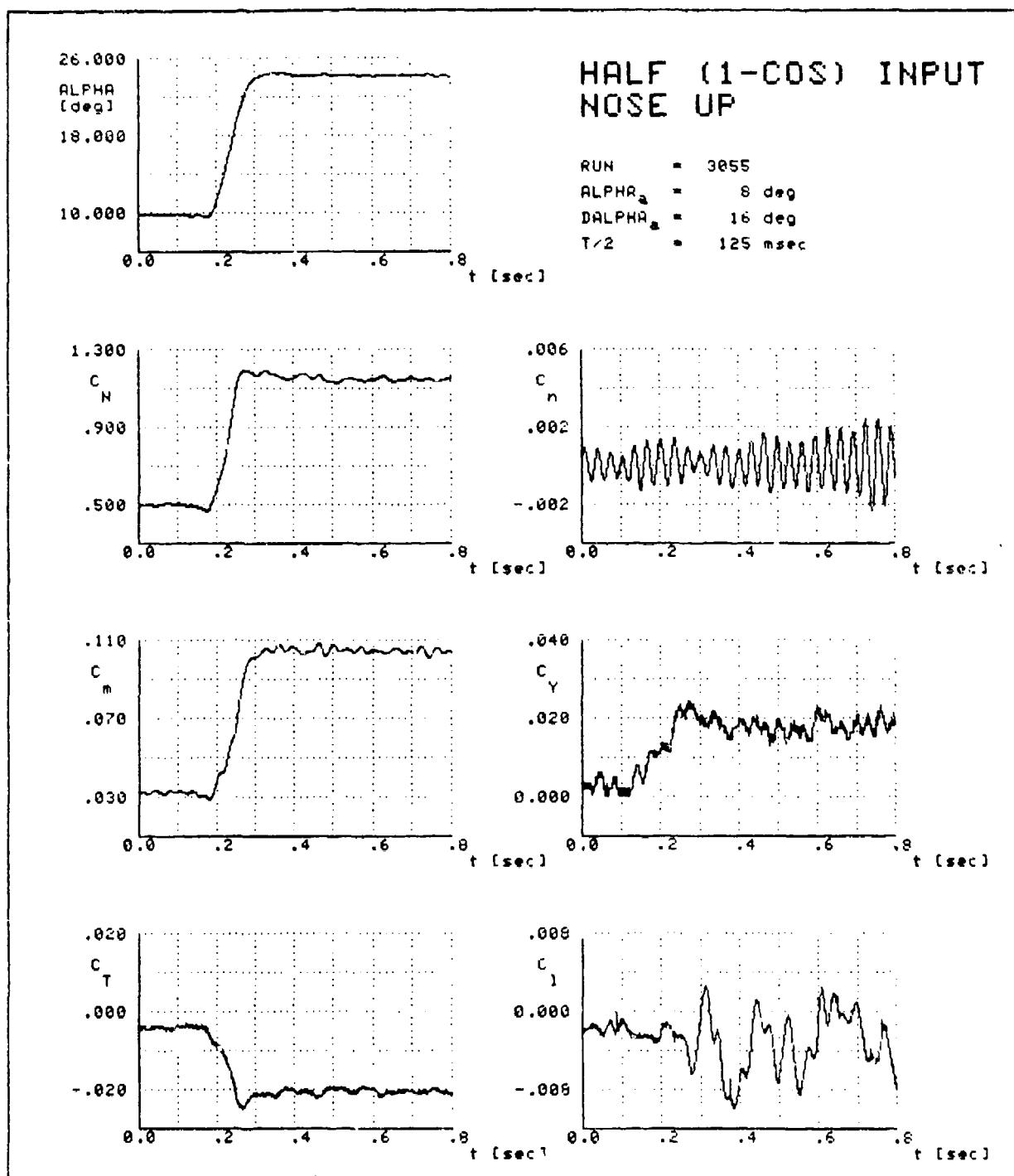


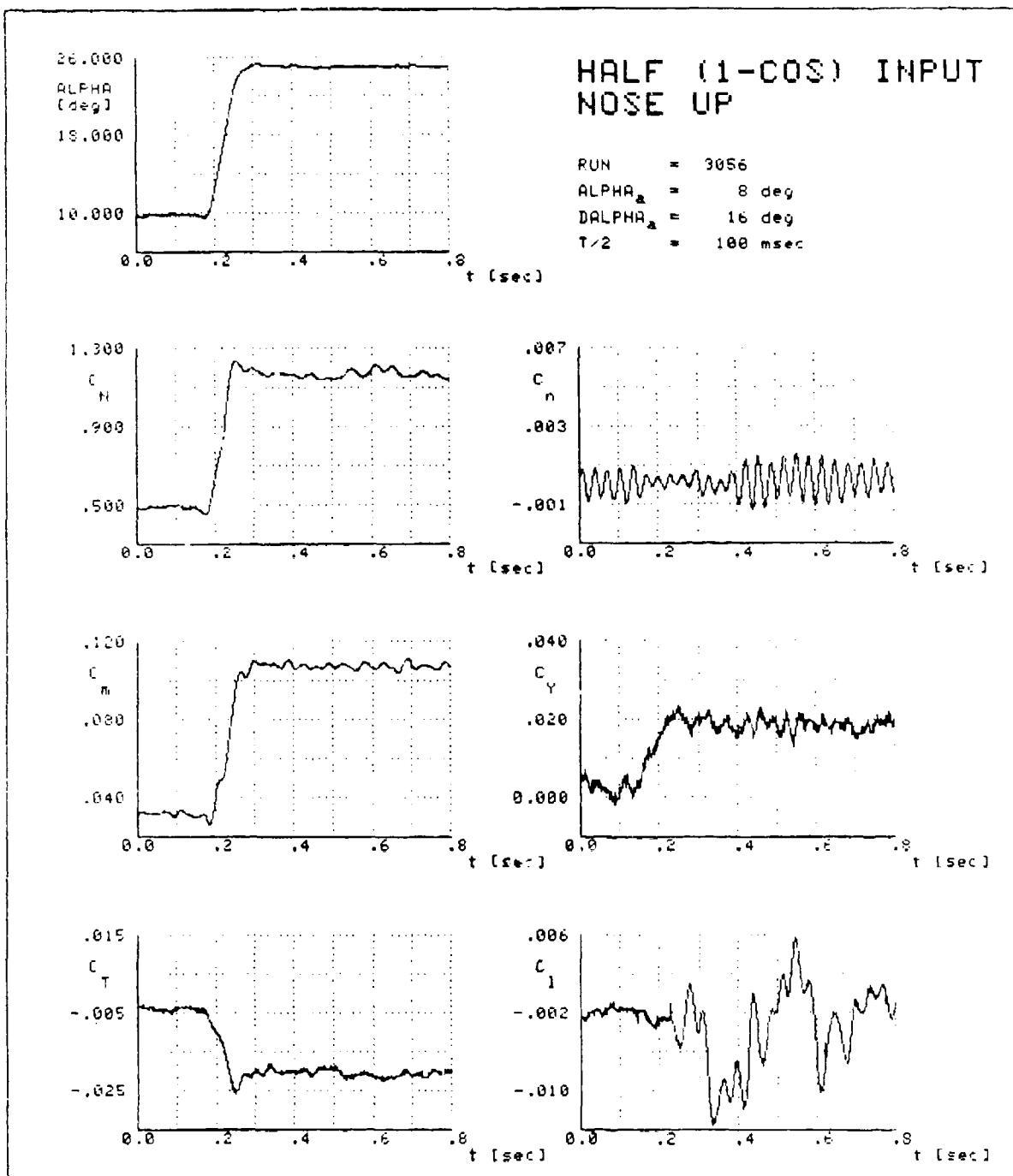


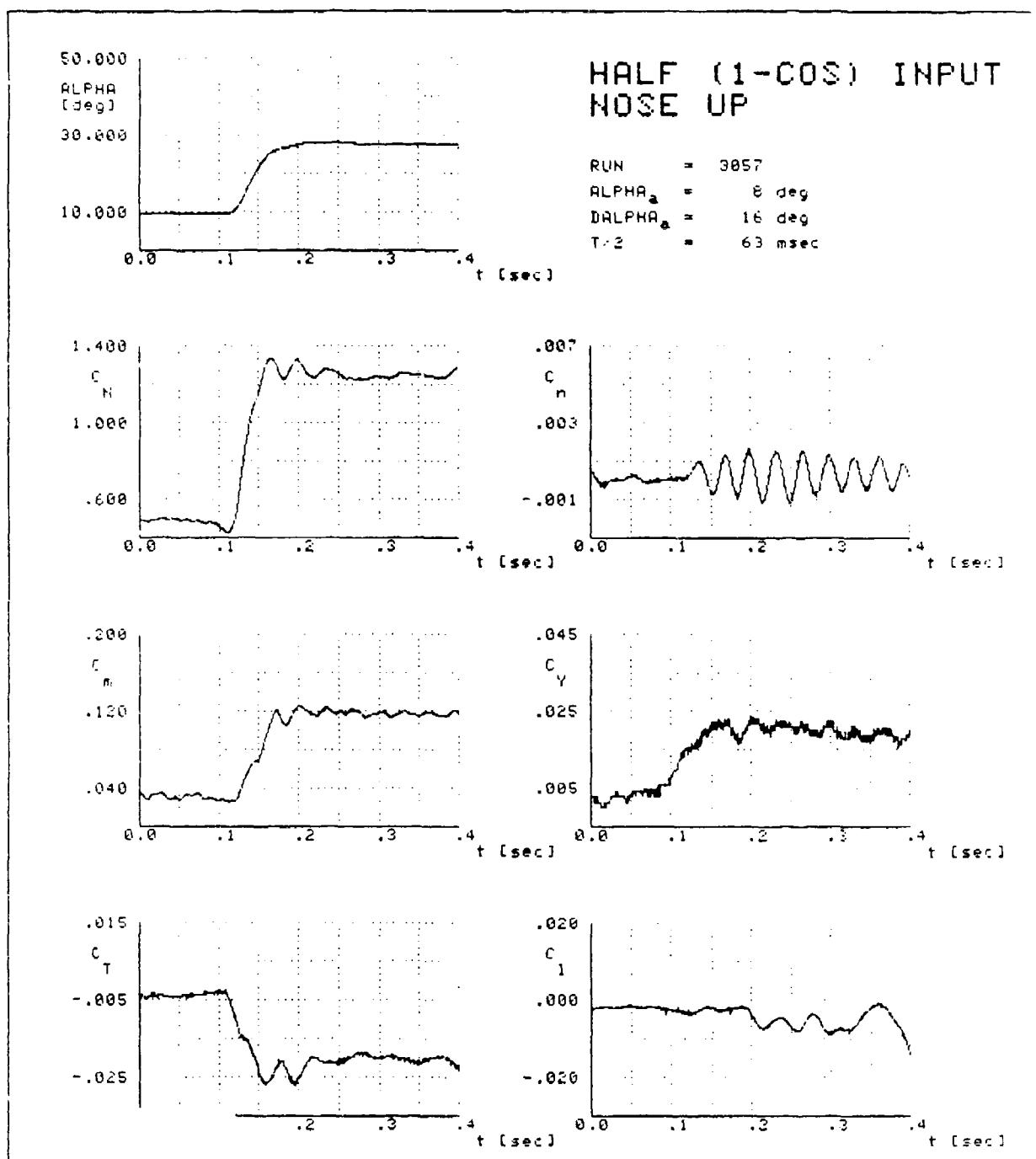






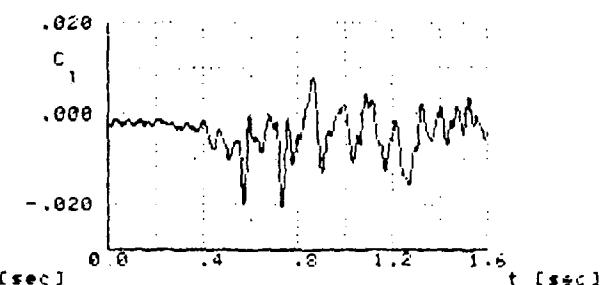
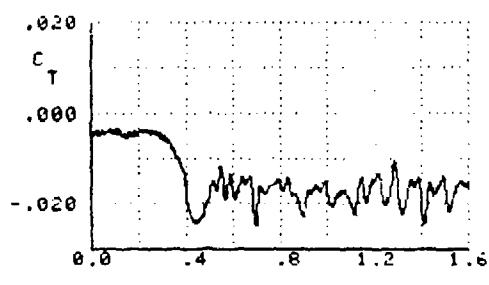
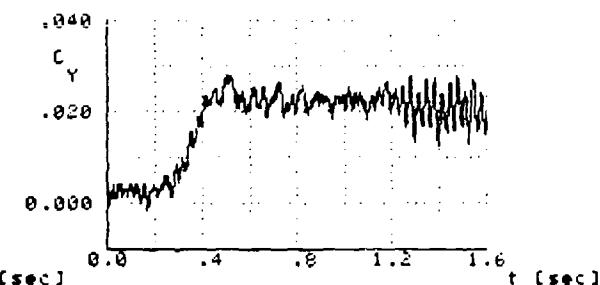
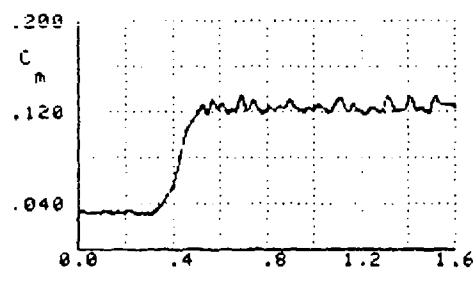
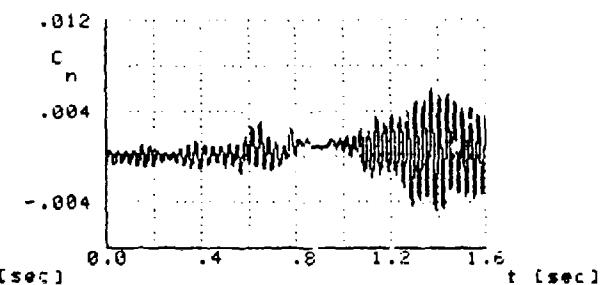
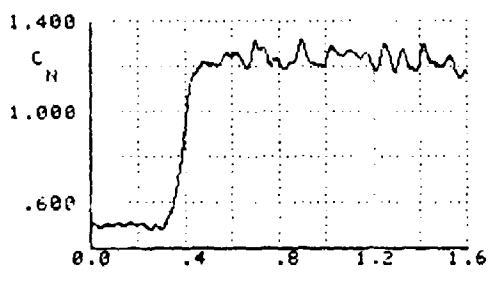
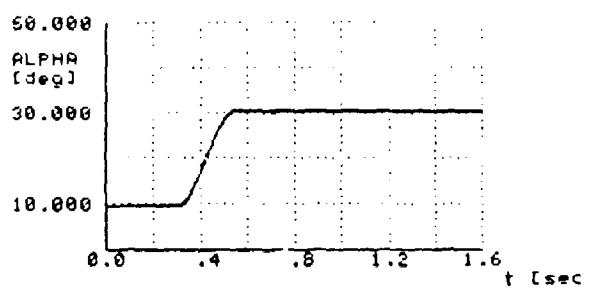


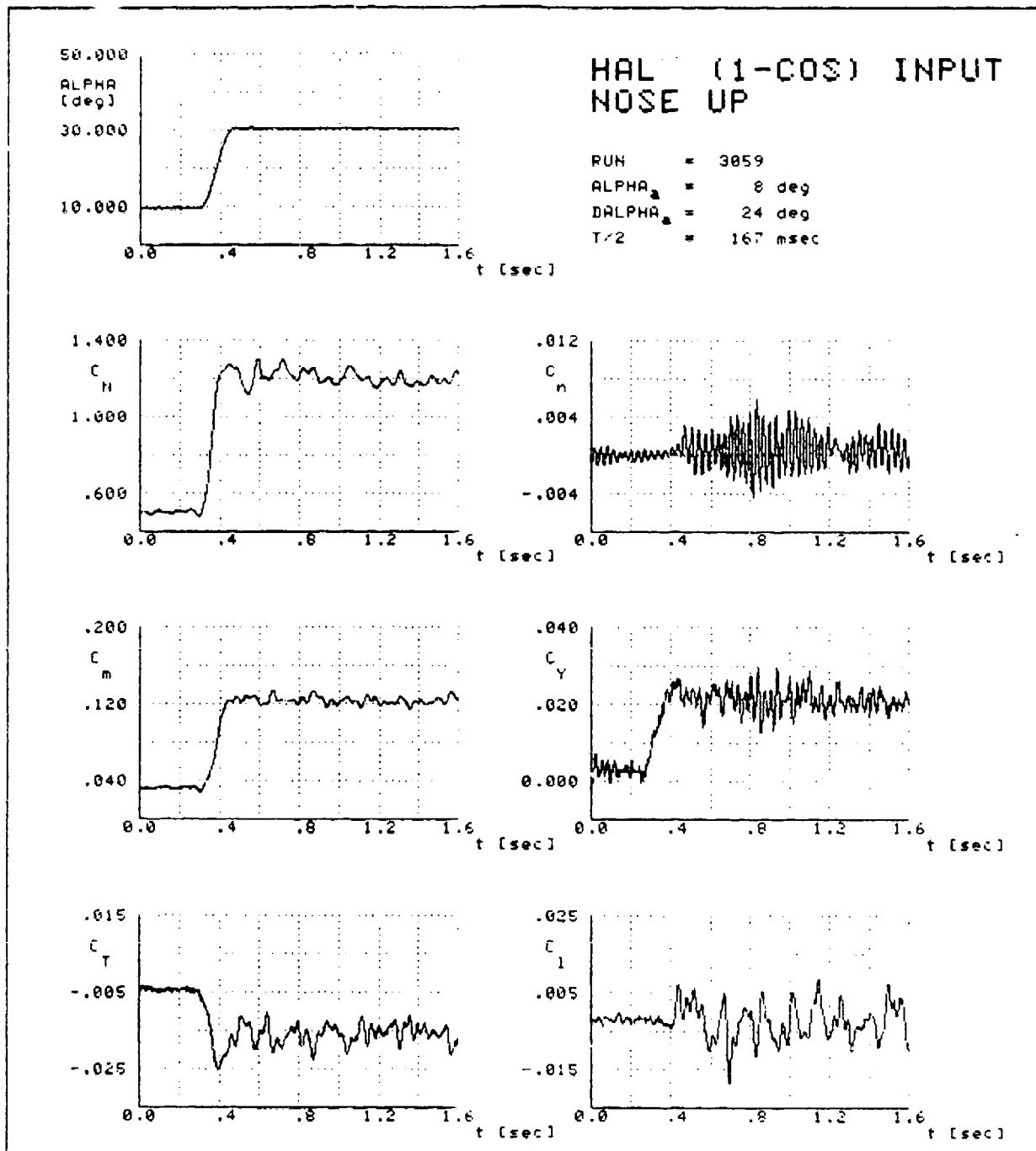


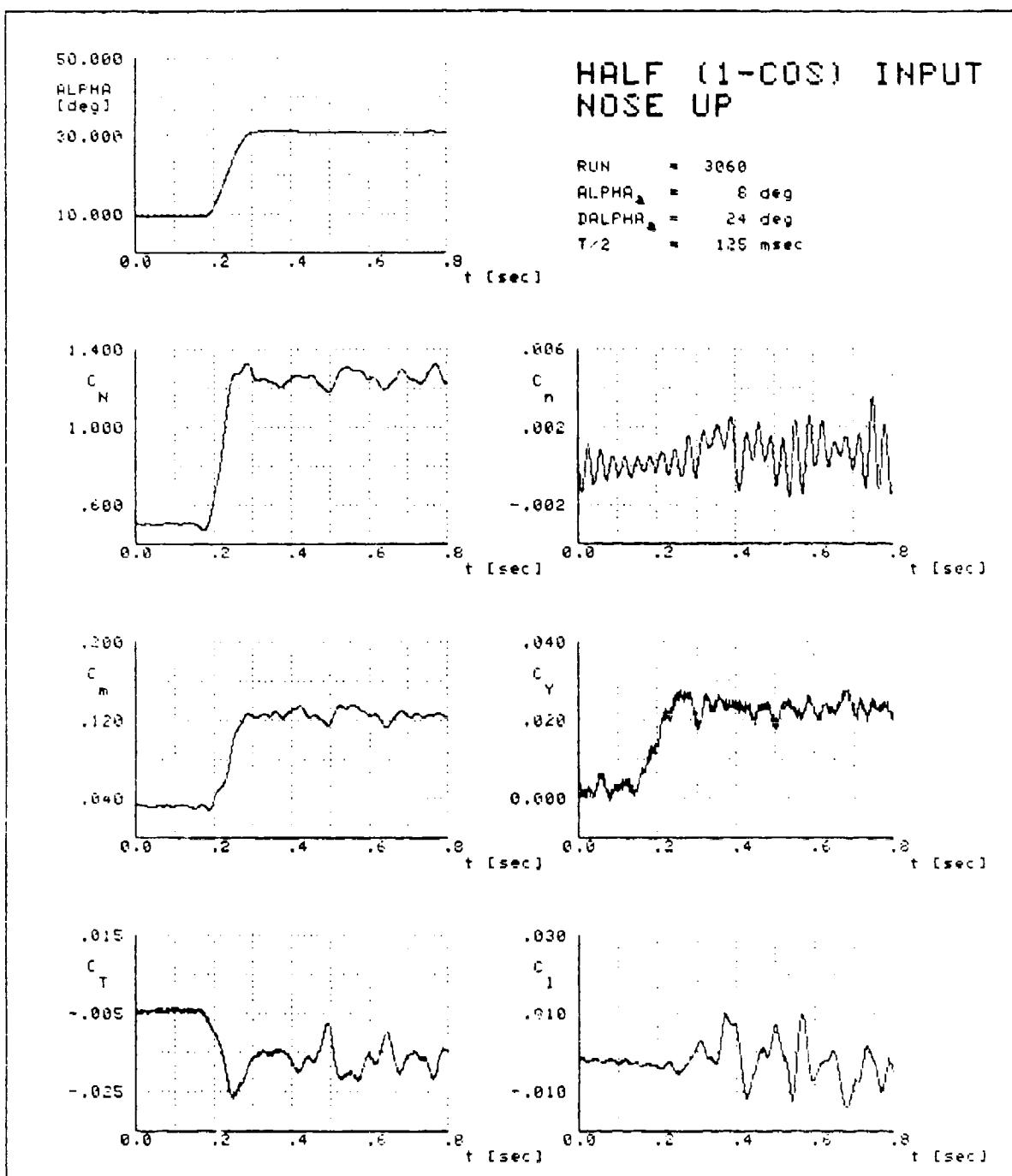


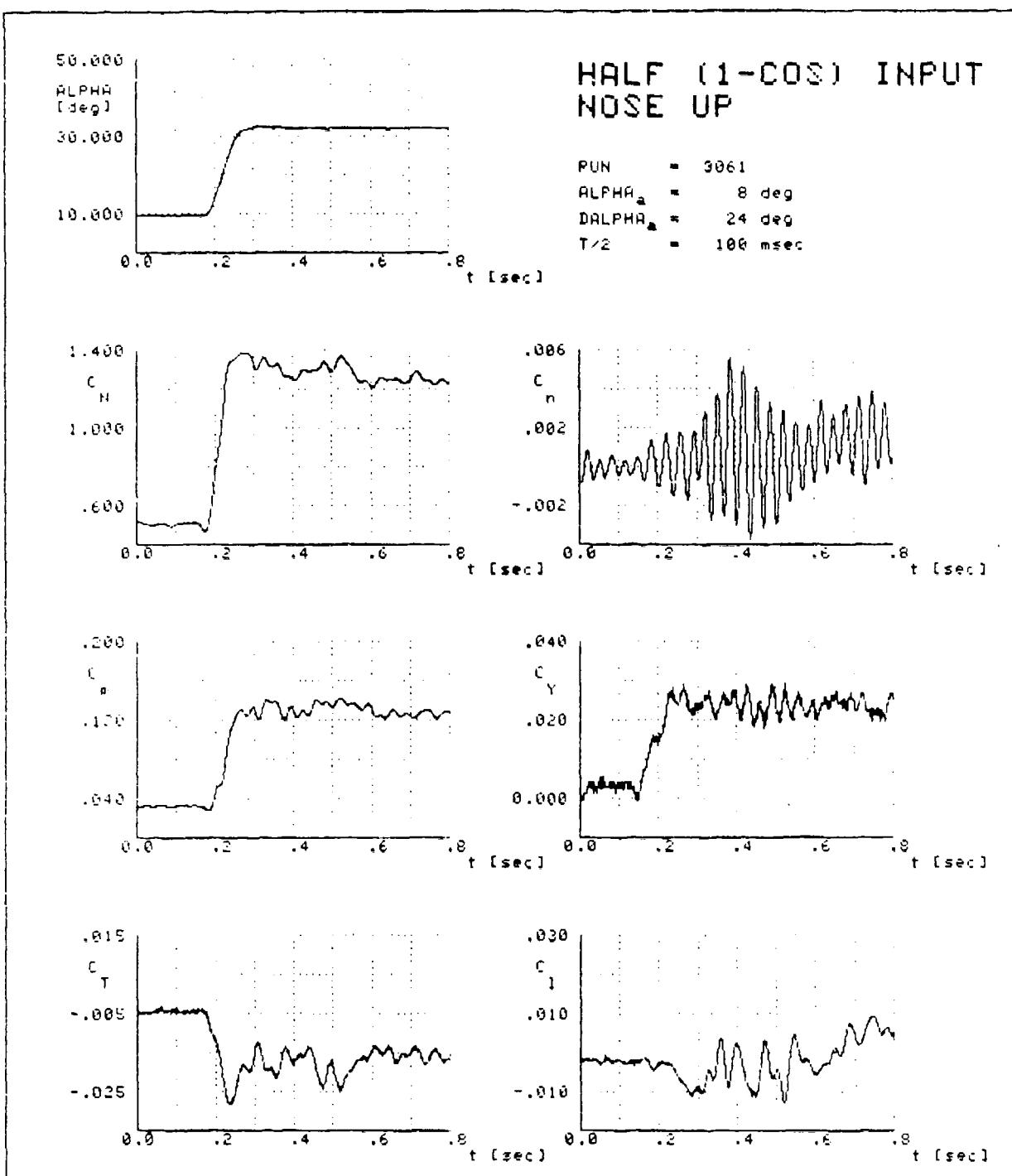
HALF (1-COS) INPUT
NOSE UP

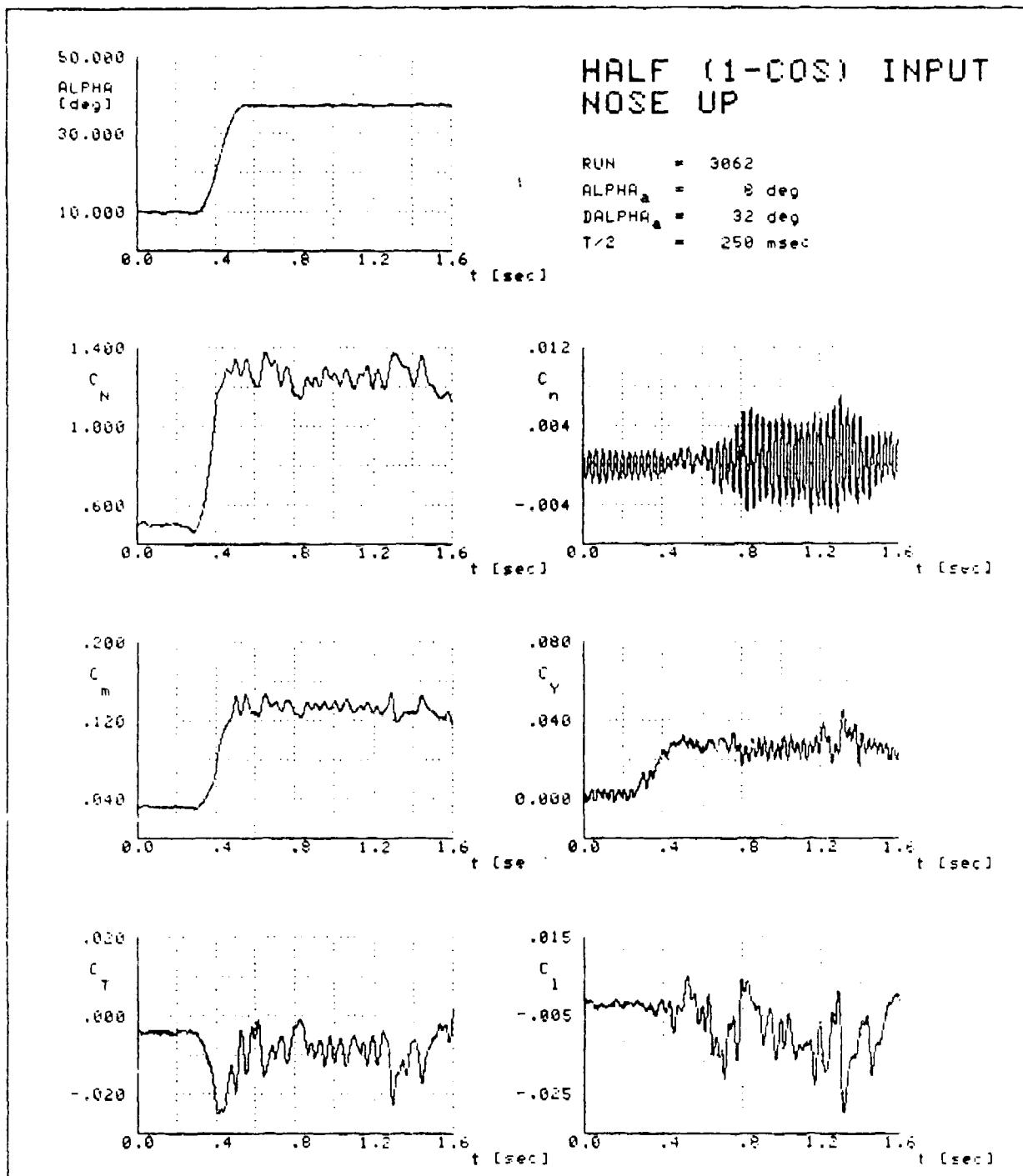
RUN = 3058
 ALPHA_a = 8 deg
 DALPHA_a = 24 deg
 $T/2$ = 258 msec

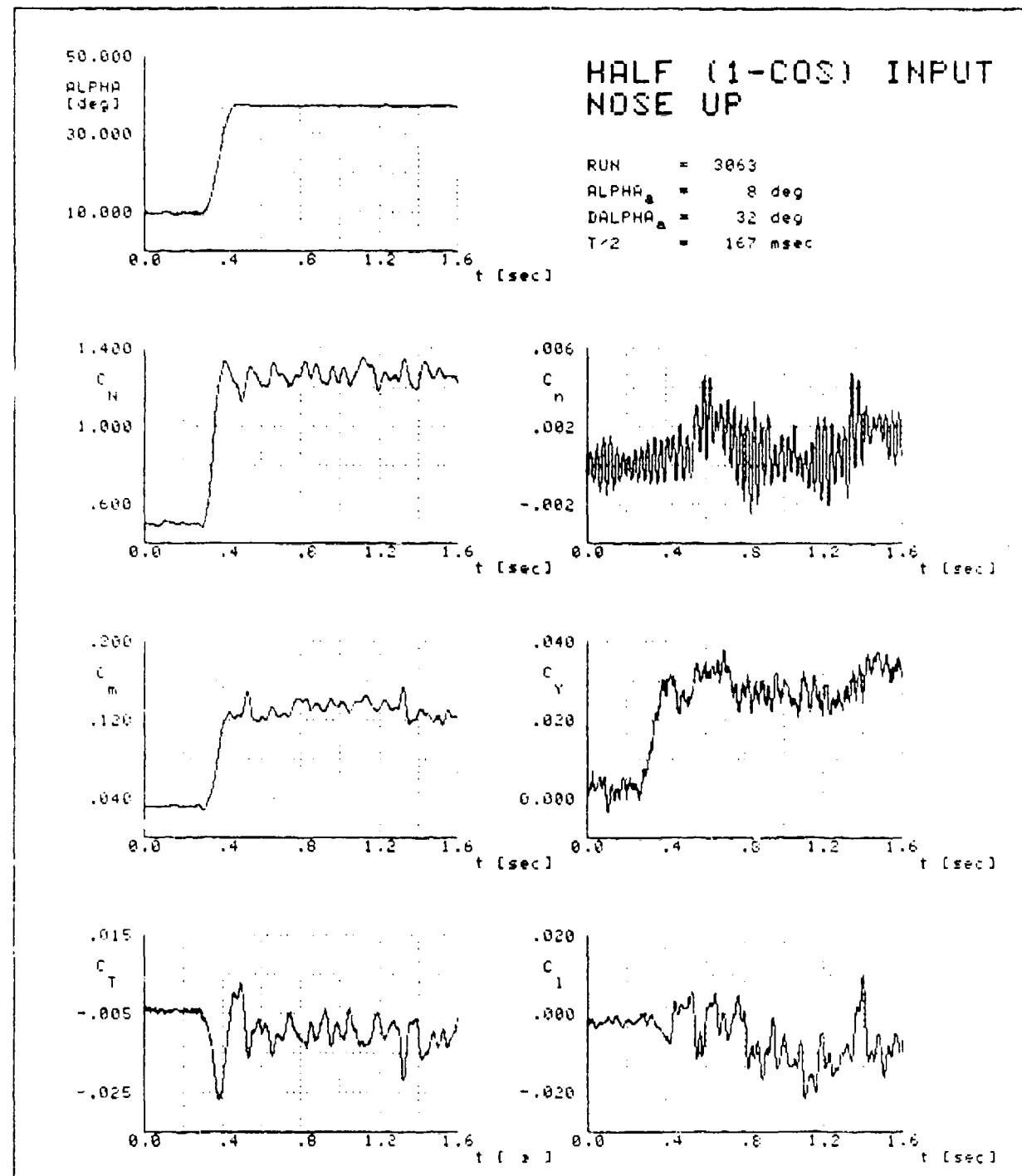


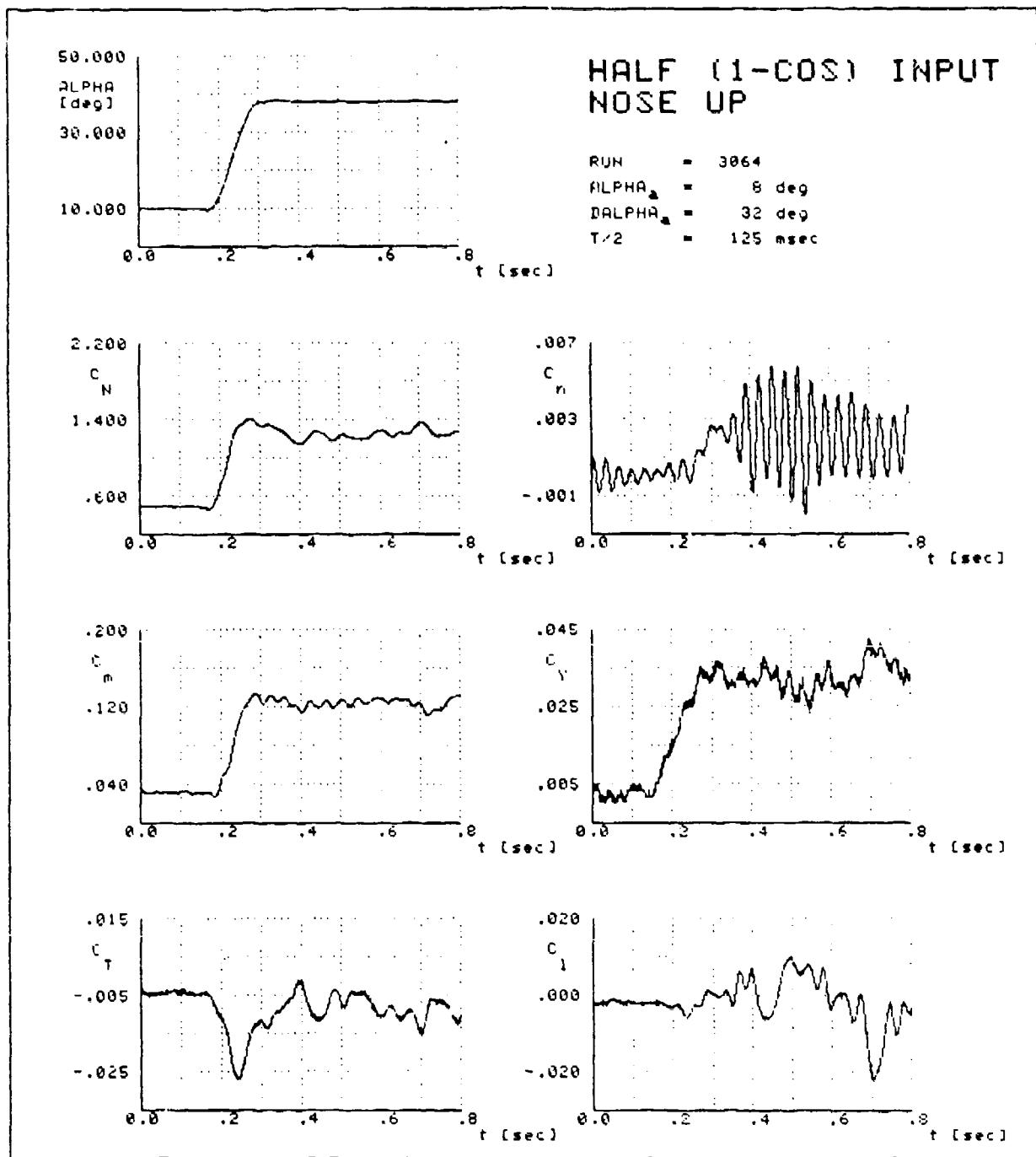


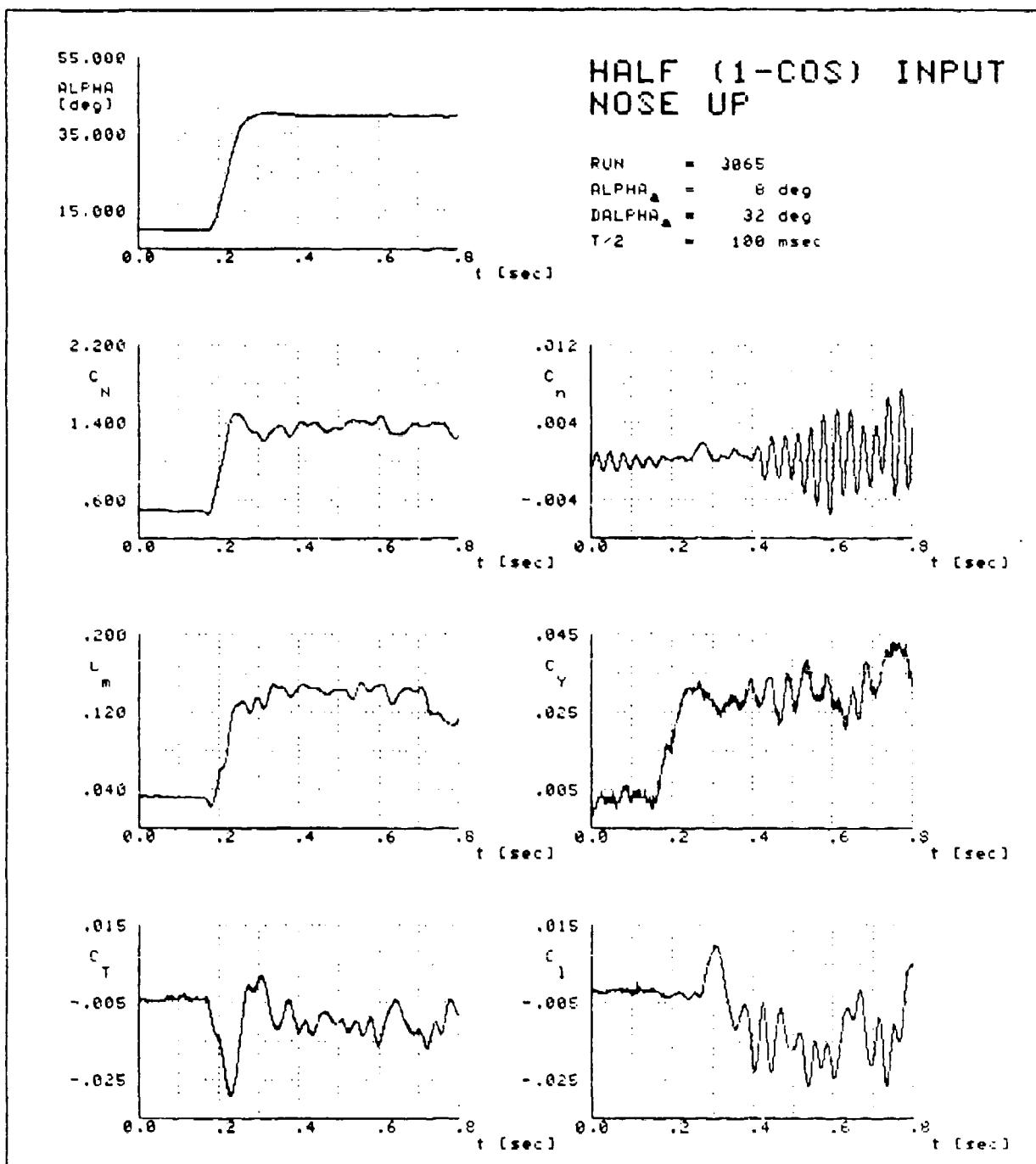


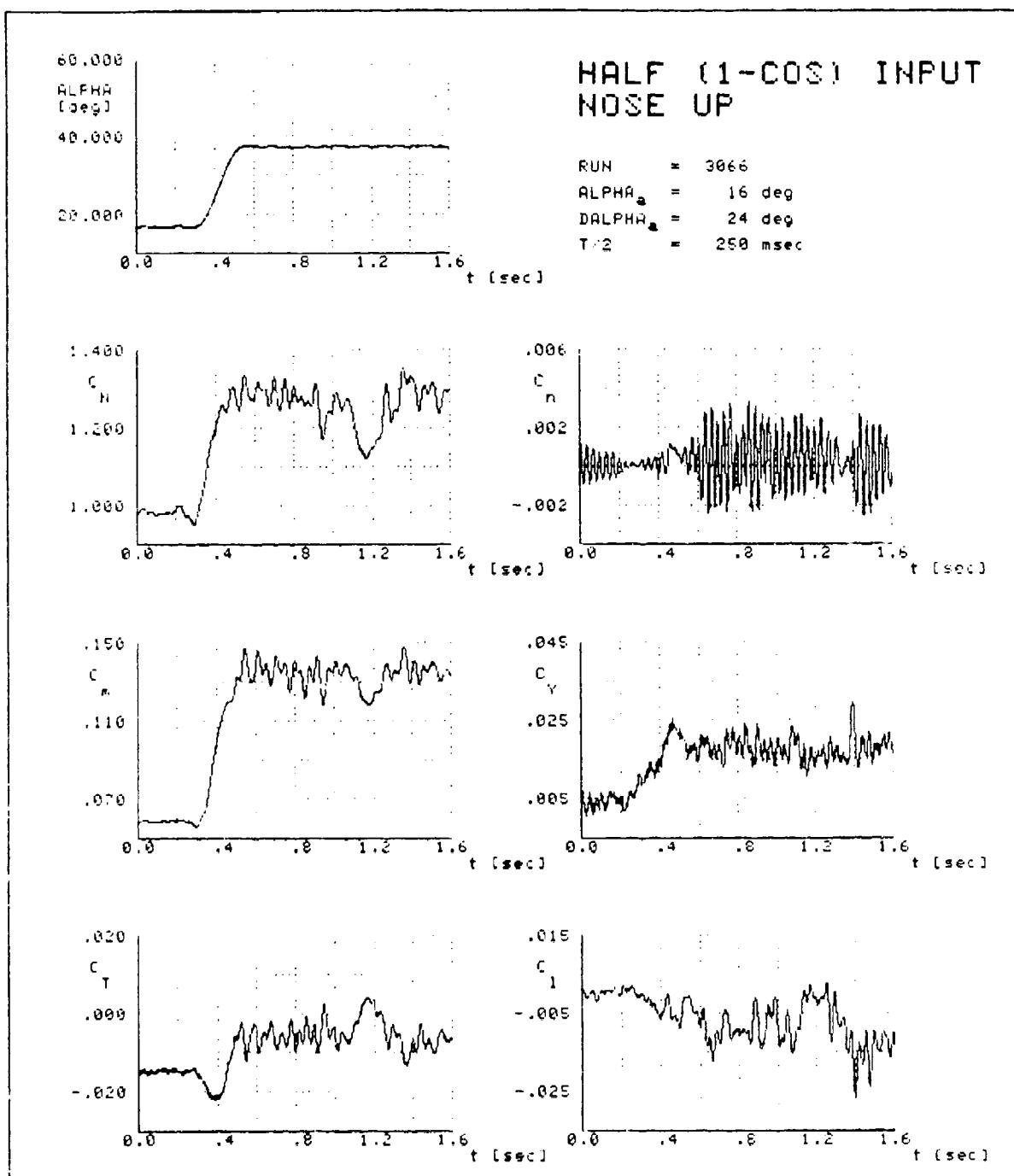


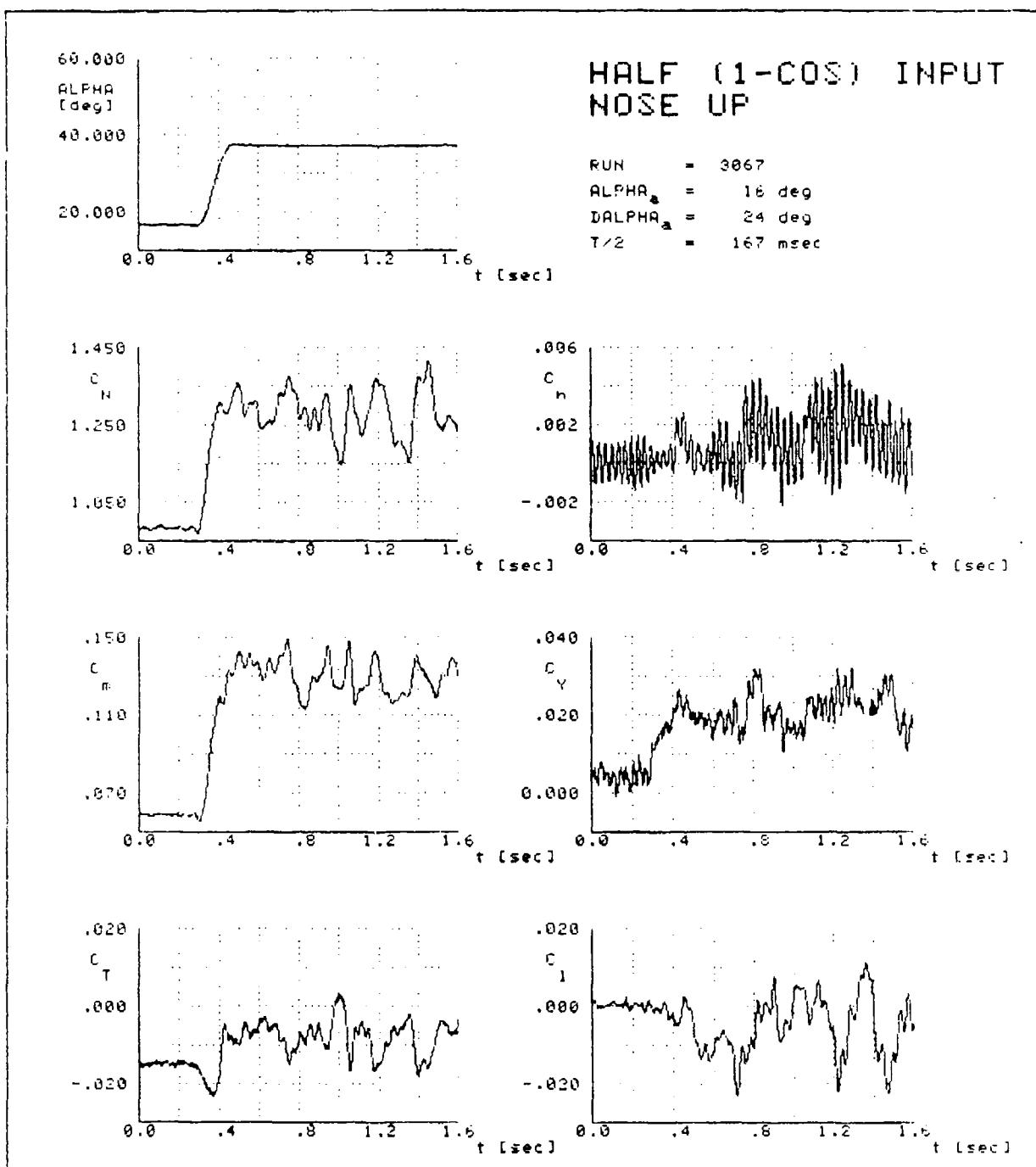


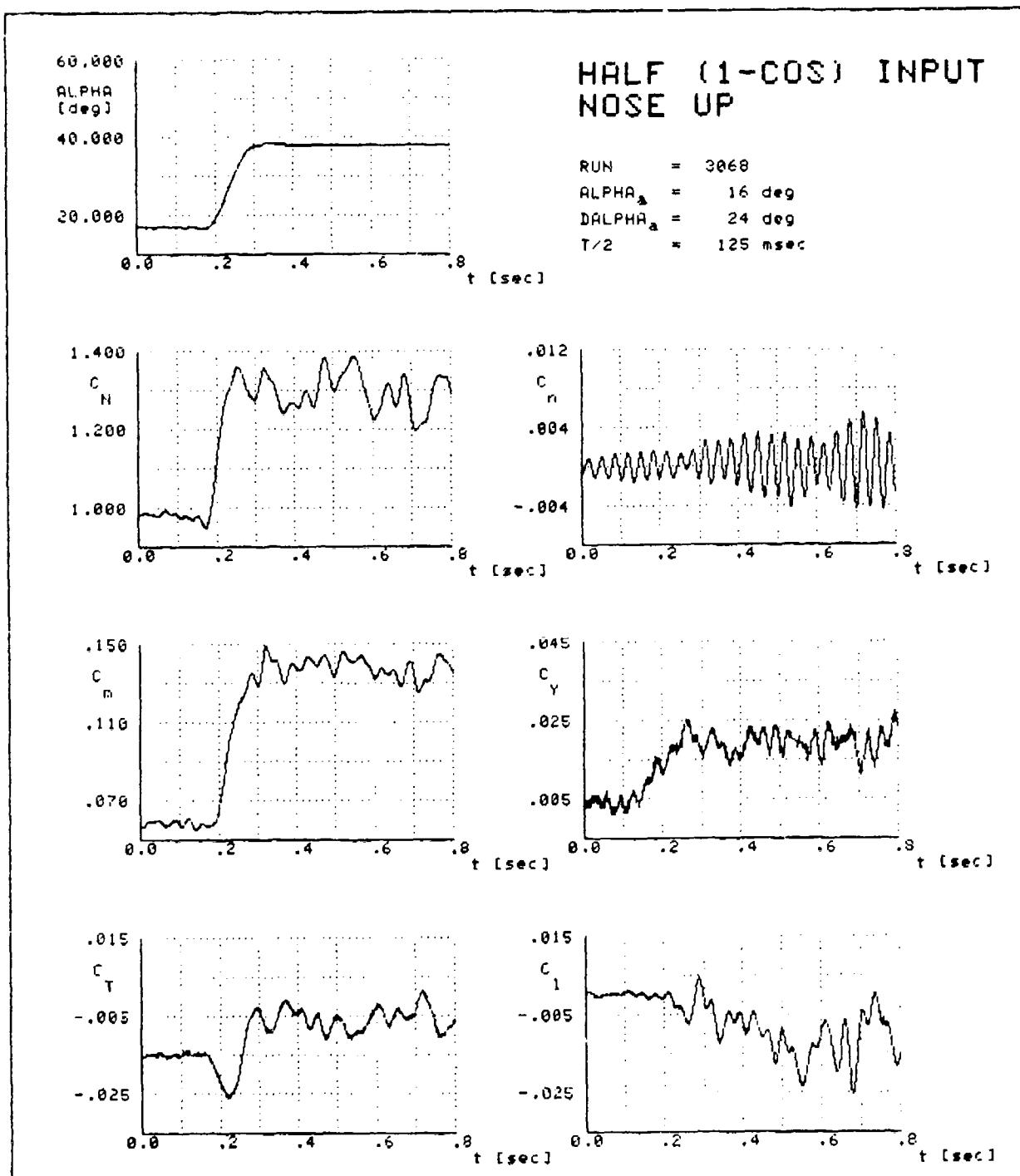


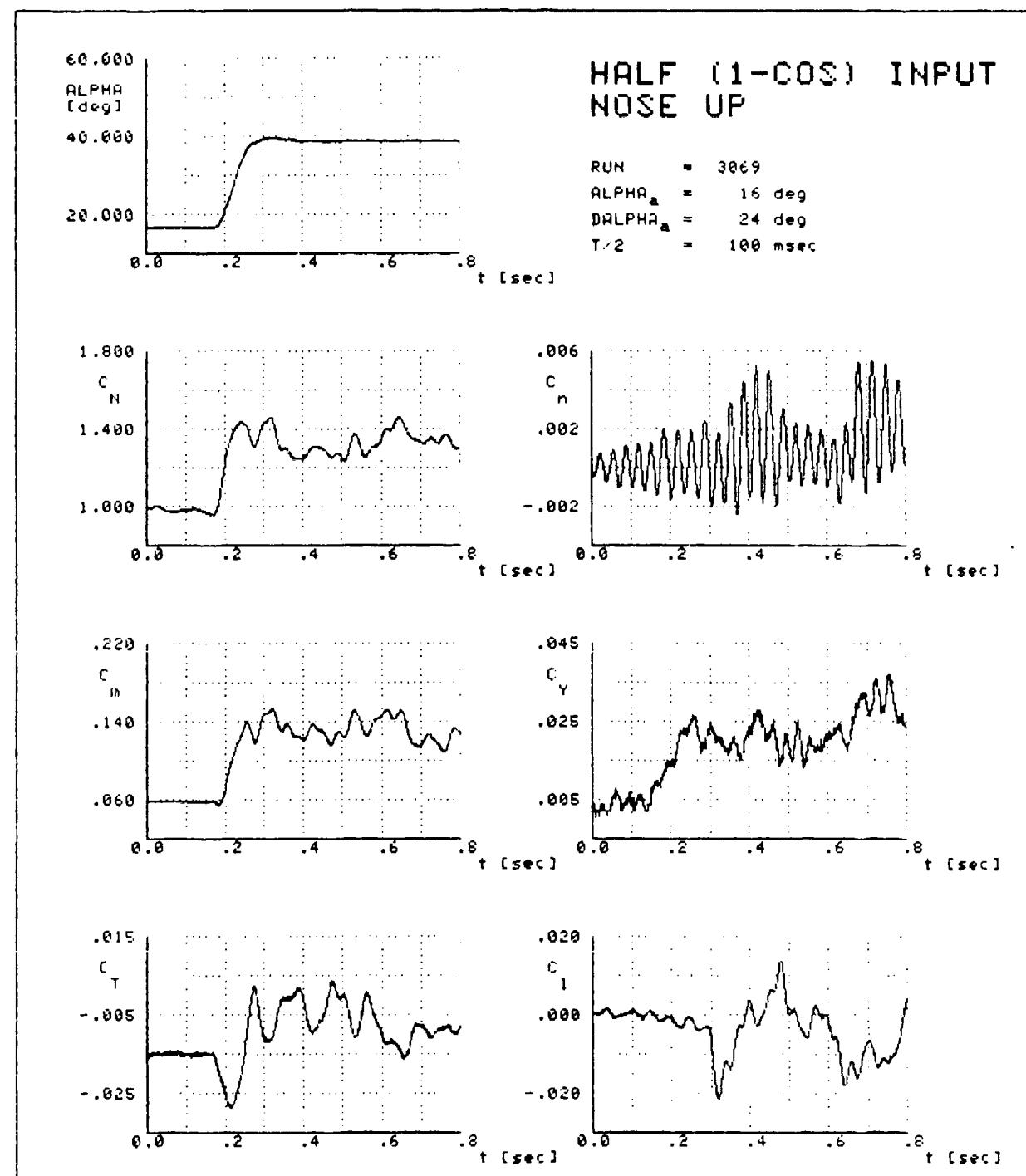


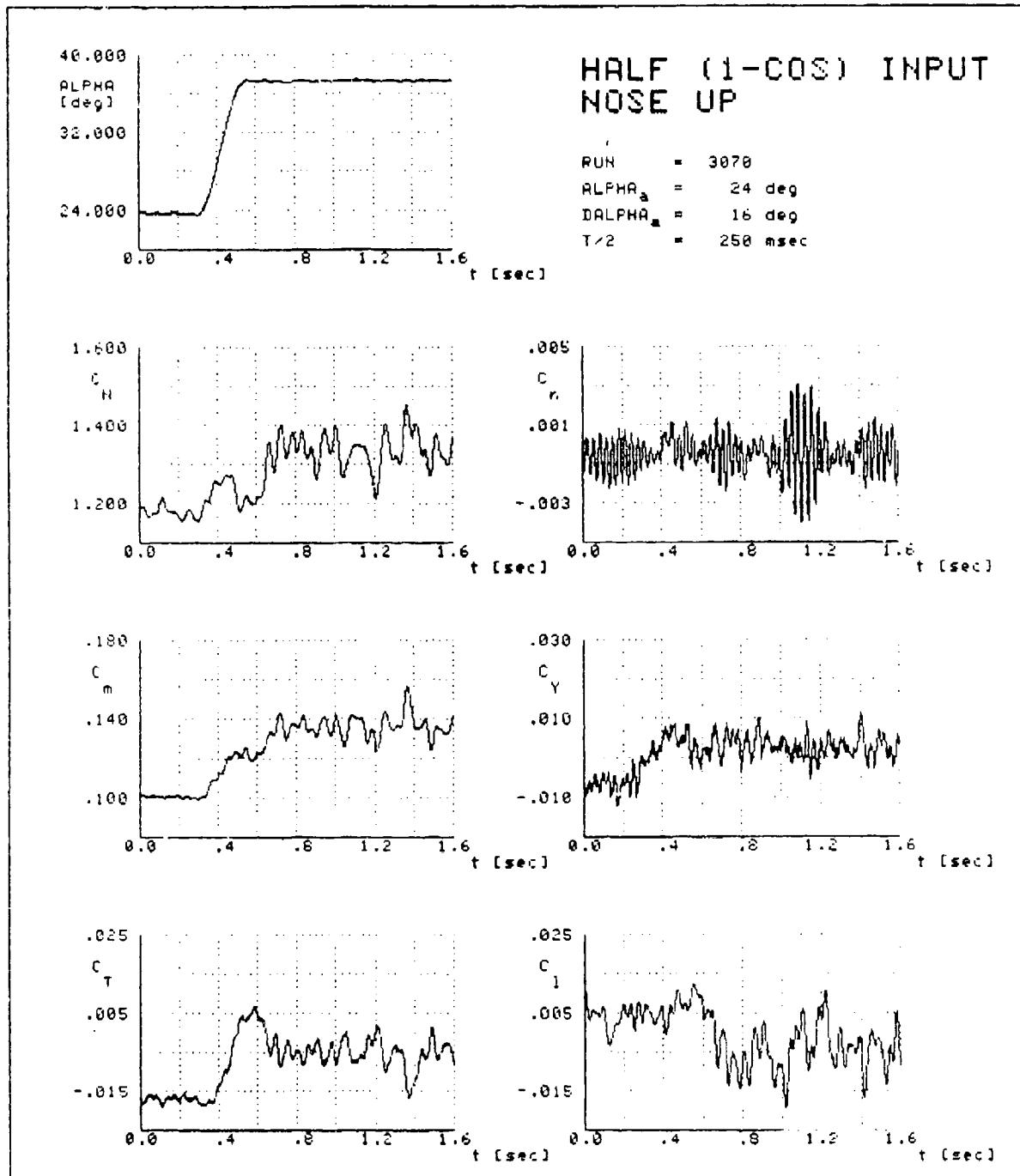


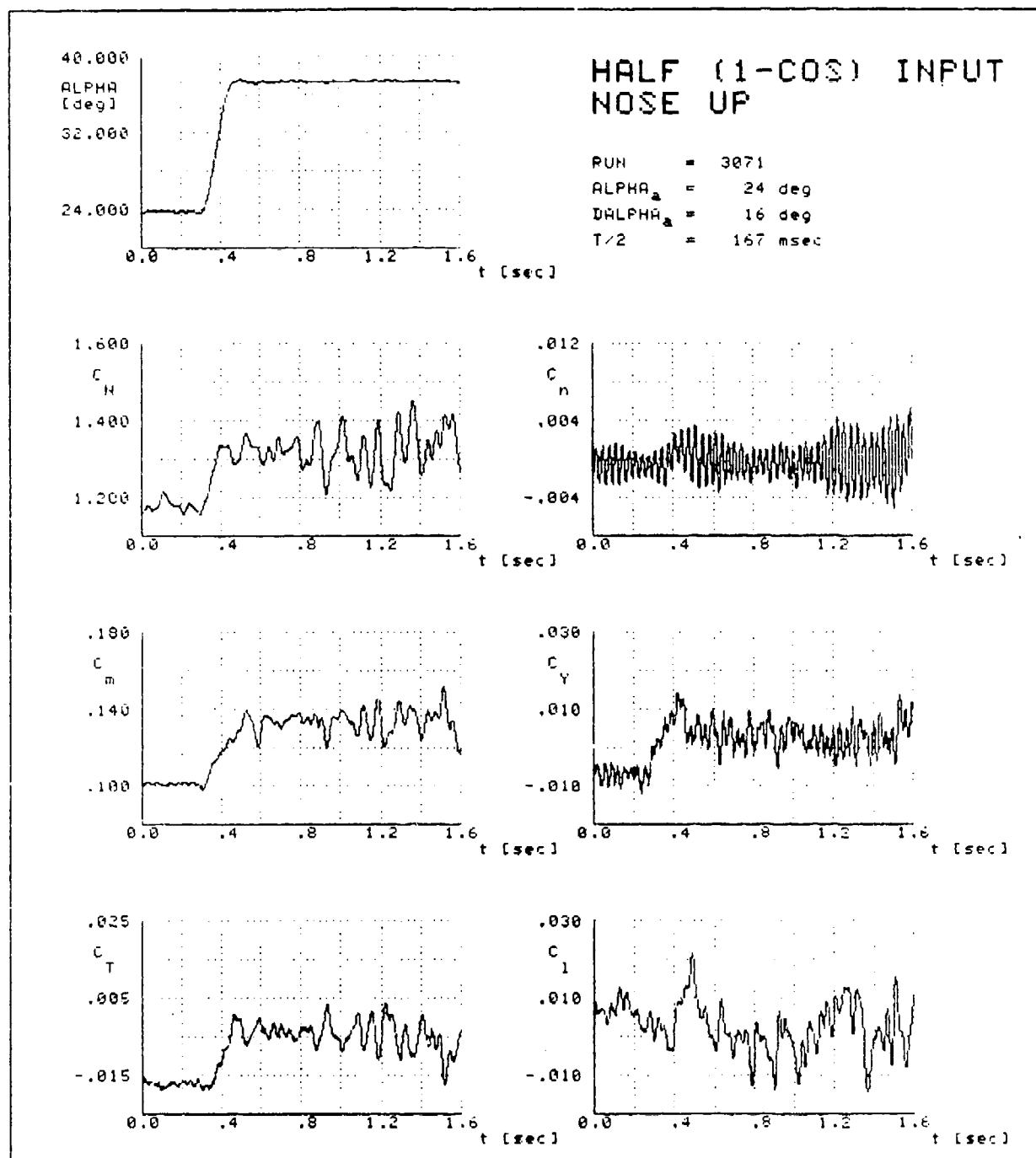


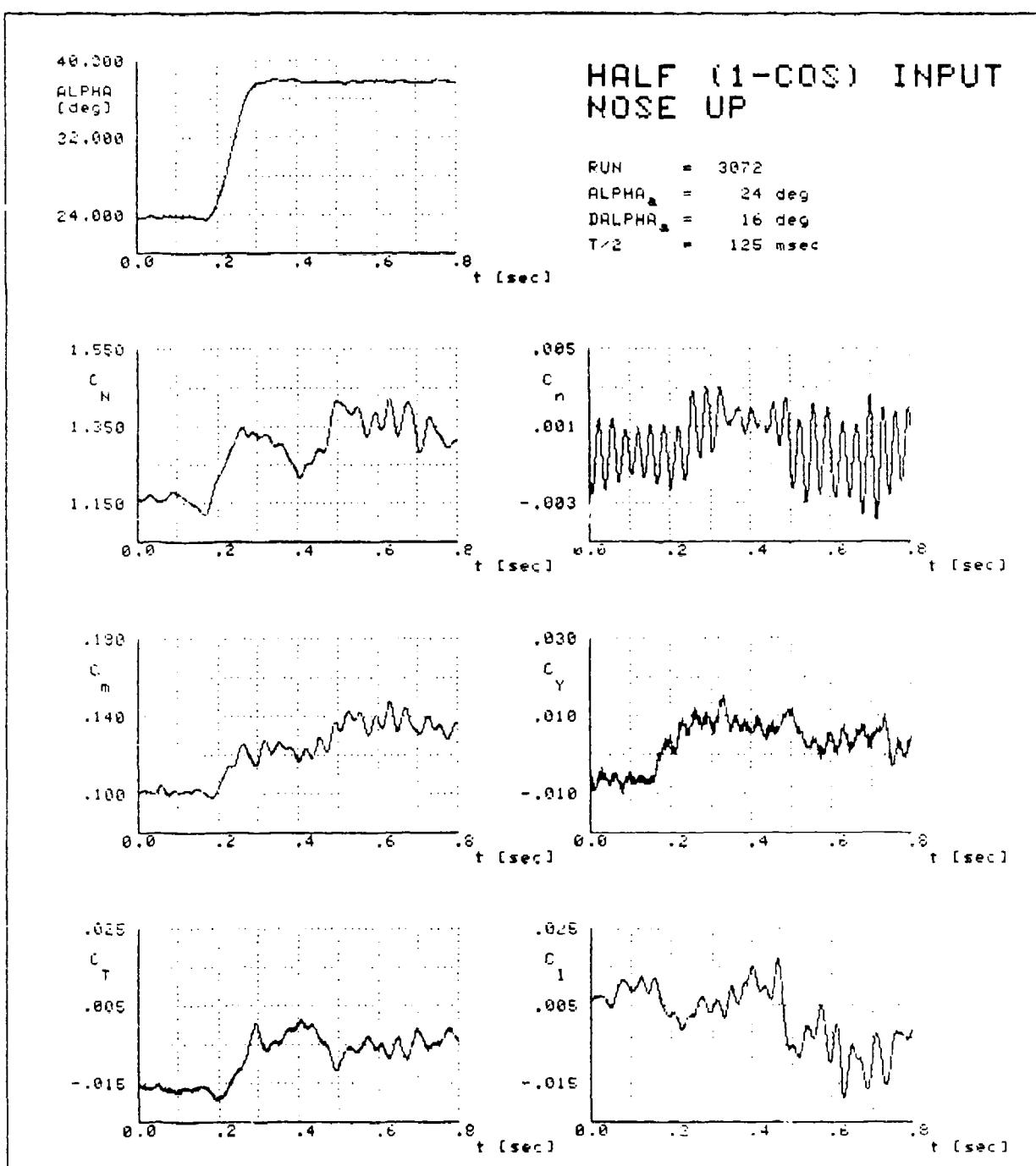


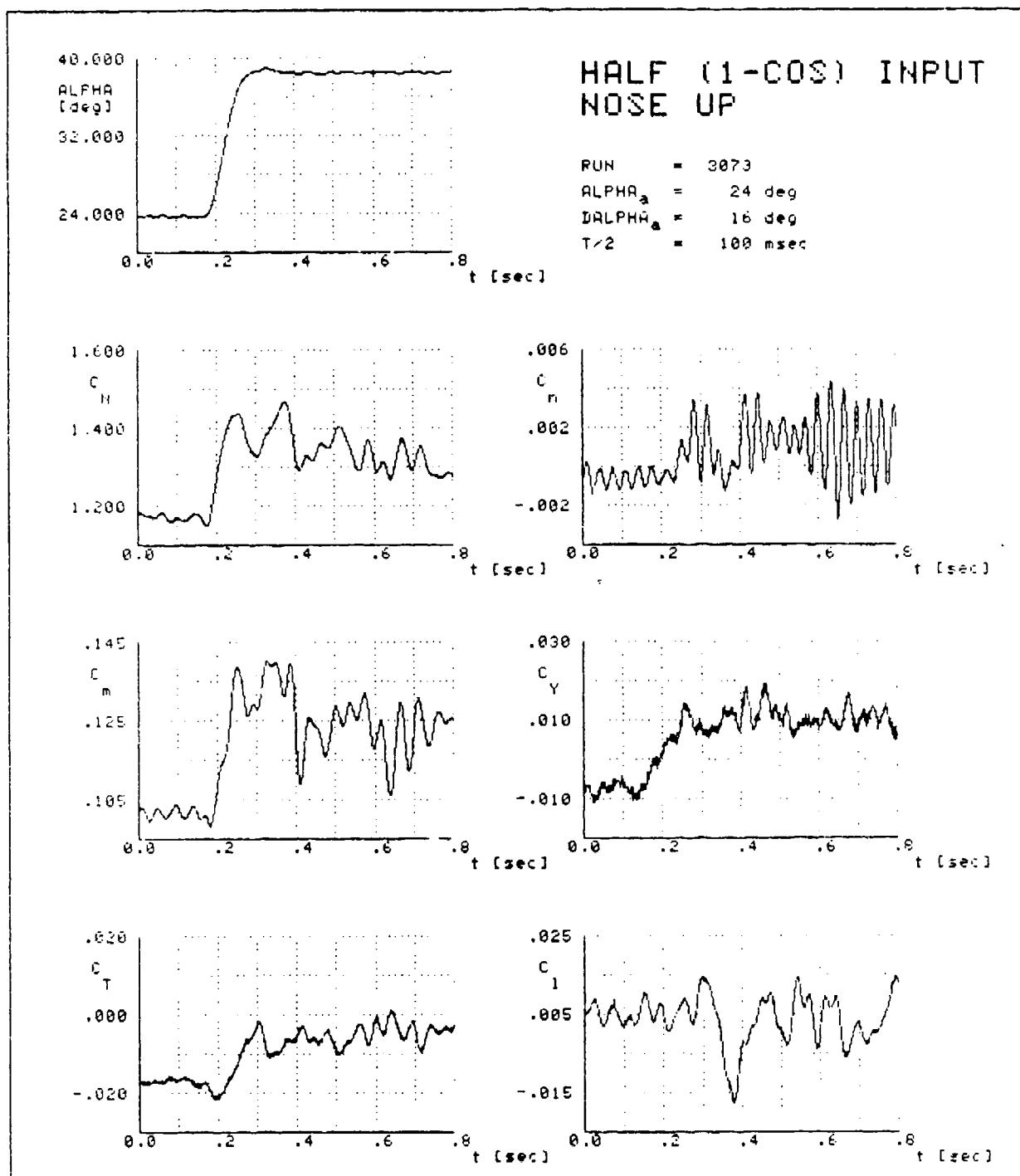


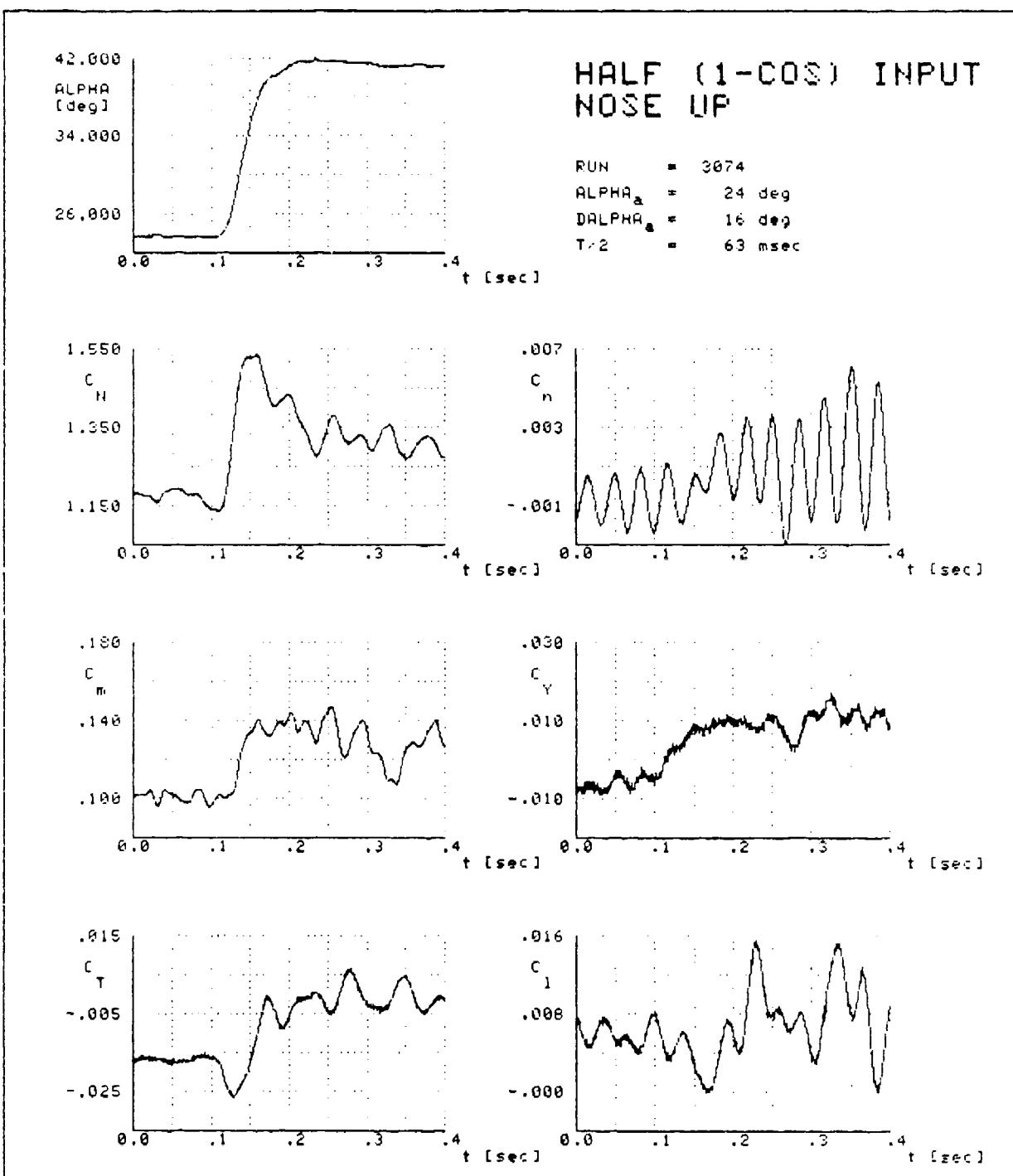


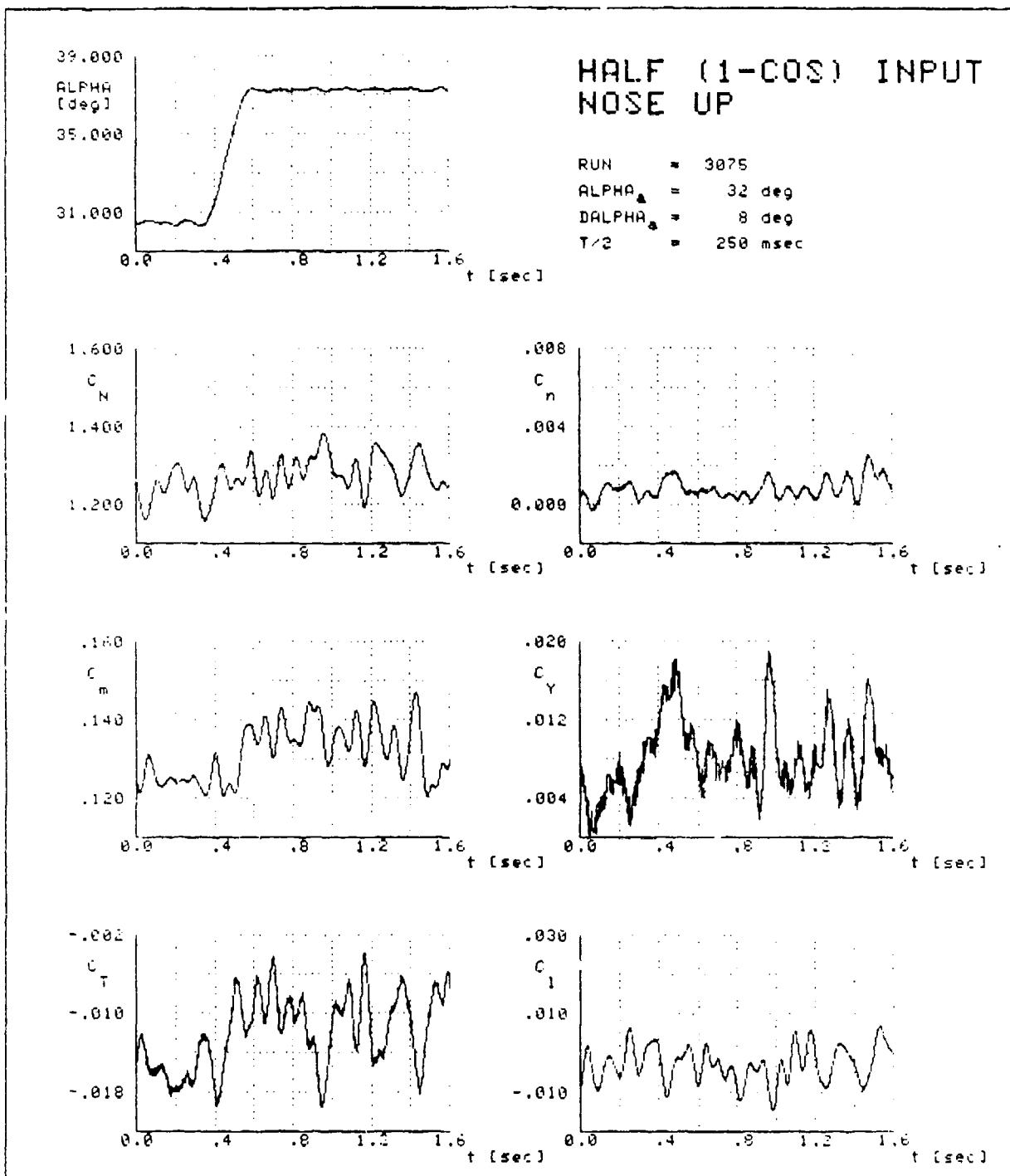


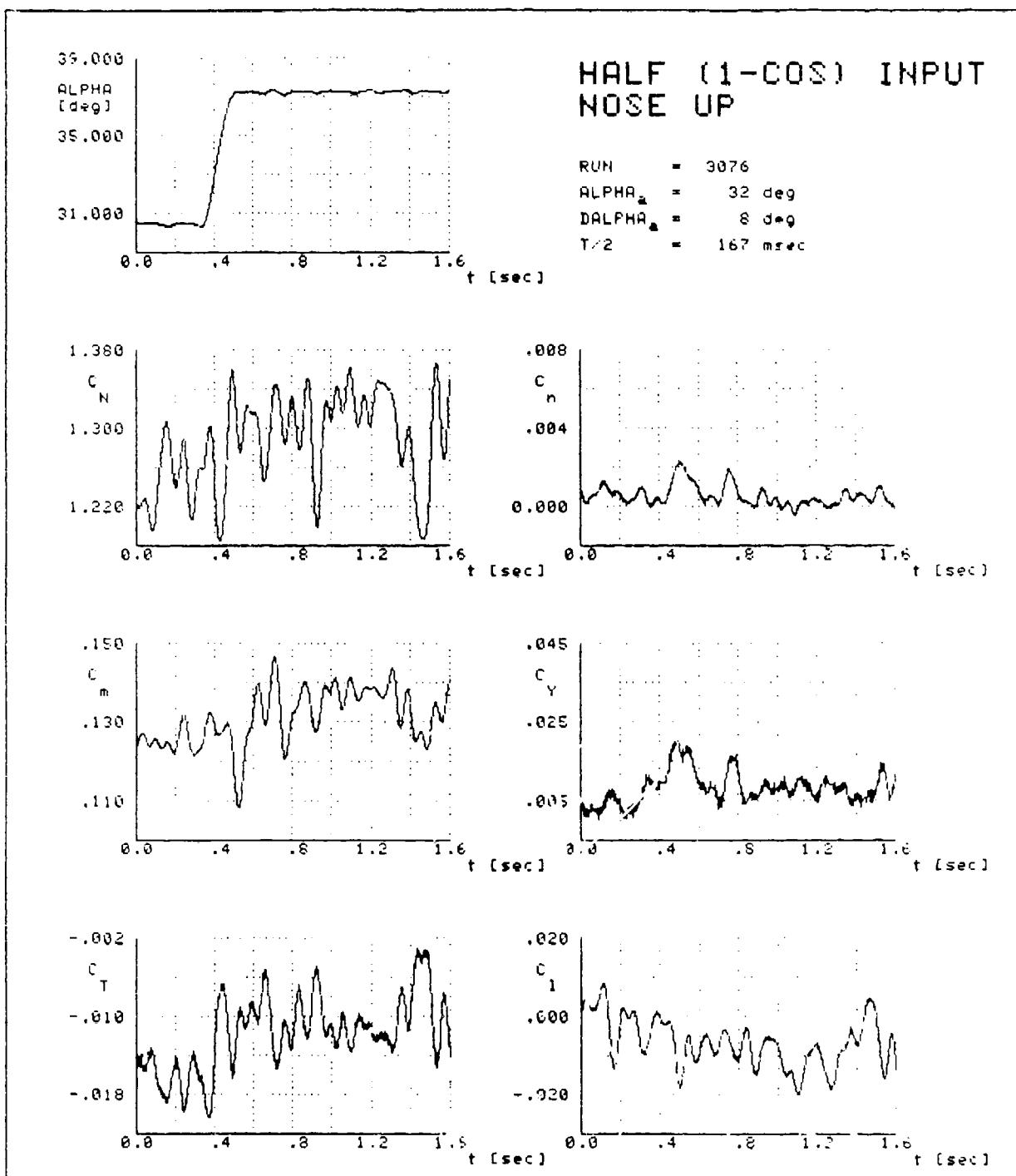


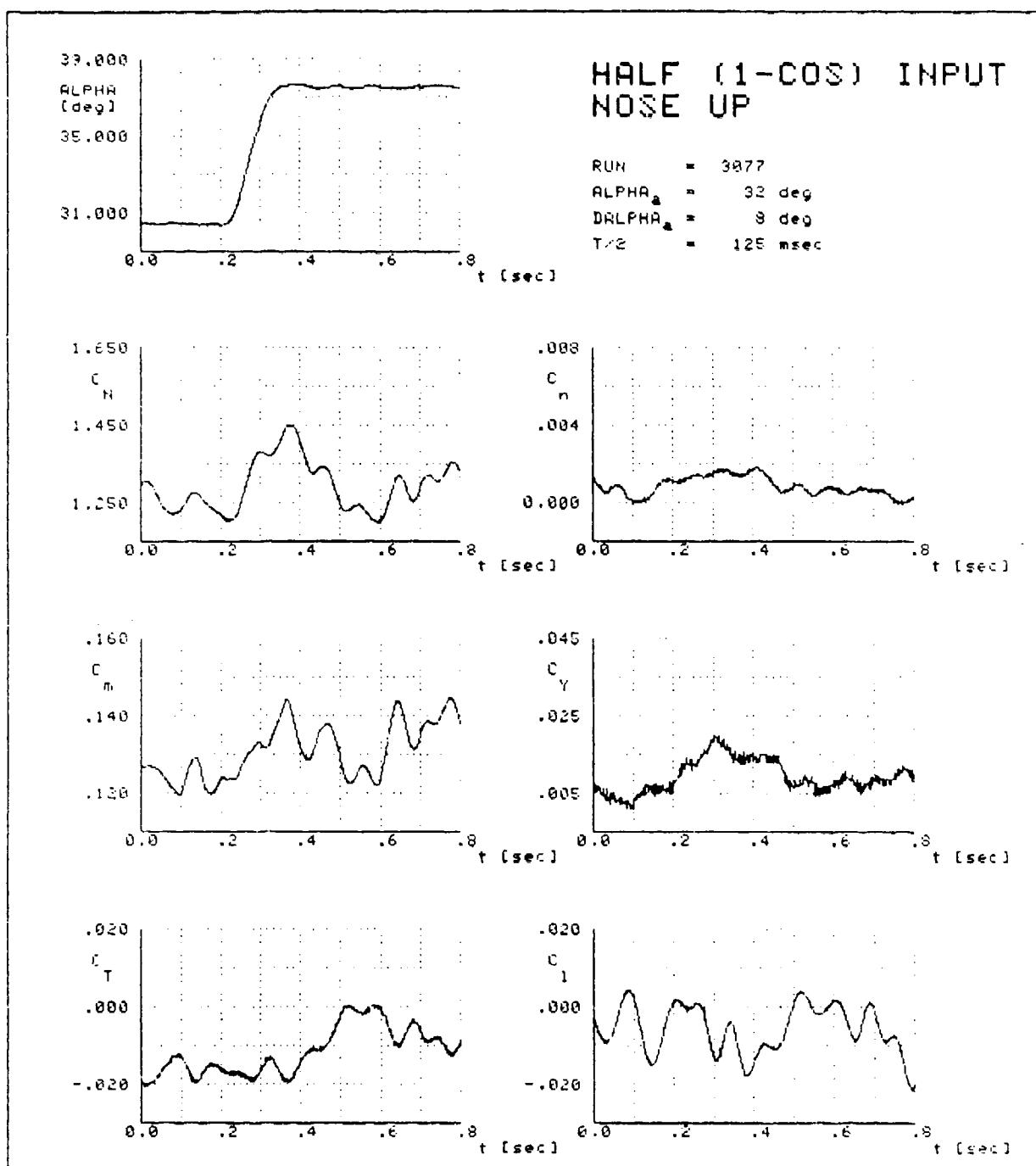


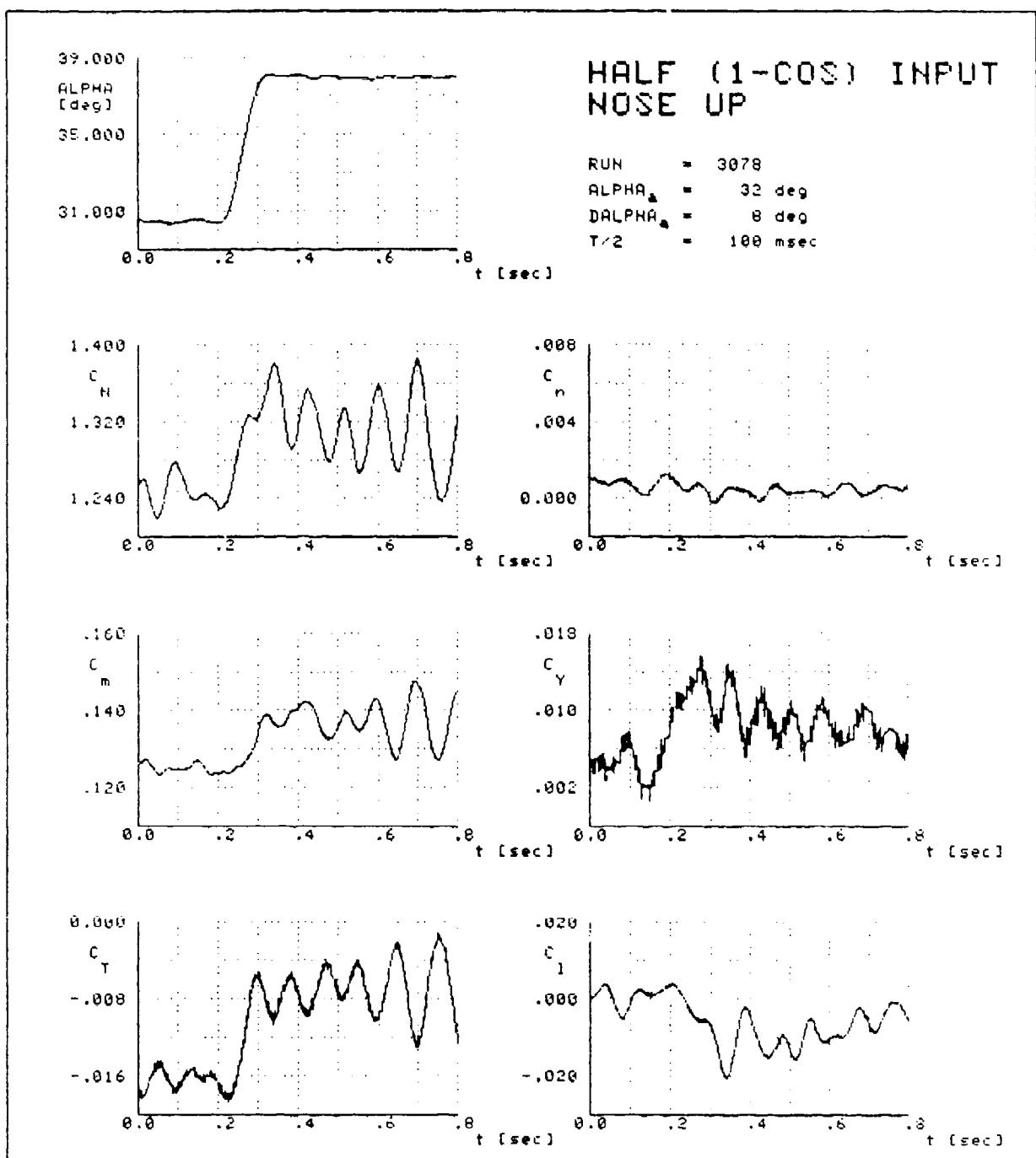


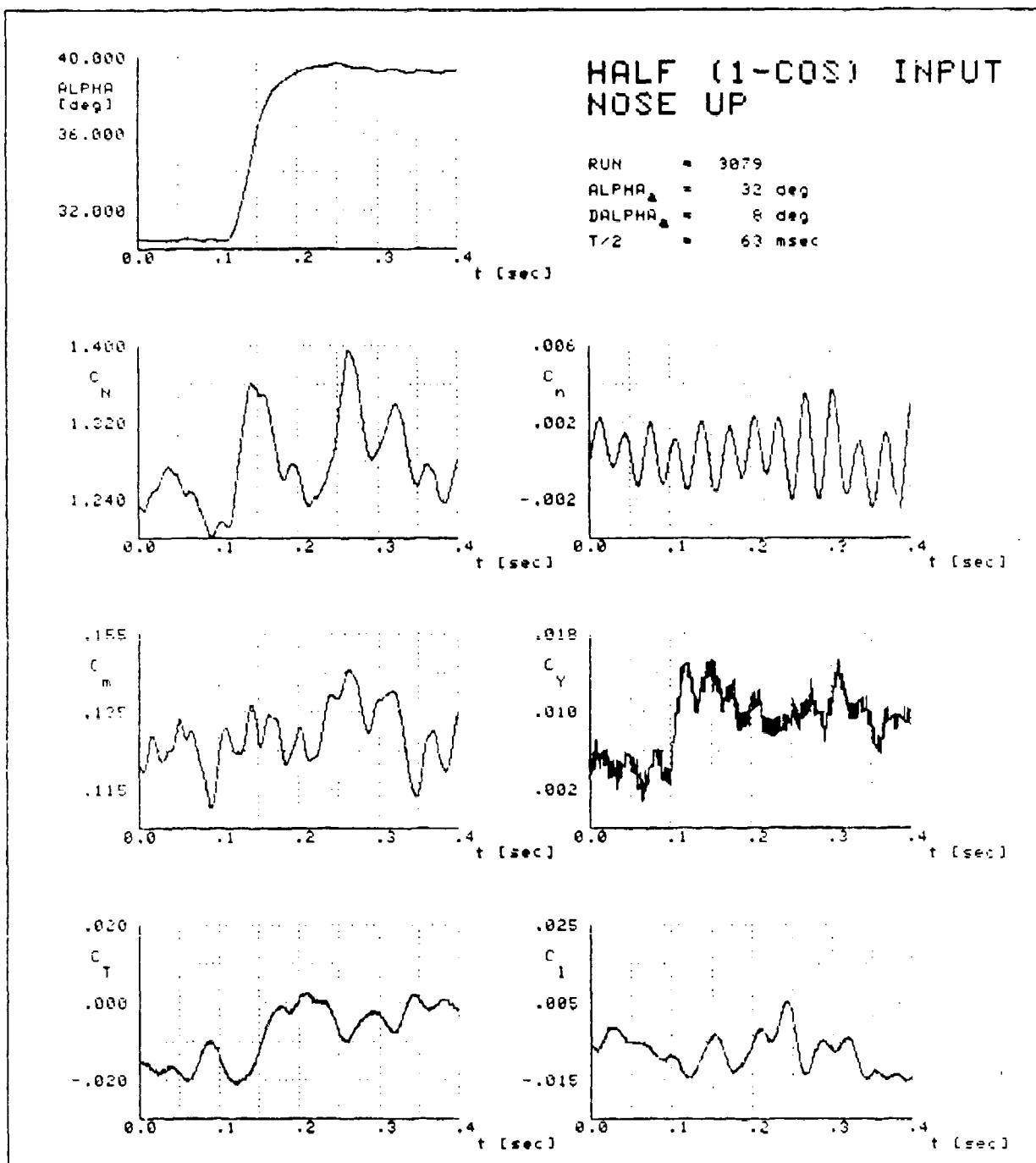


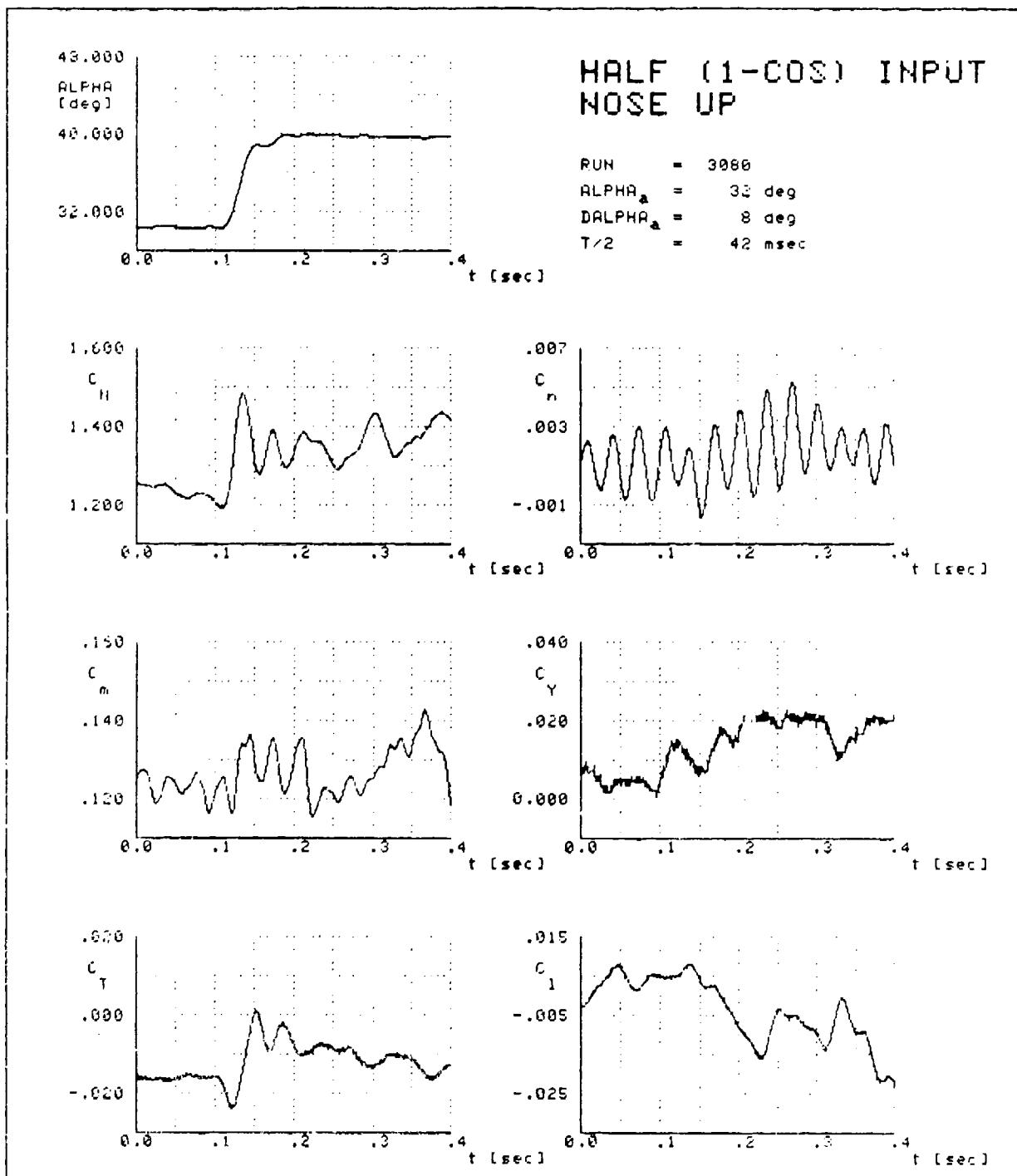


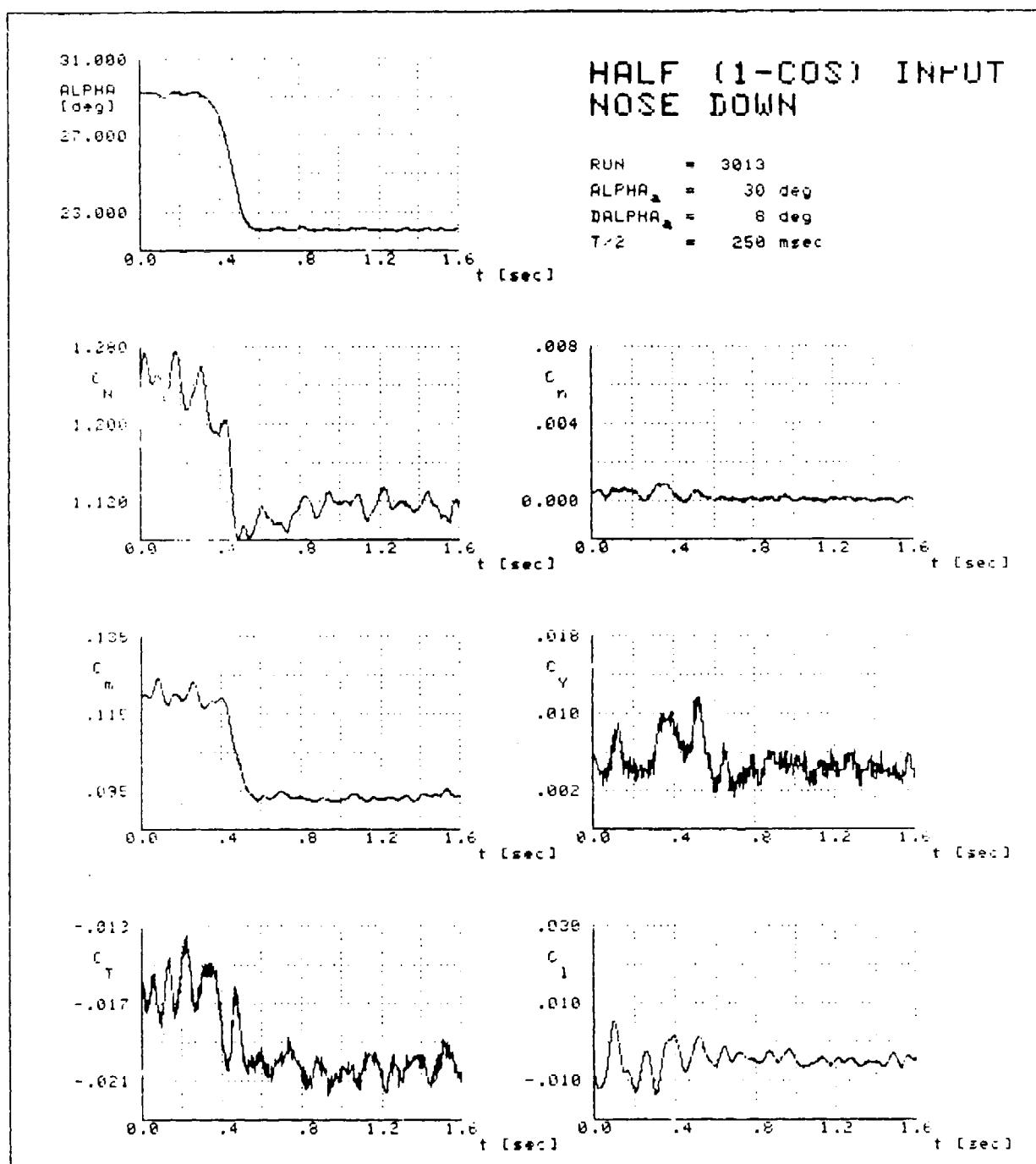


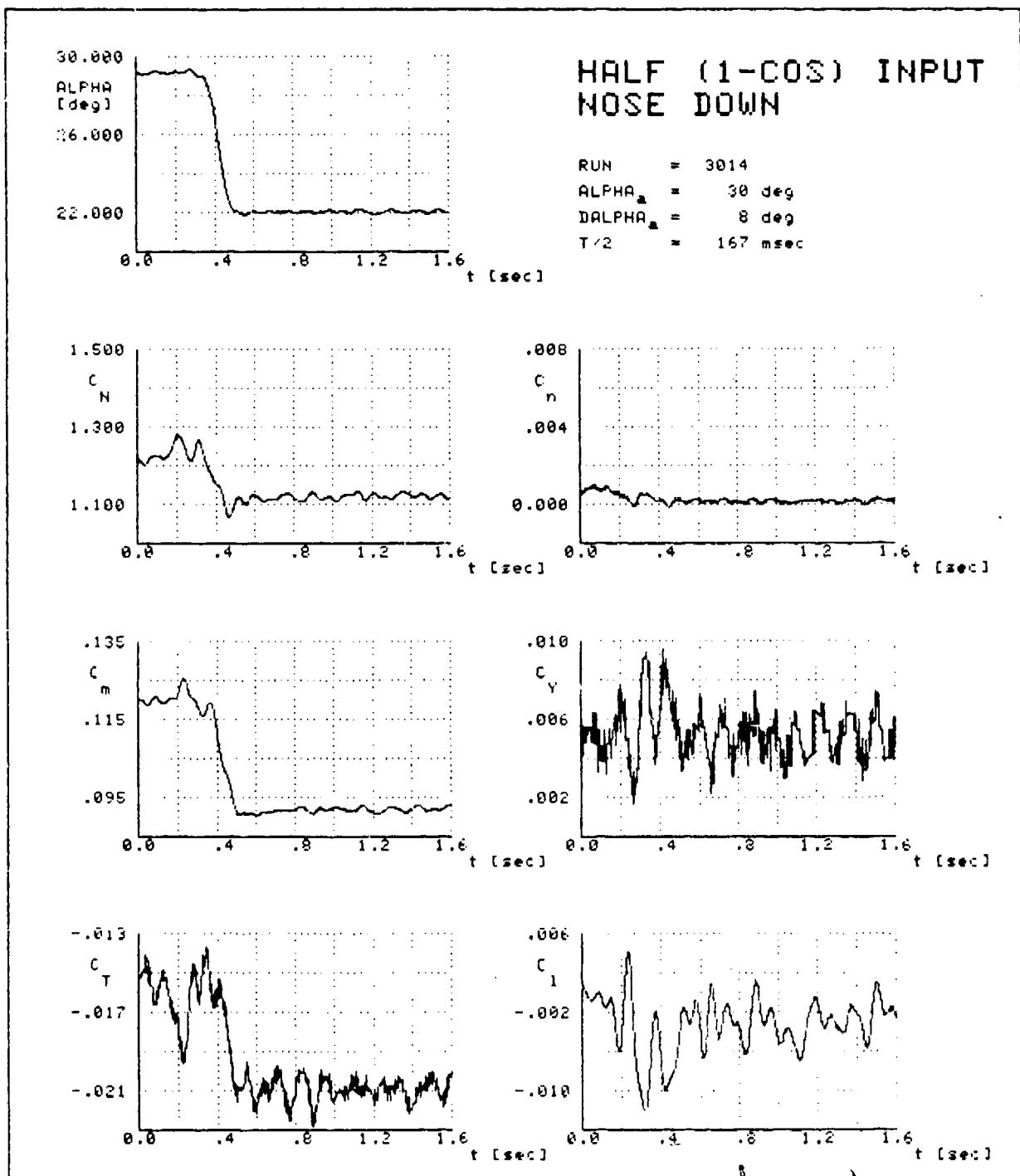


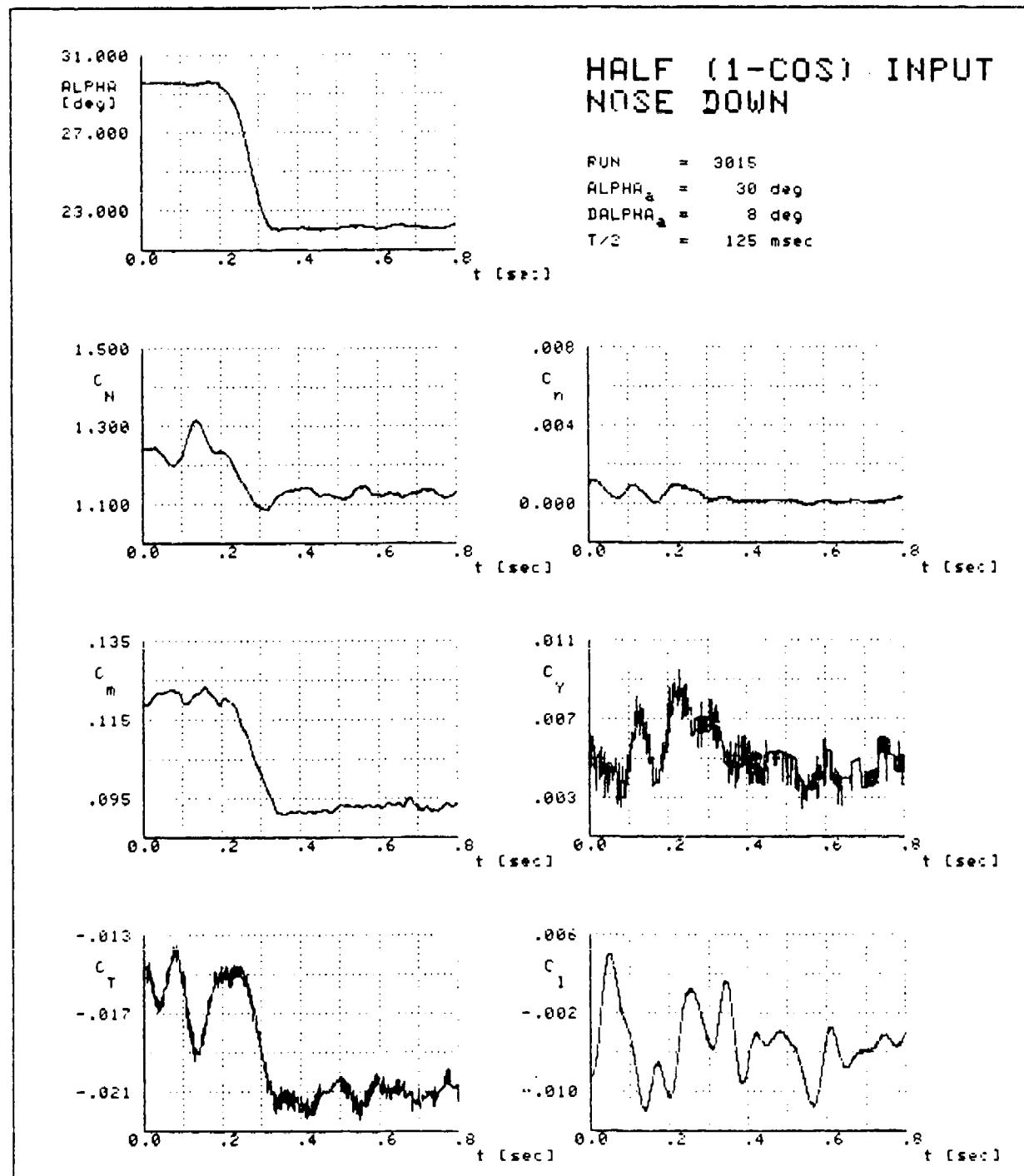


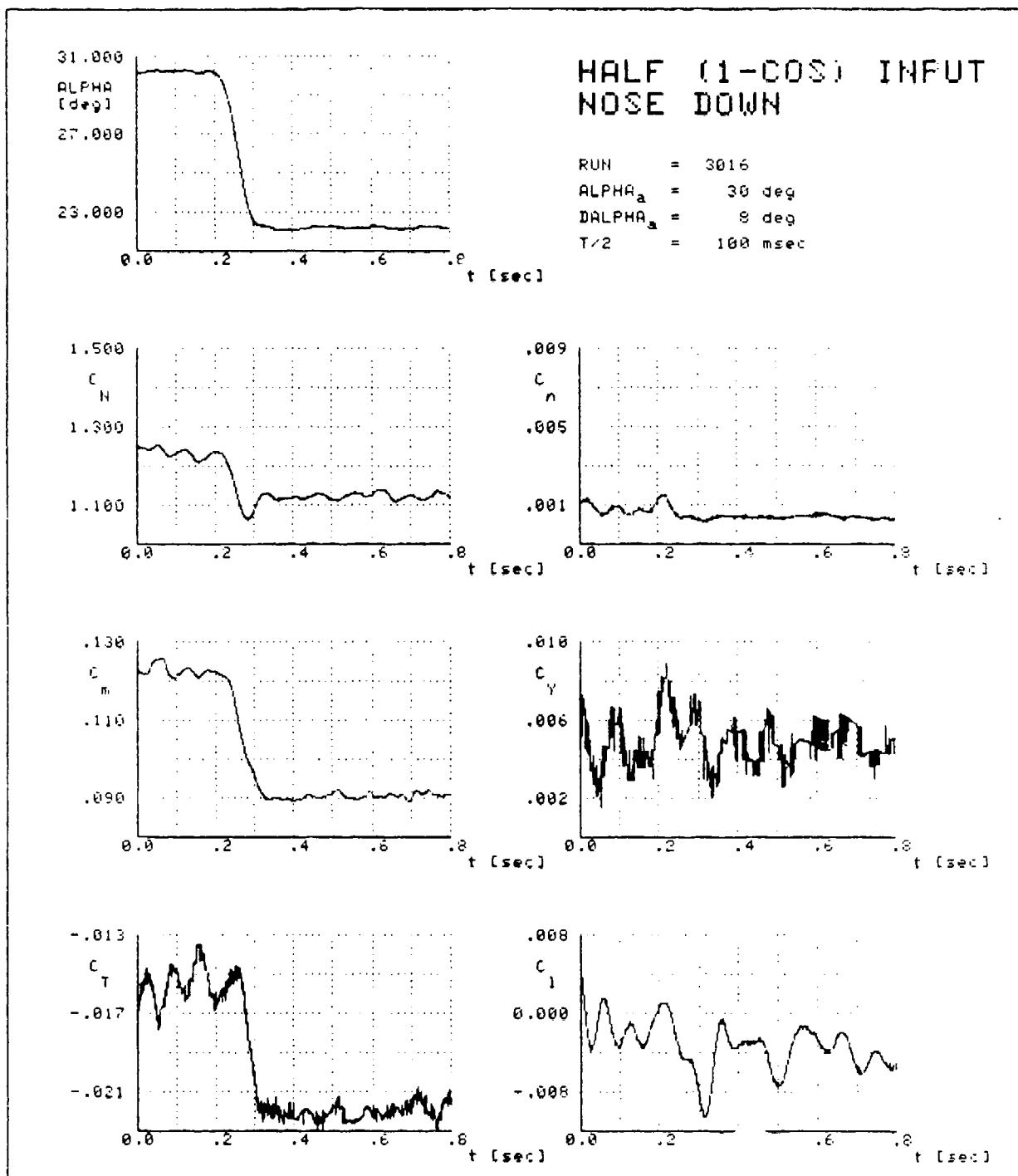


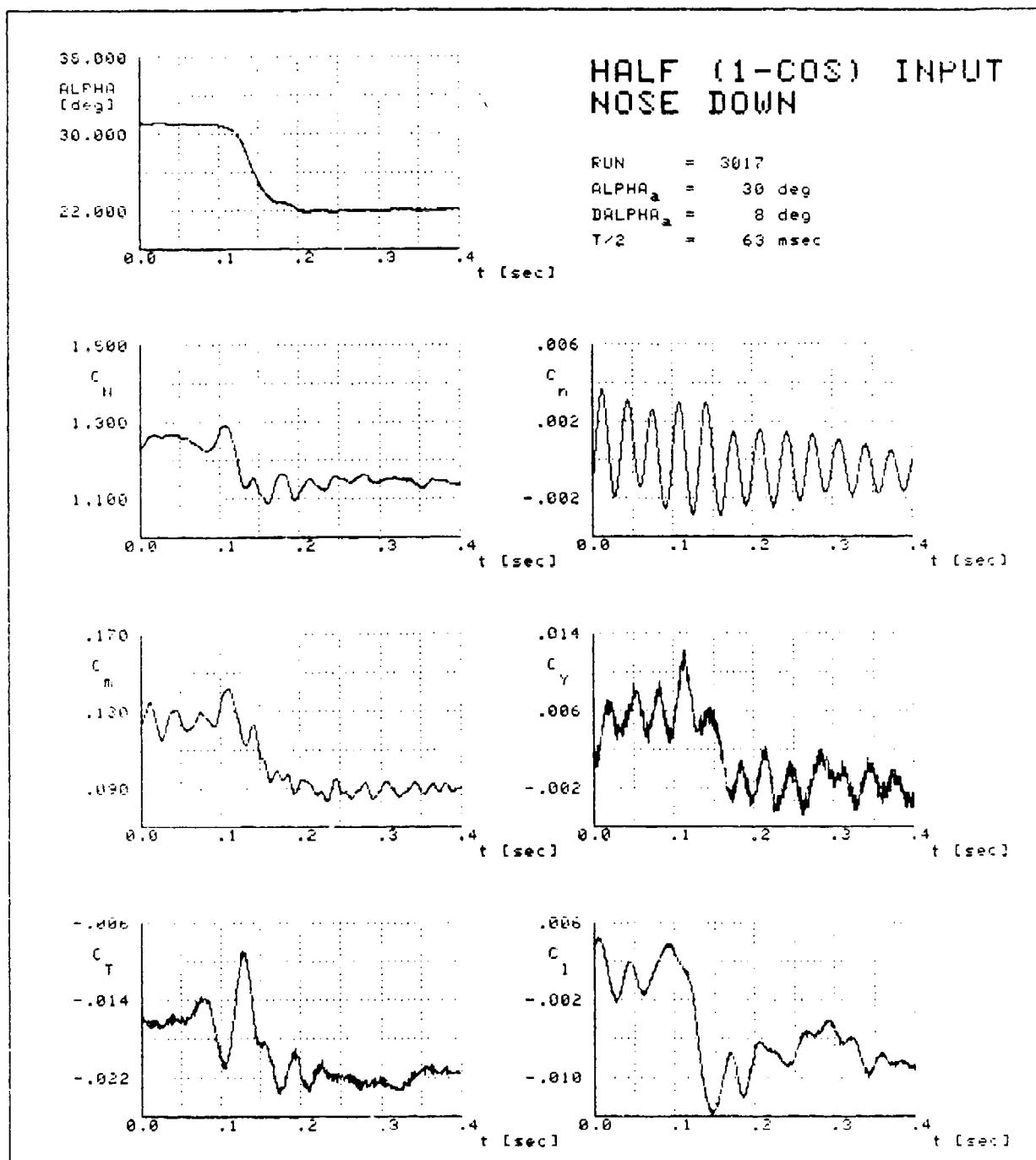


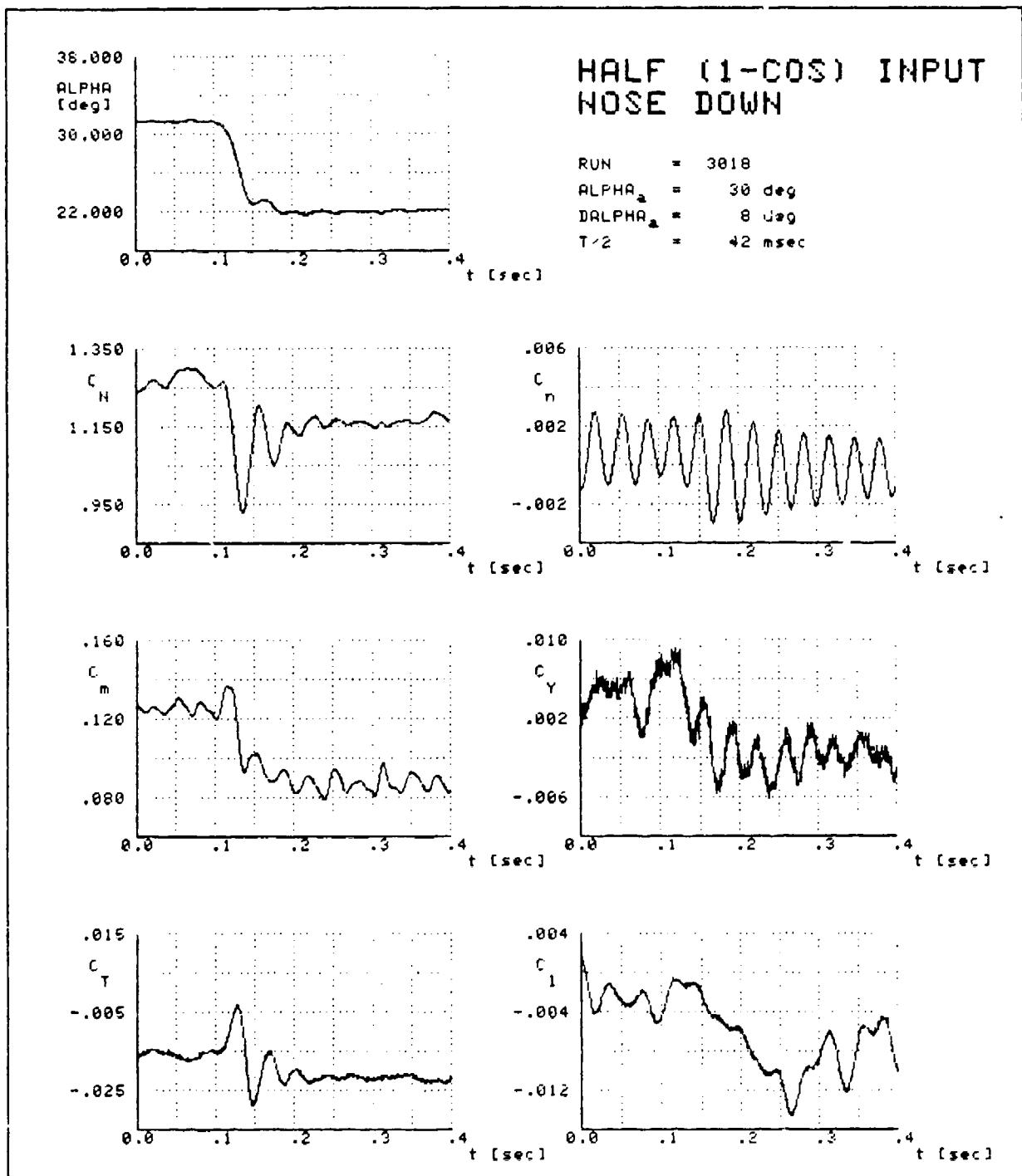


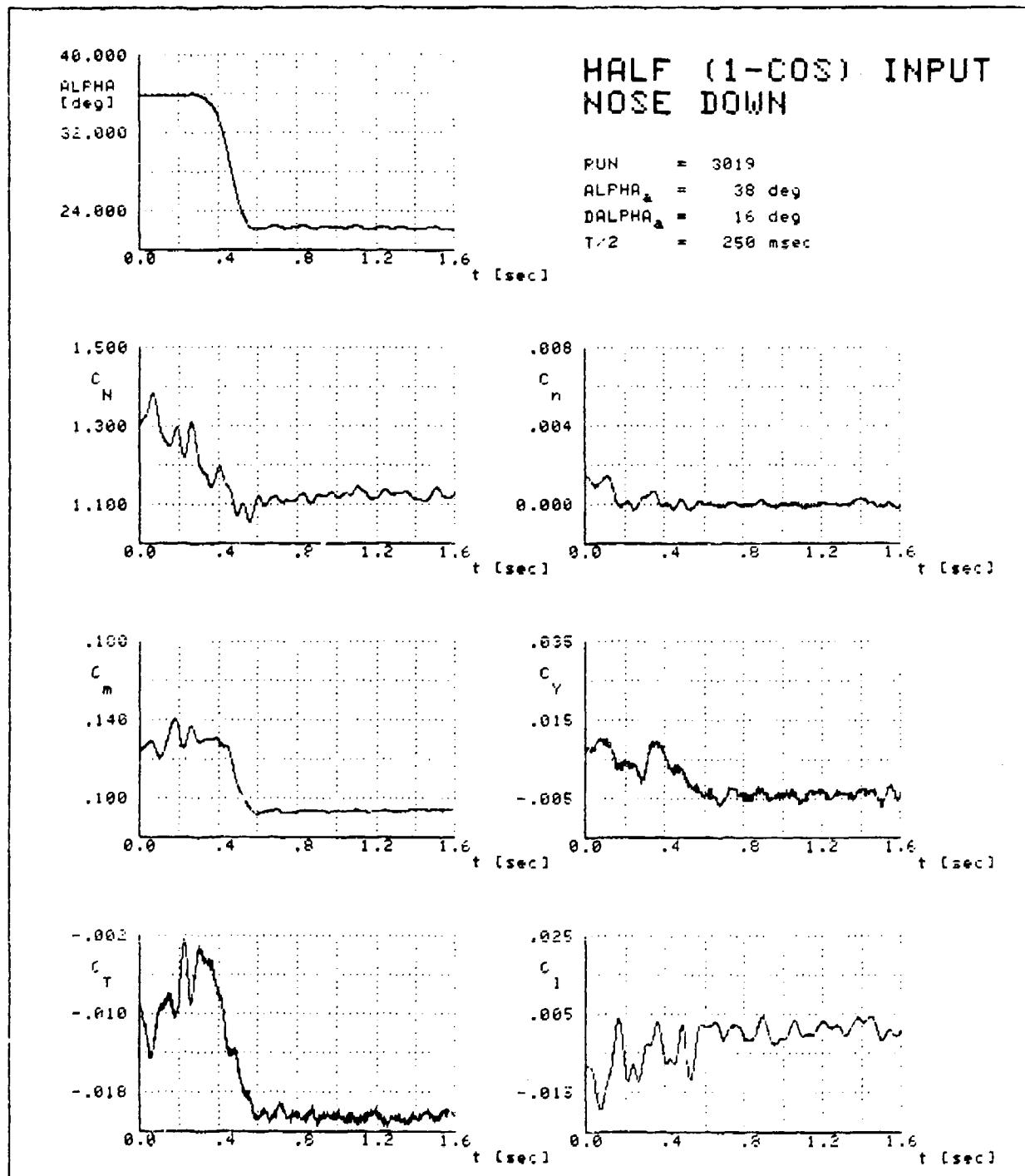


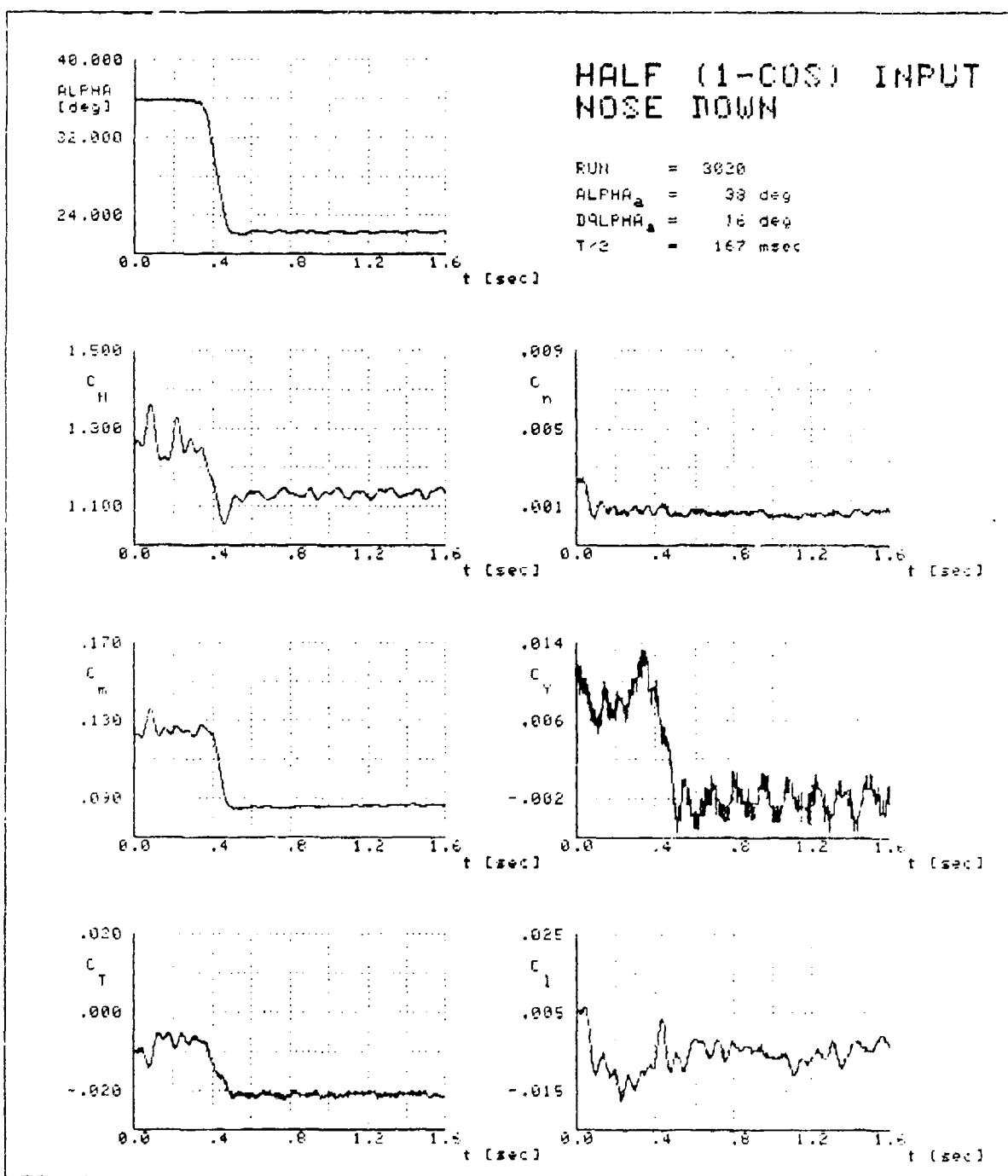


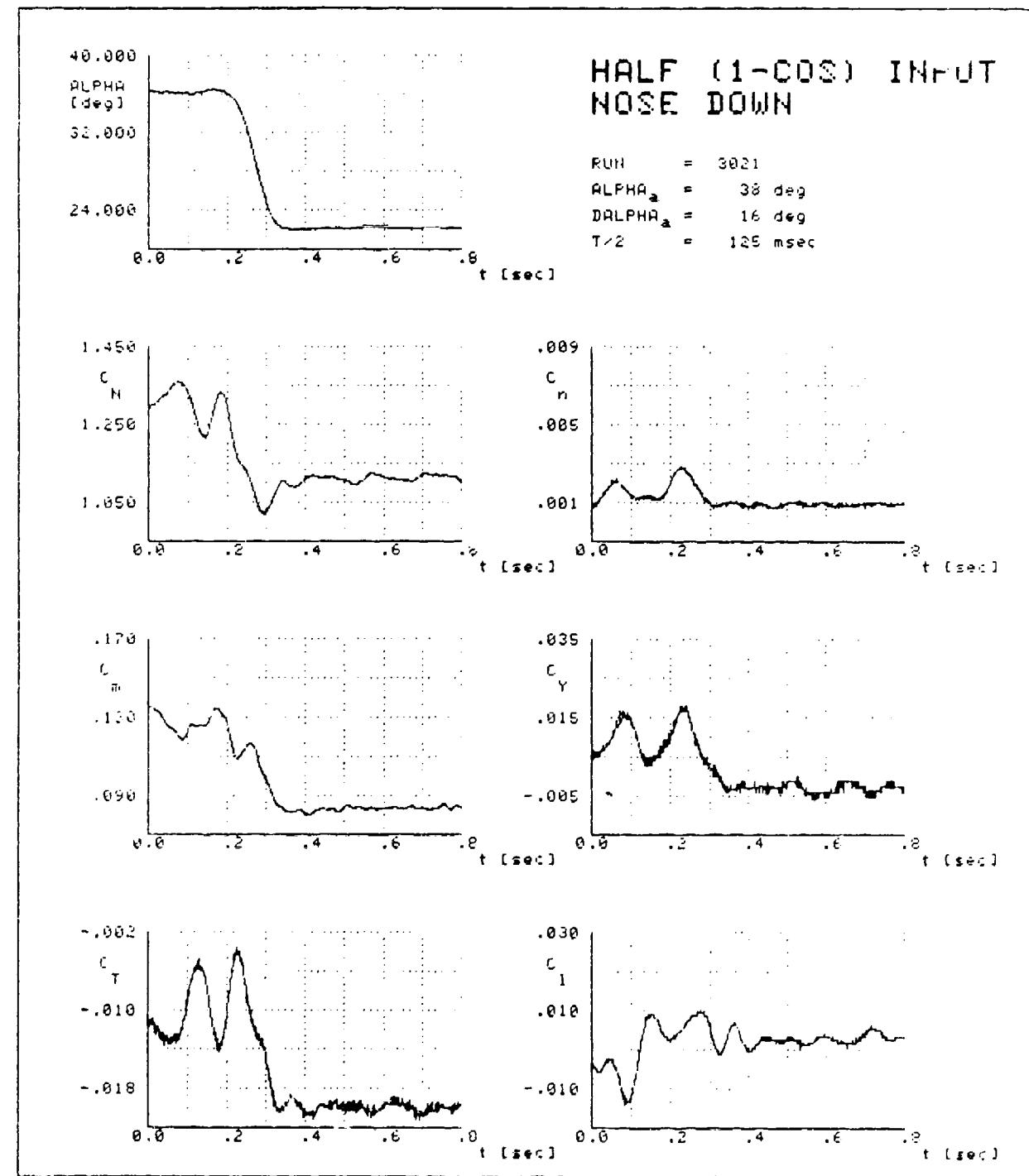


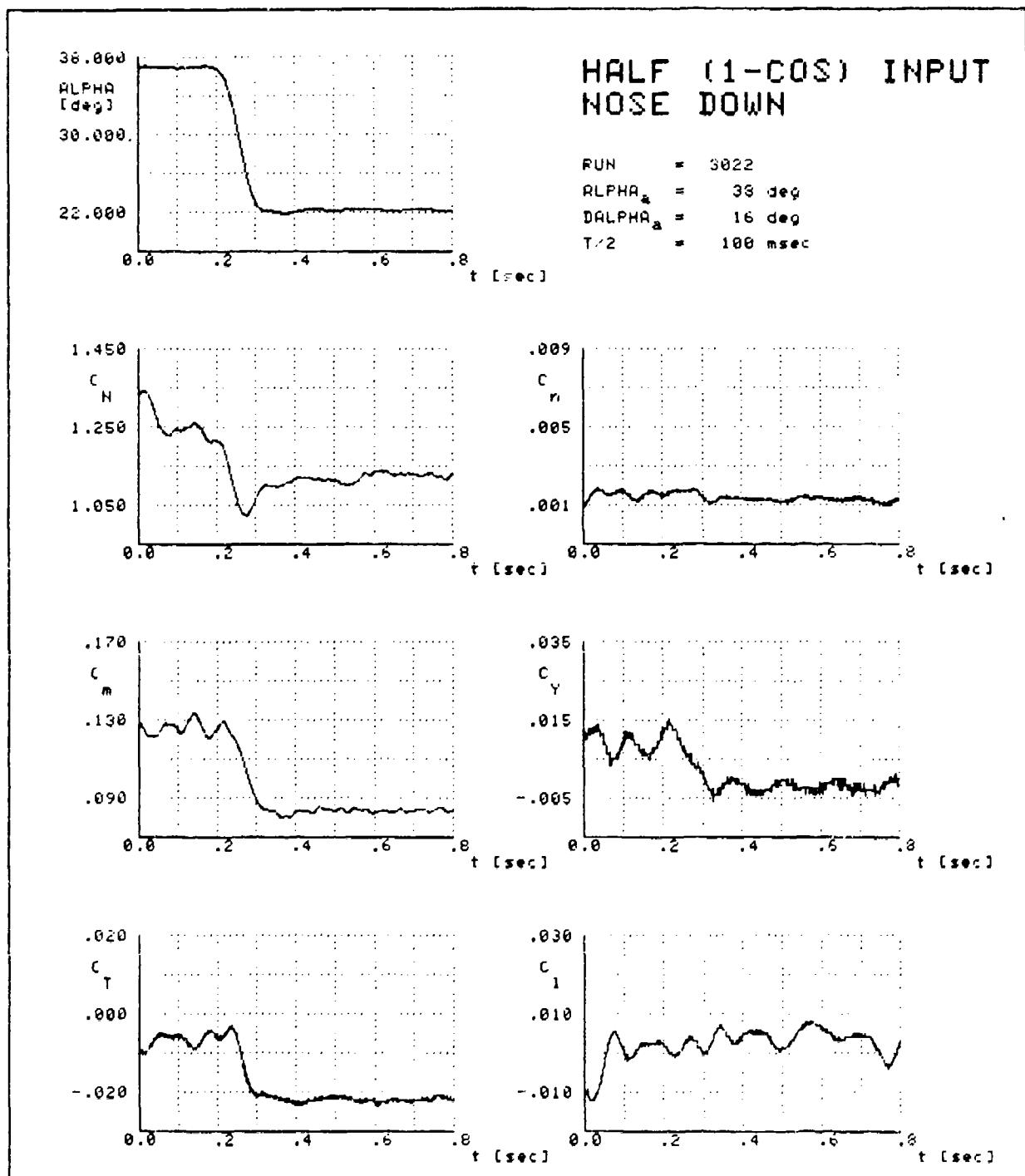


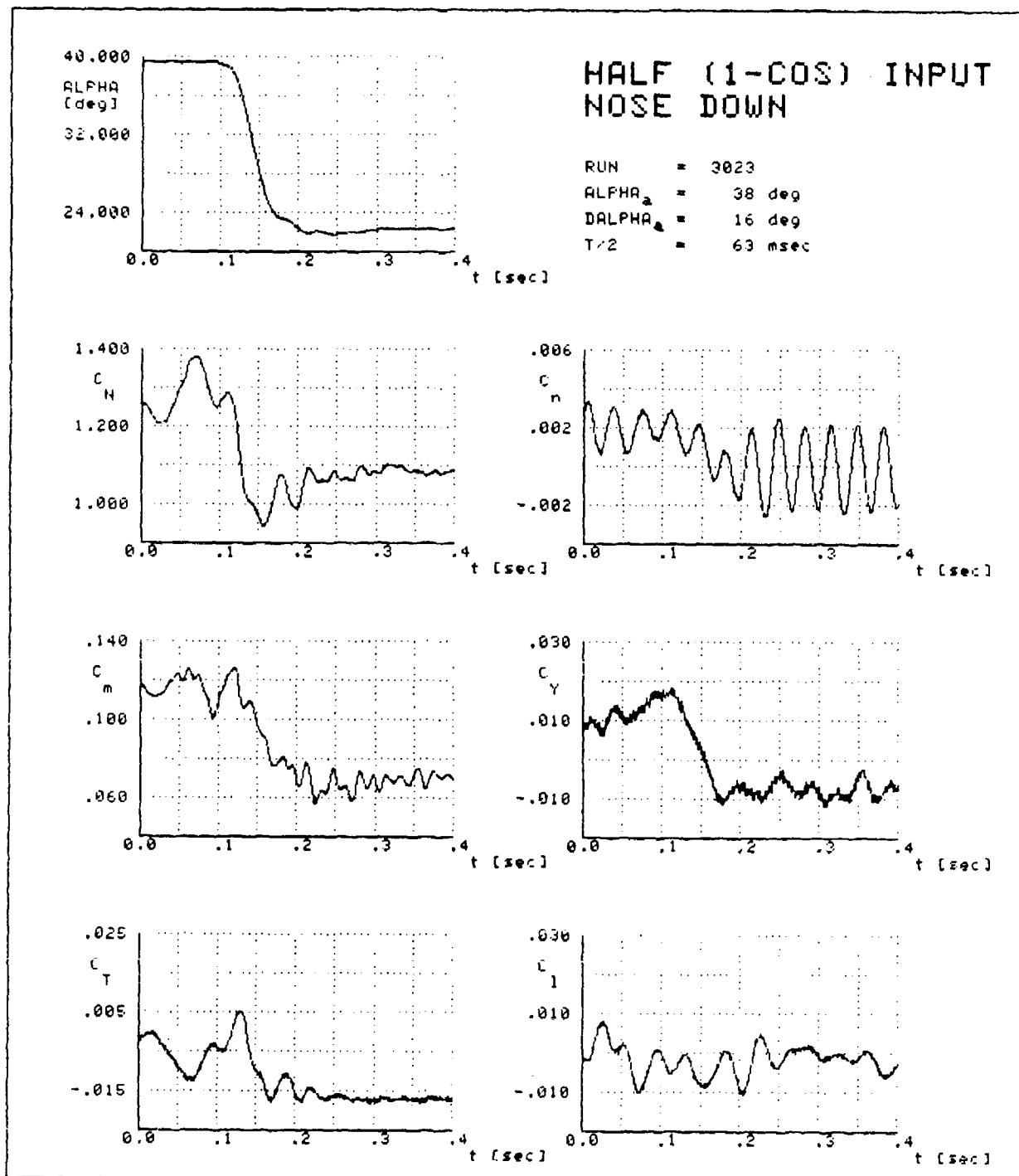


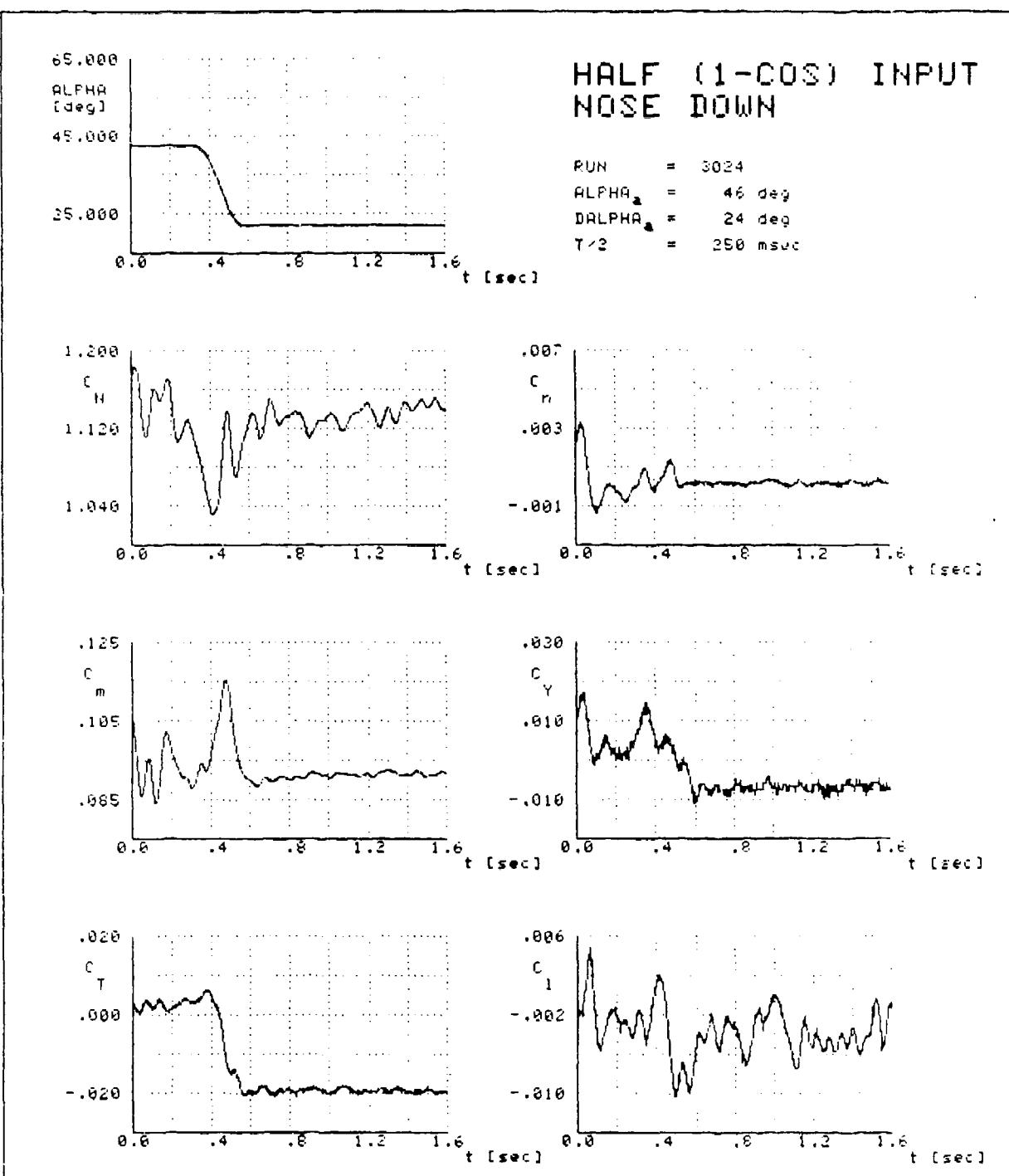


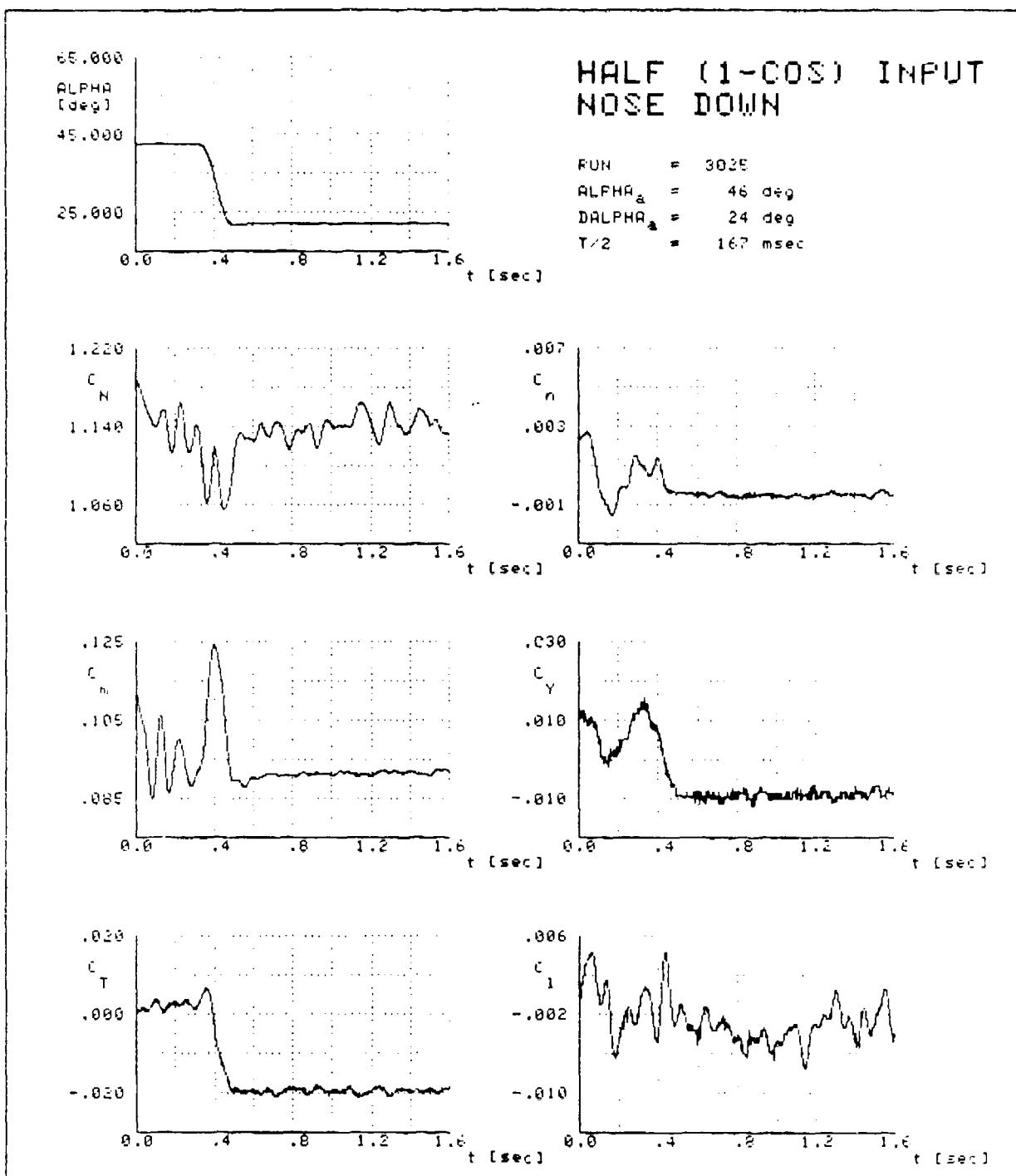


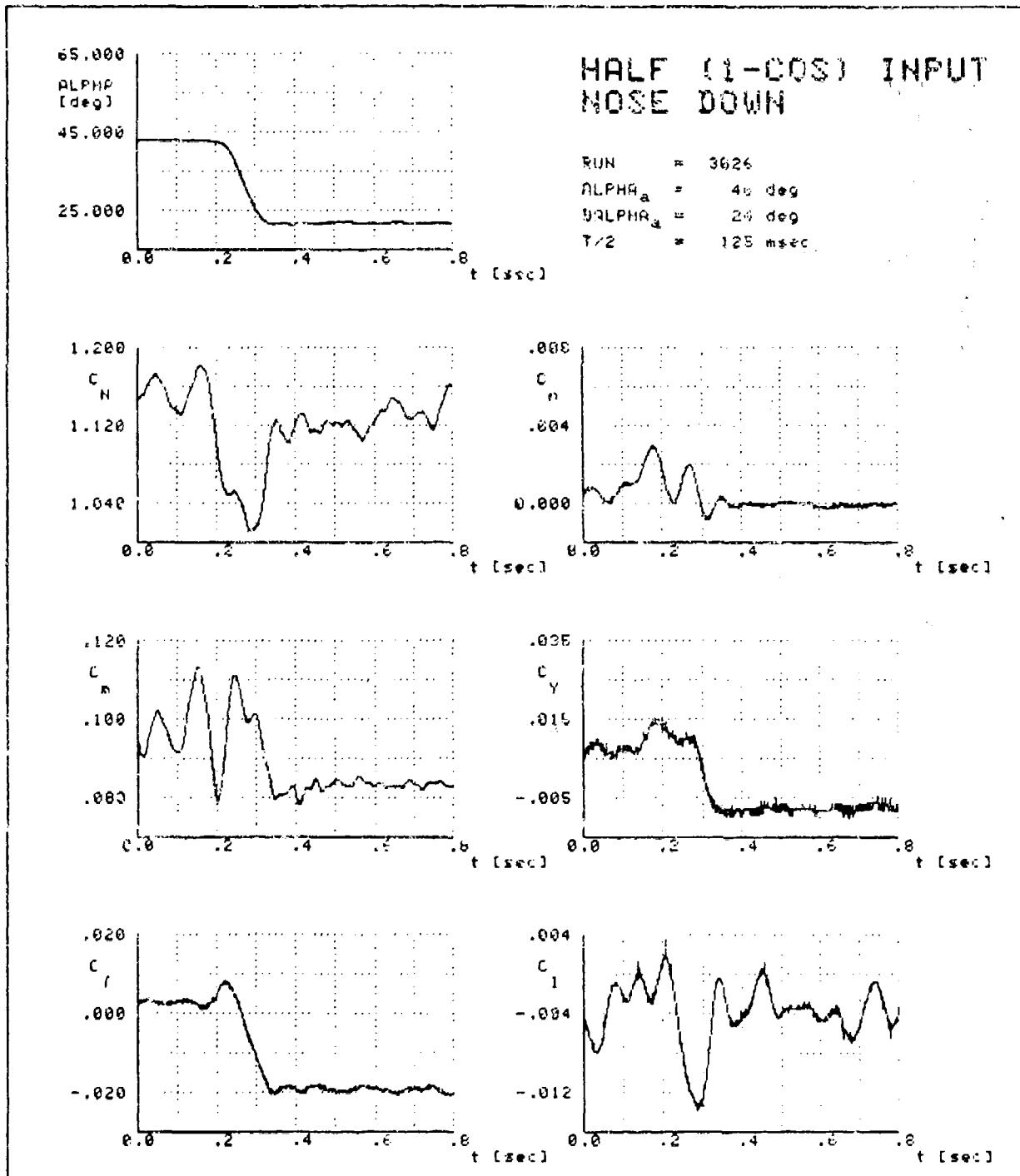


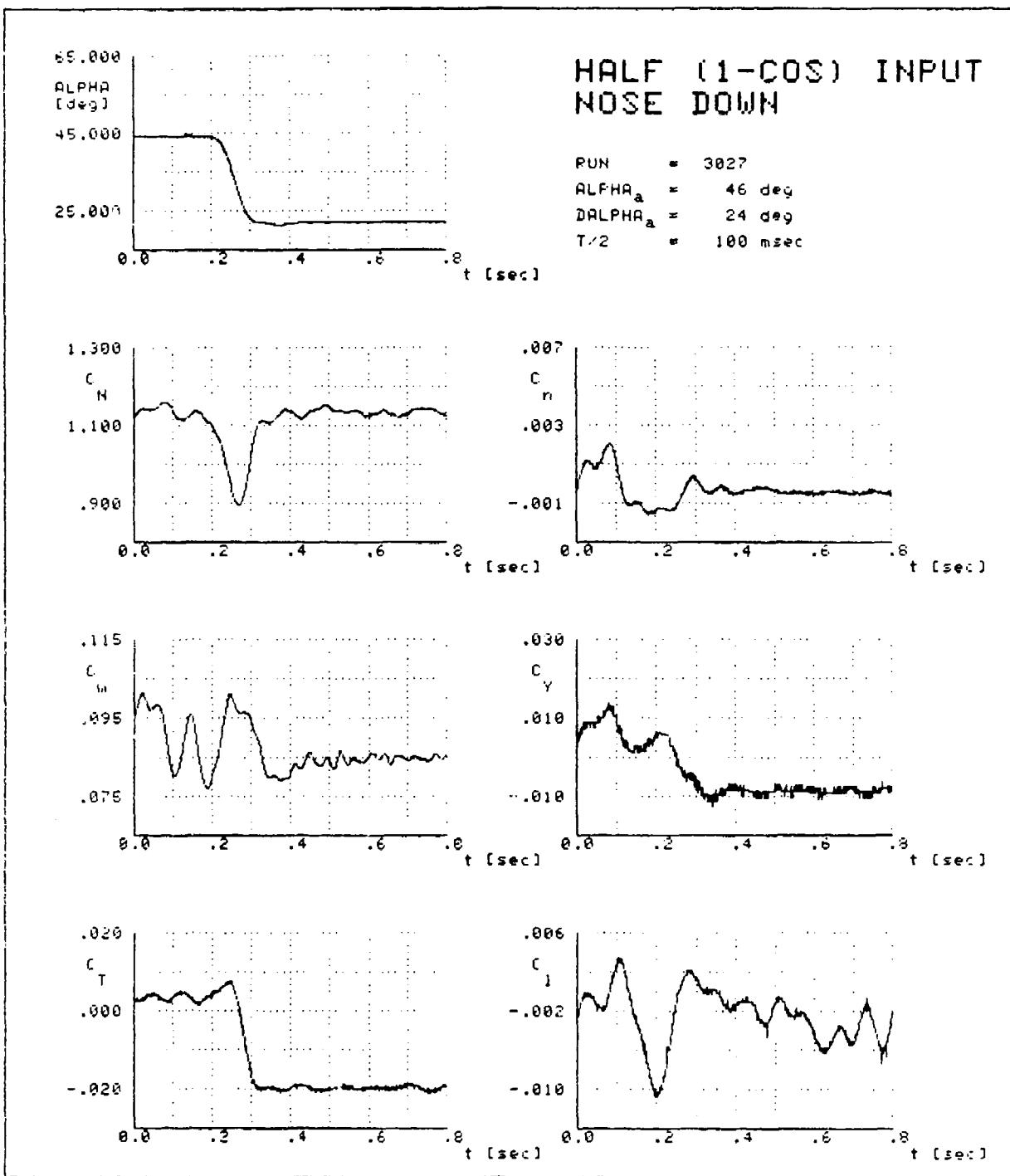


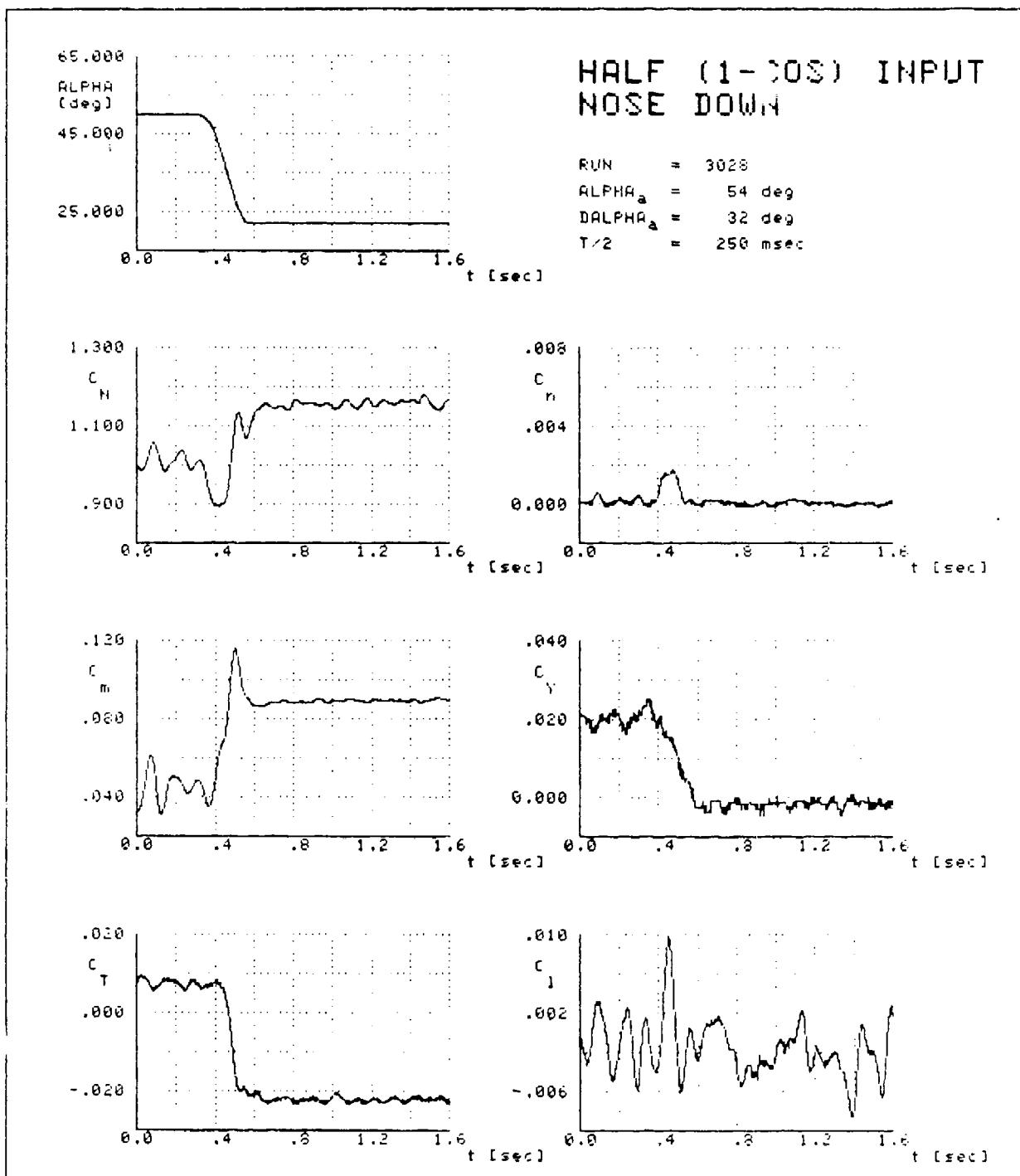


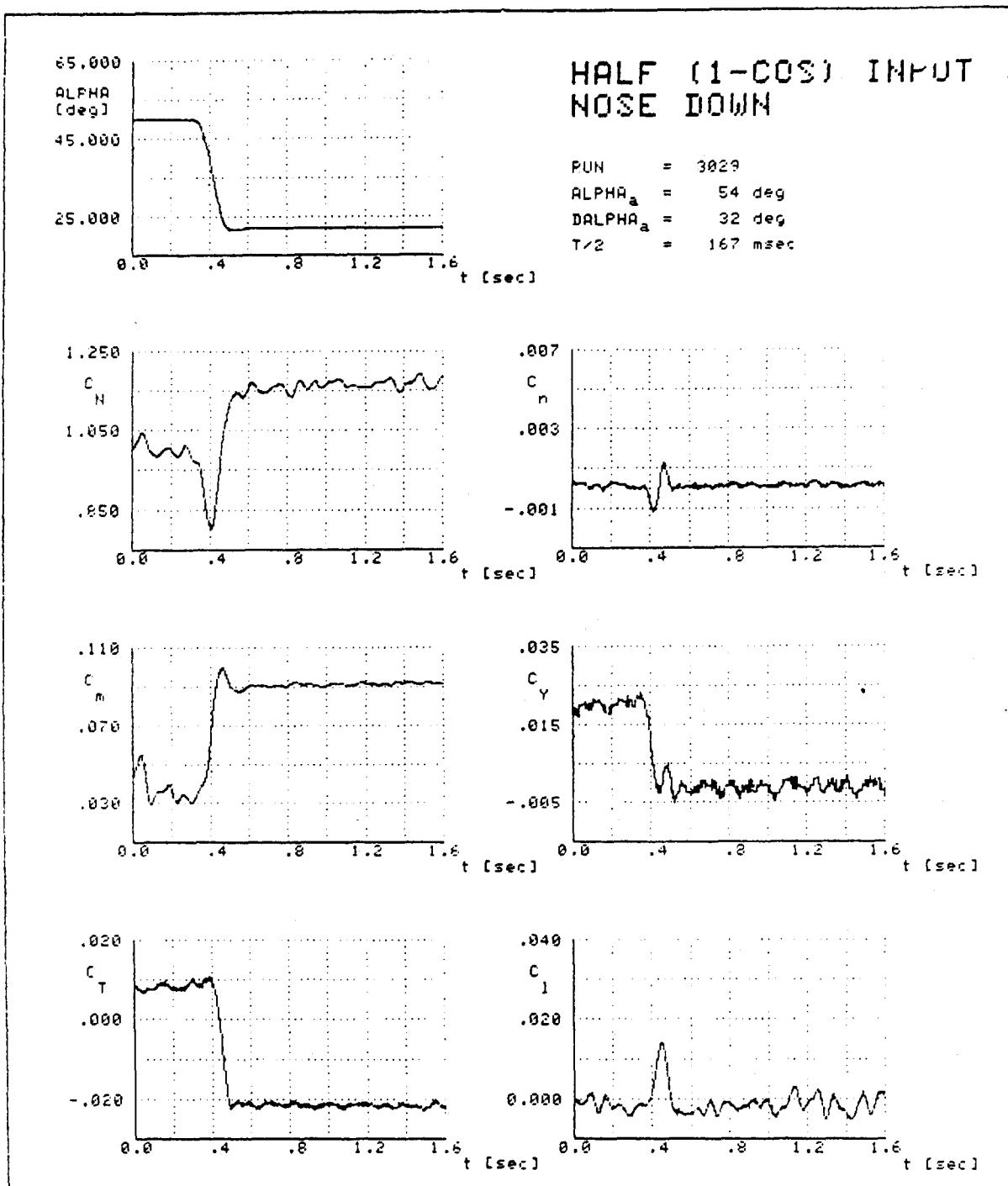


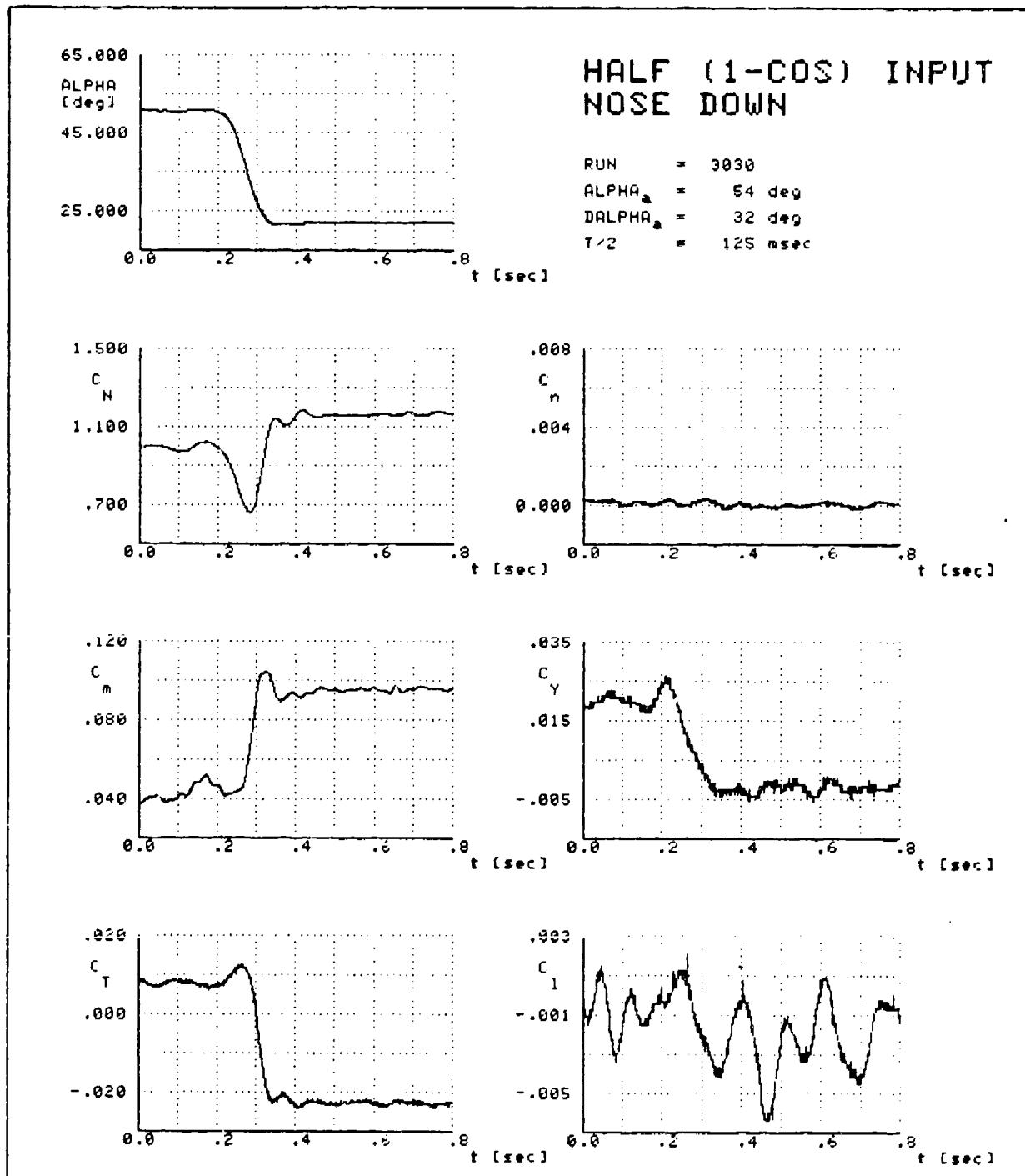


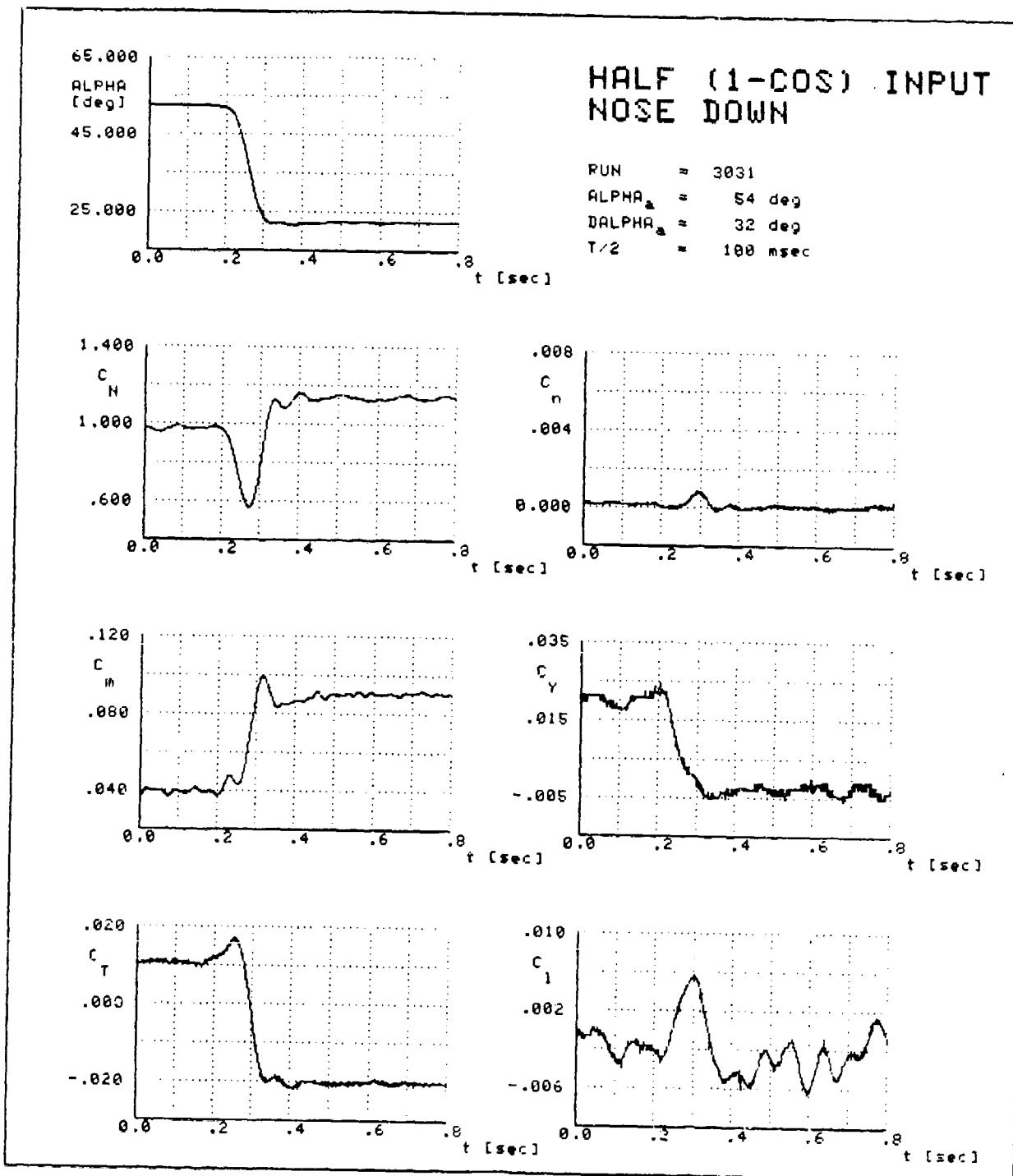


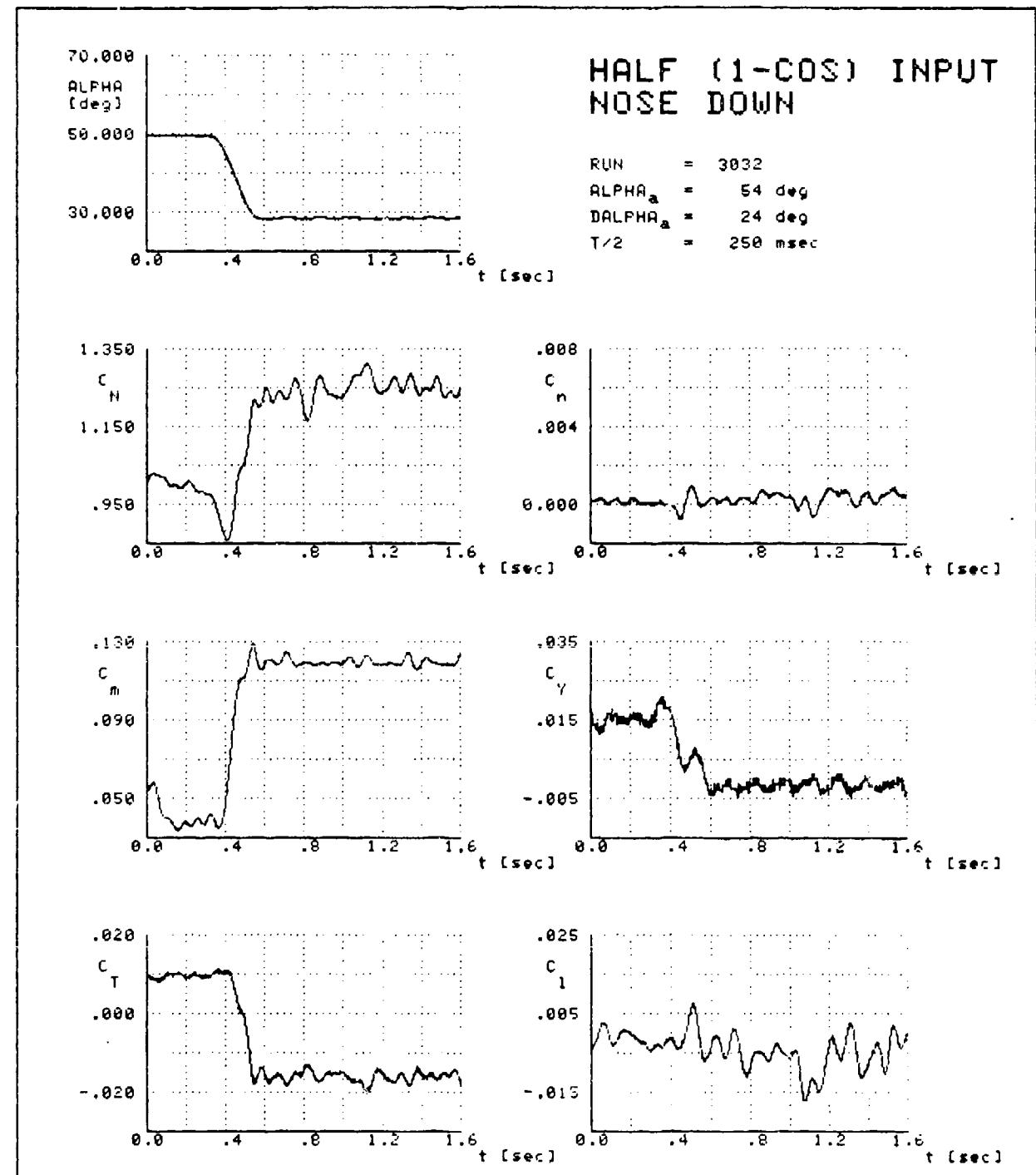


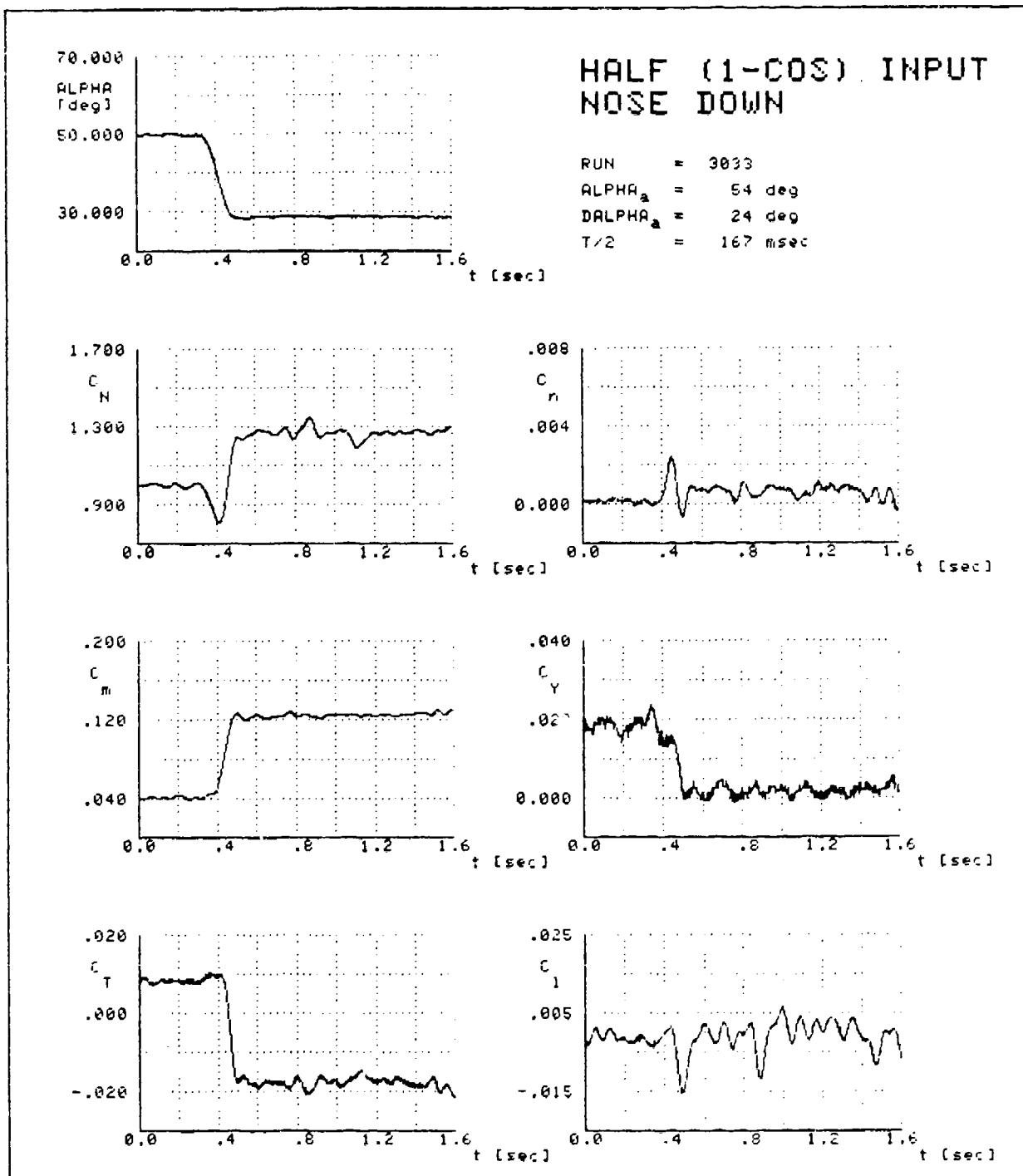


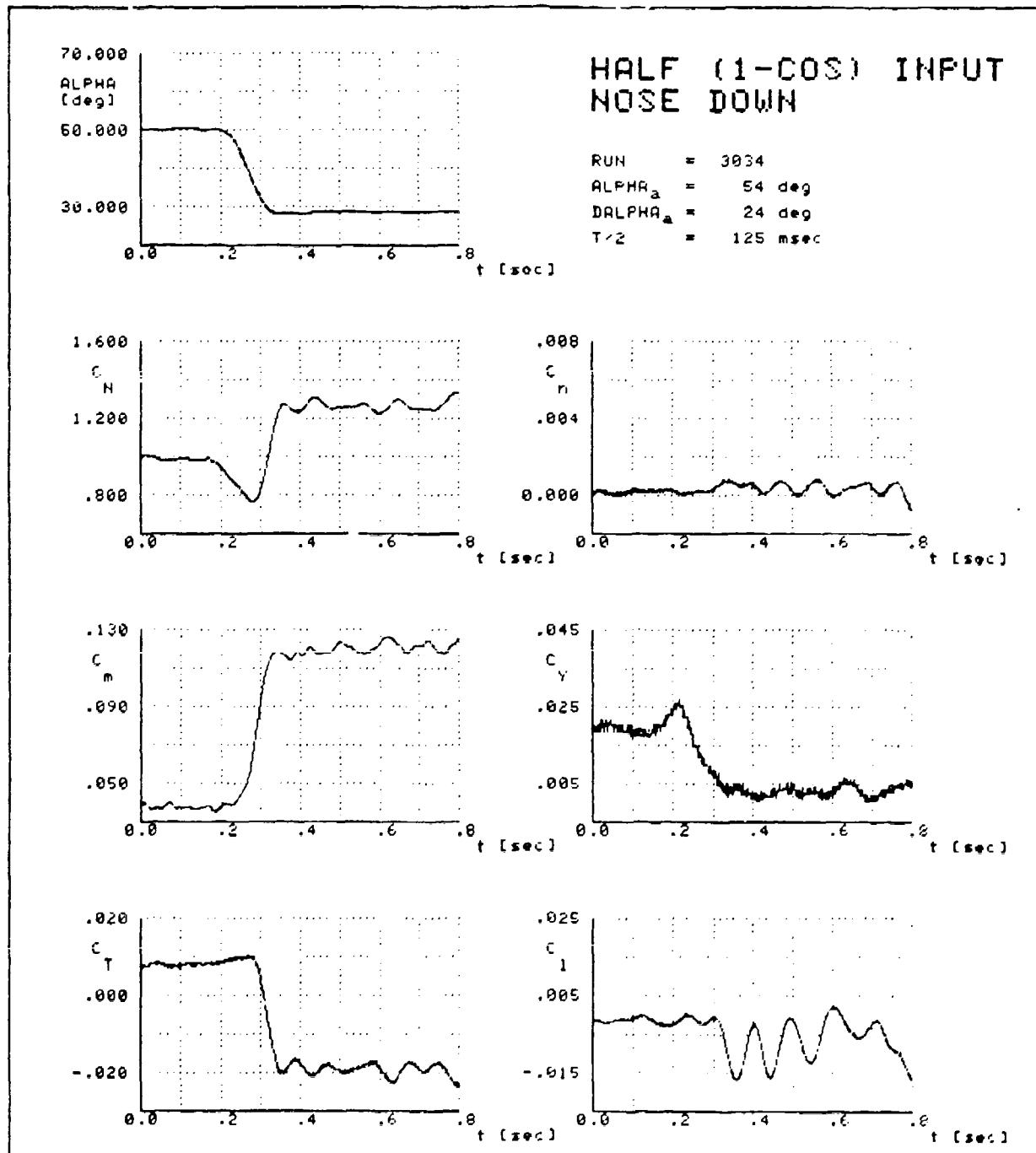


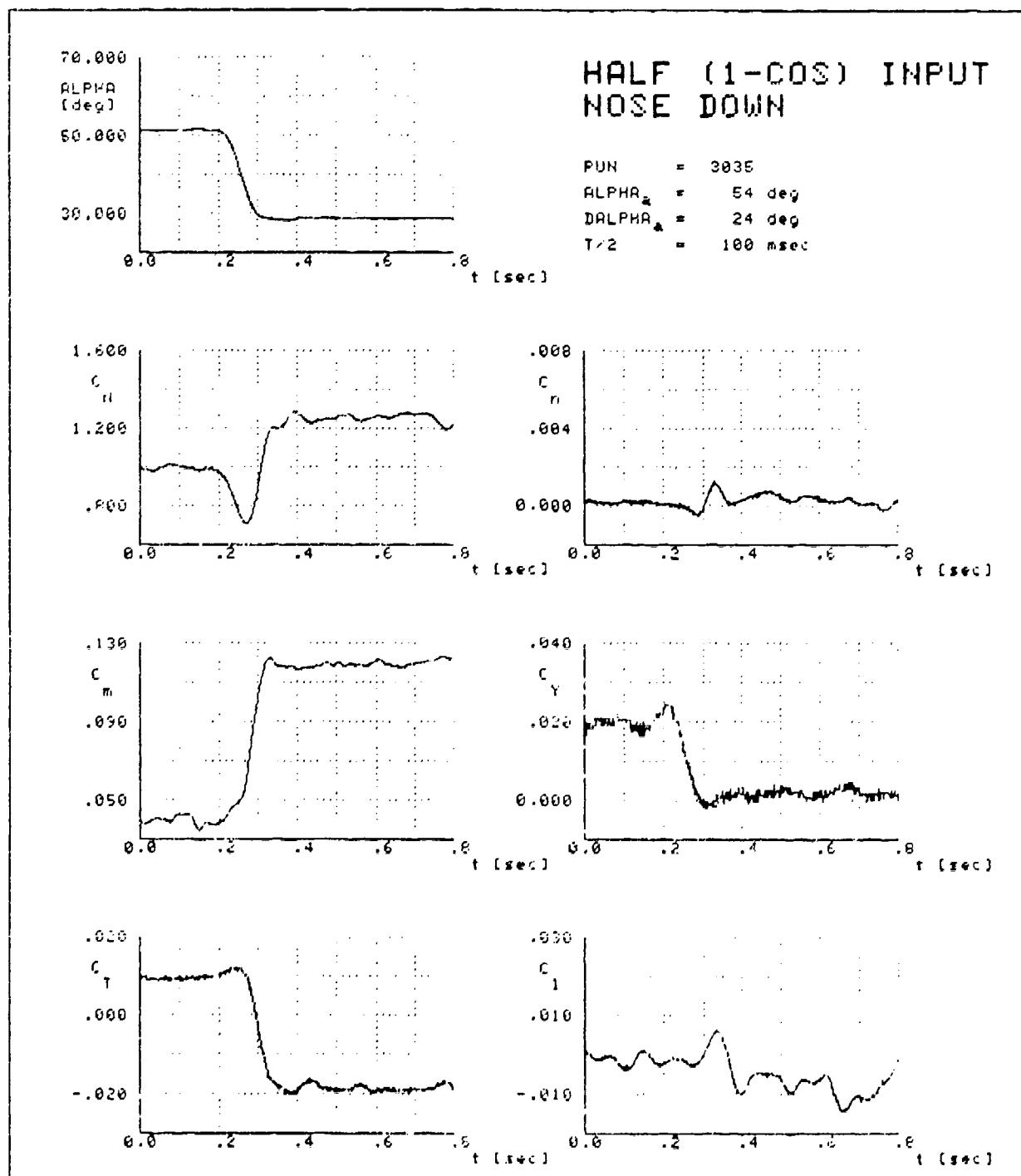


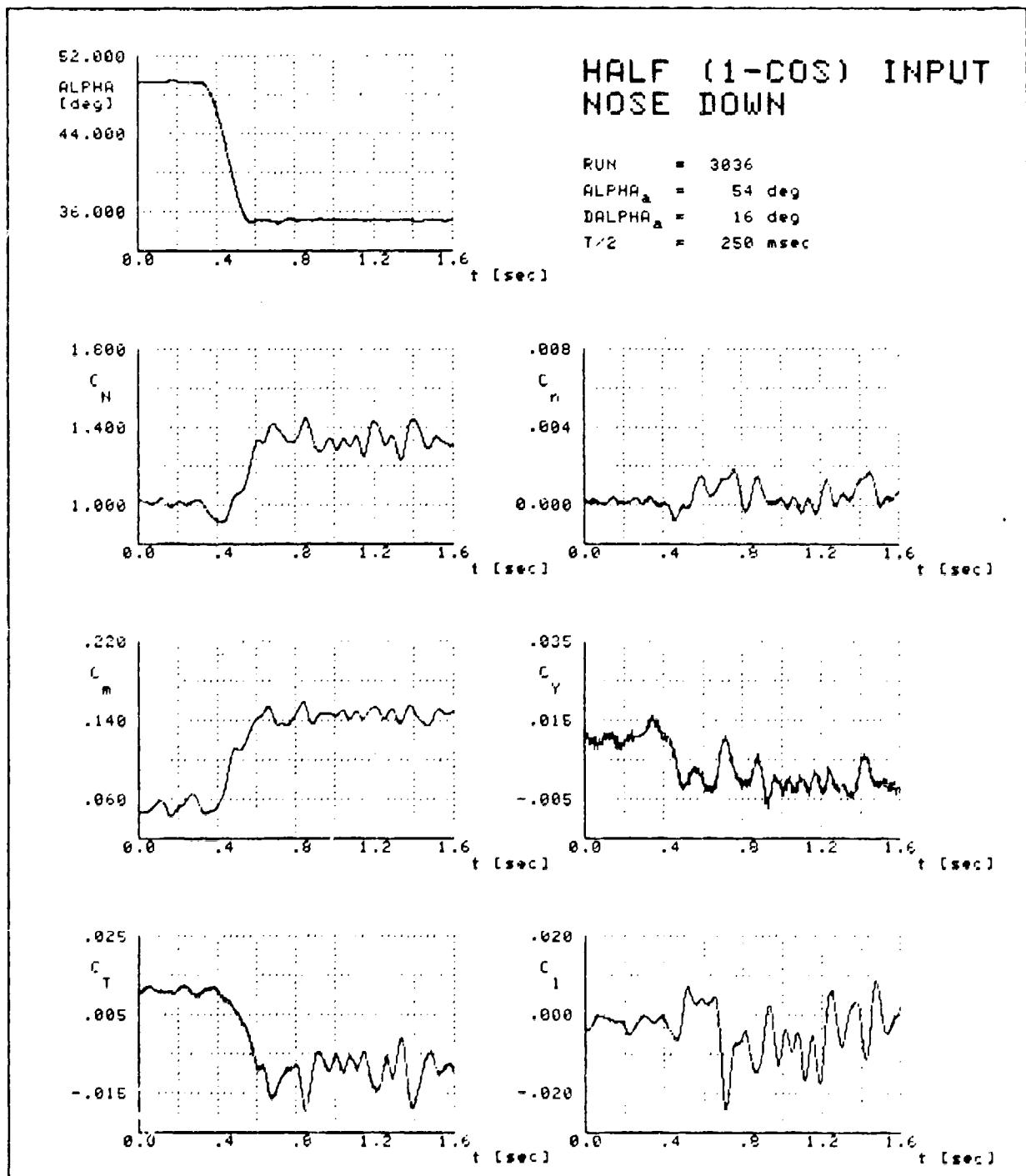


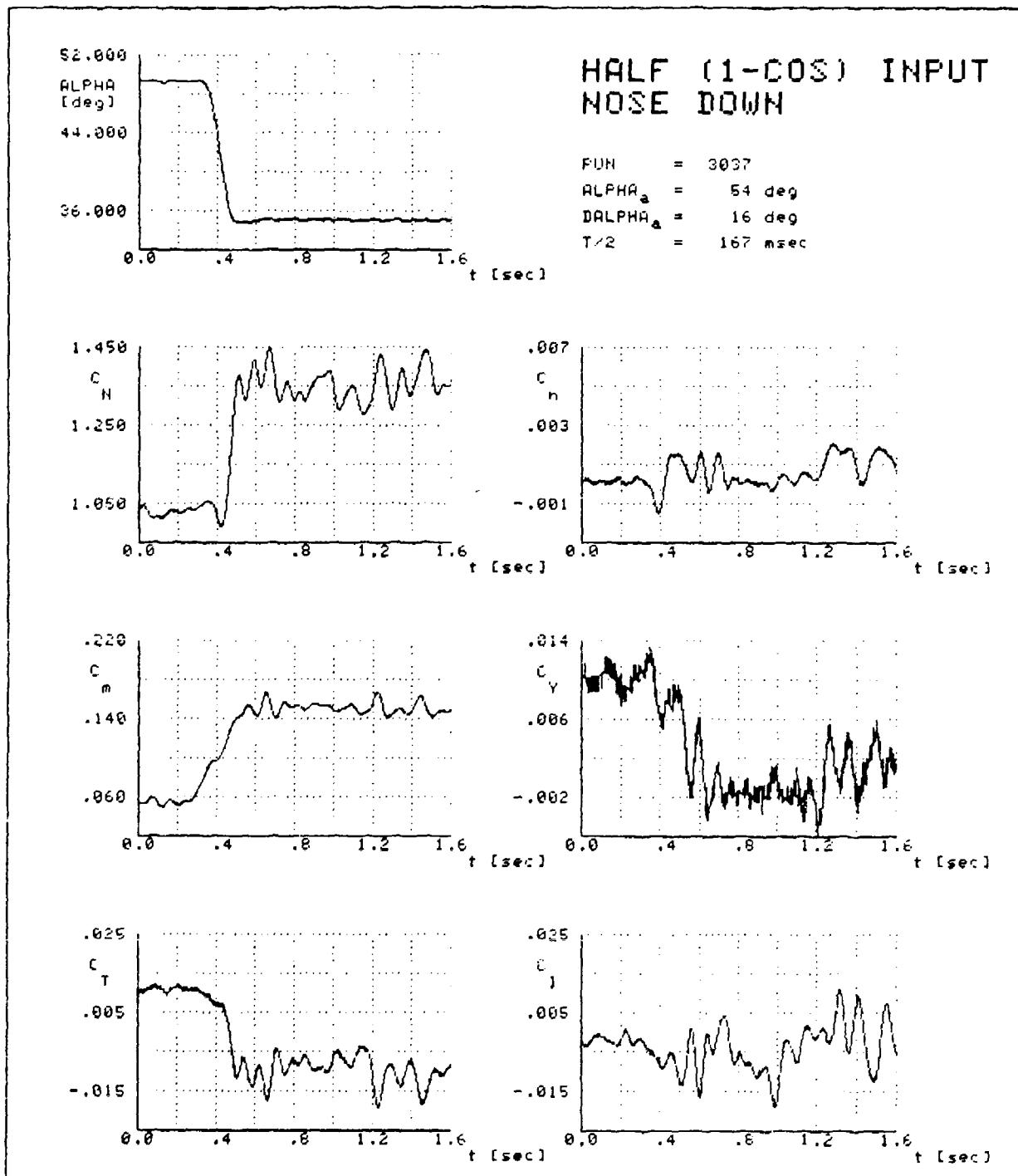


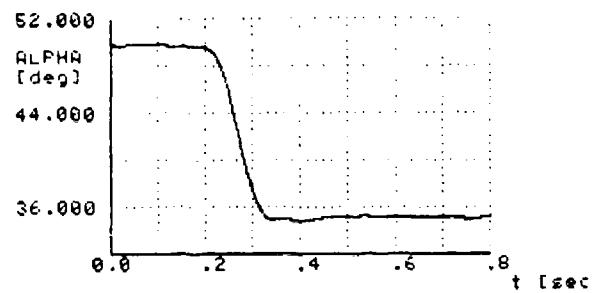






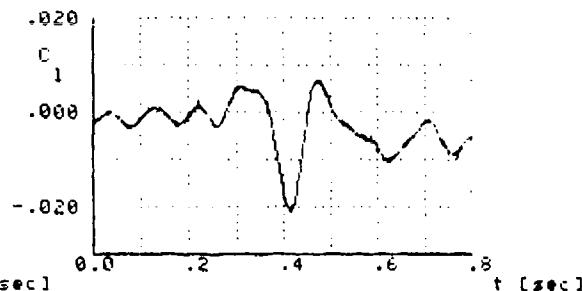
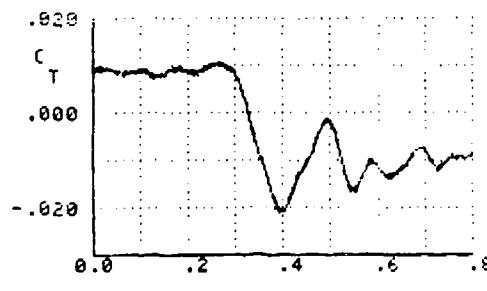
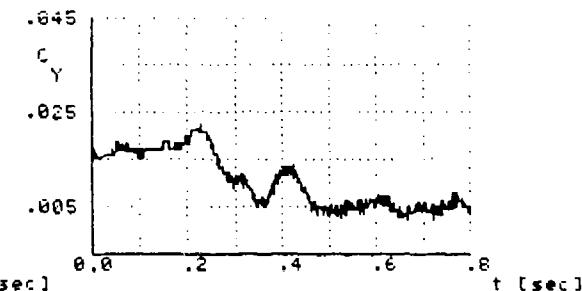
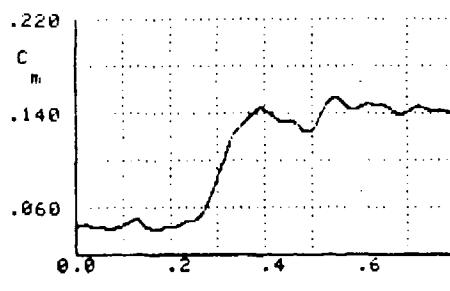
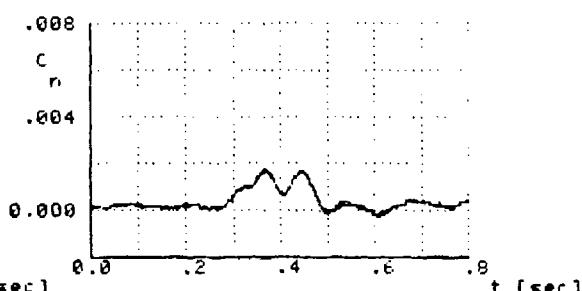
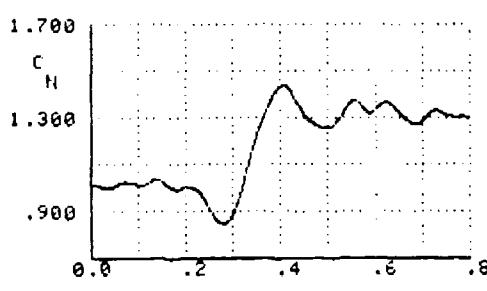


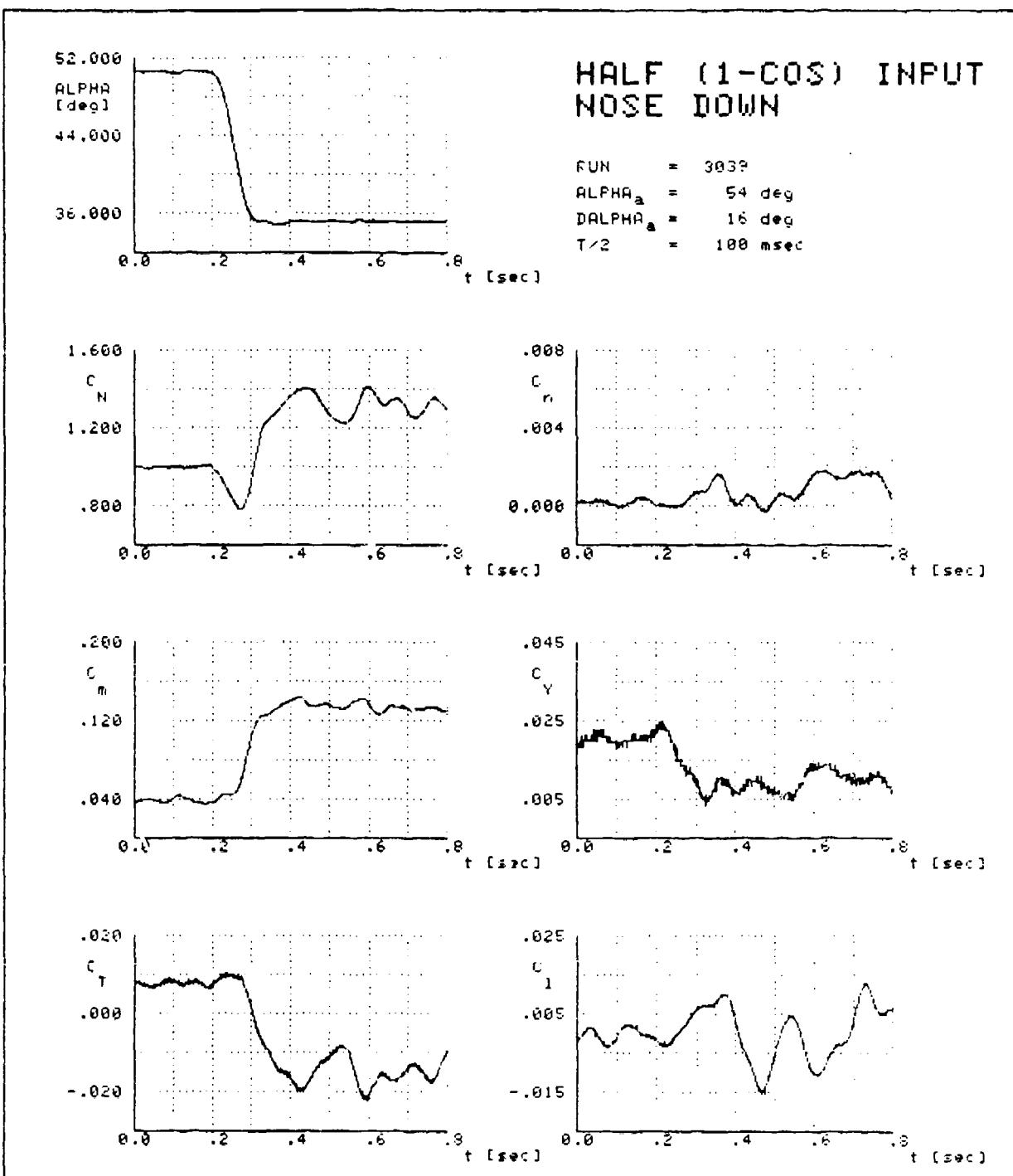




HALF (1-COS) INPUT NOSE DOWN

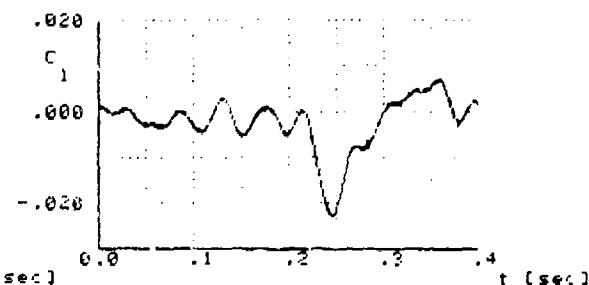
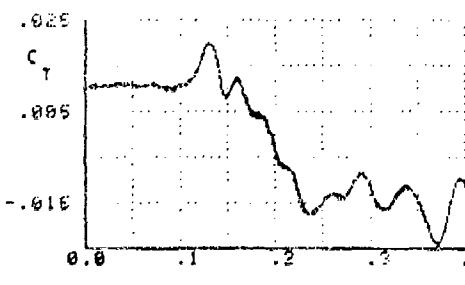
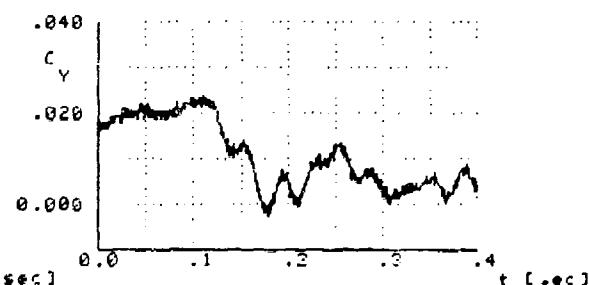
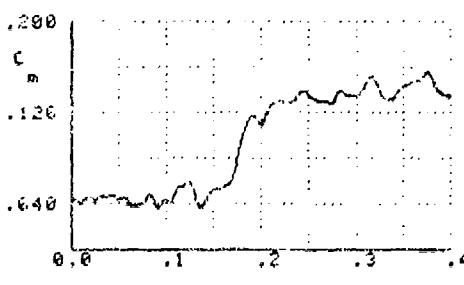
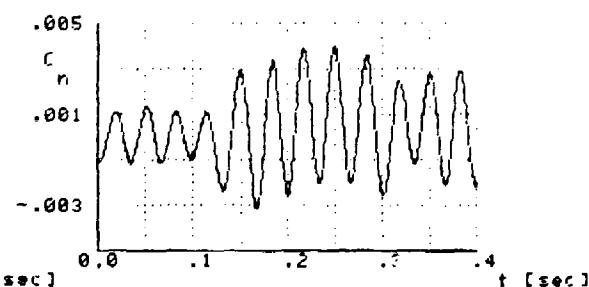
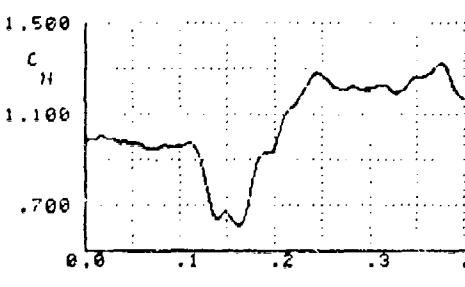
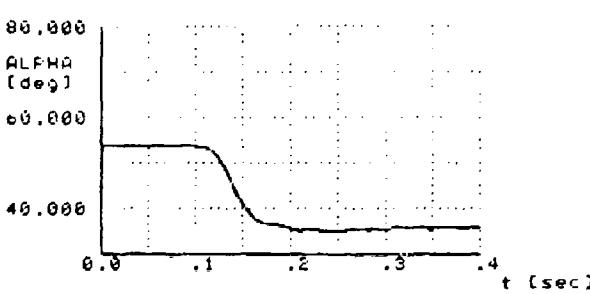
RUN = 3038
 $\text{ALPHA}_a = 54 \text{ deg}$
 $\Delta\text{ALPHA}_a = 16 \text{ deg}$
 $T/2 = 125 \text{ msec}$

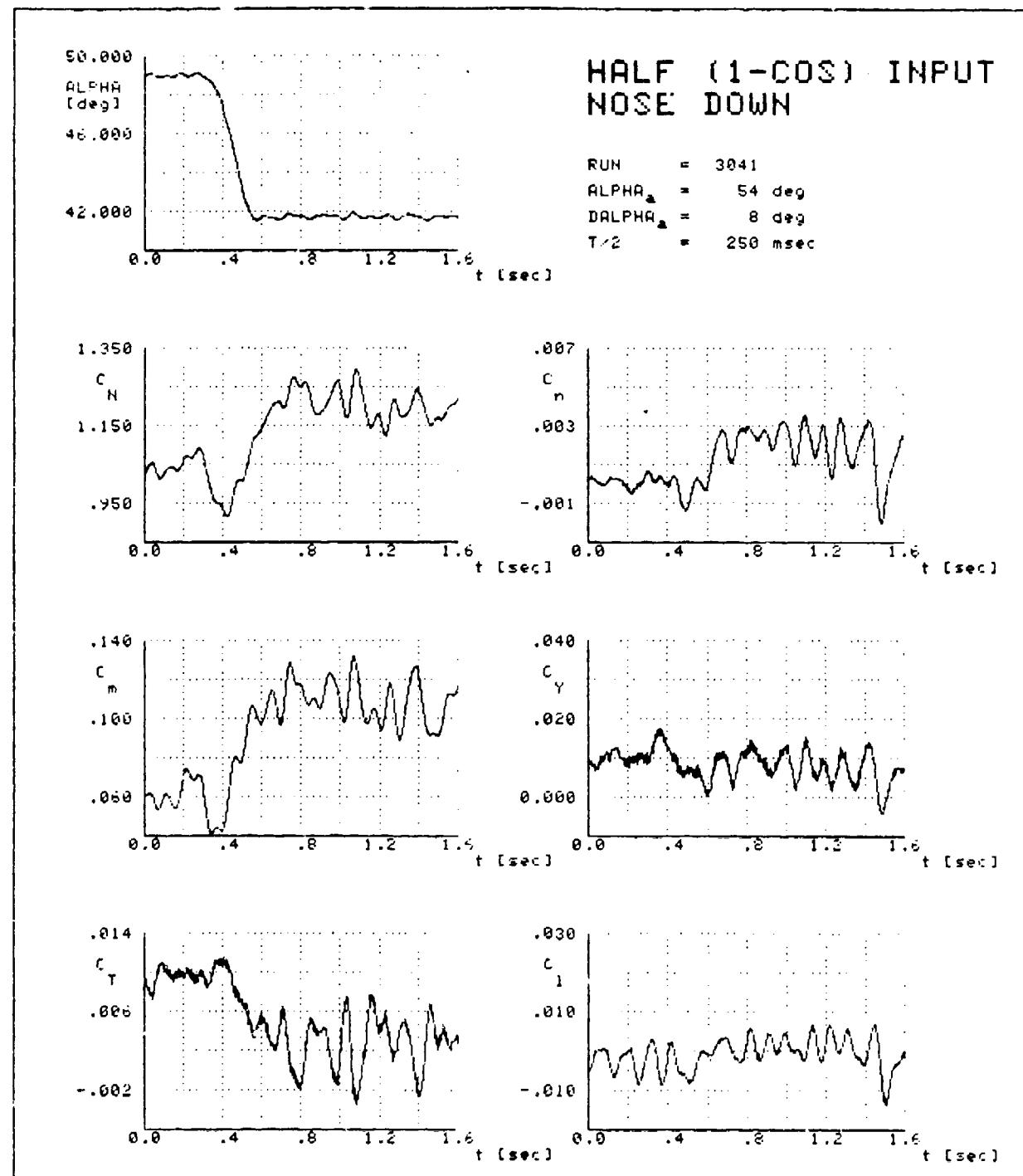


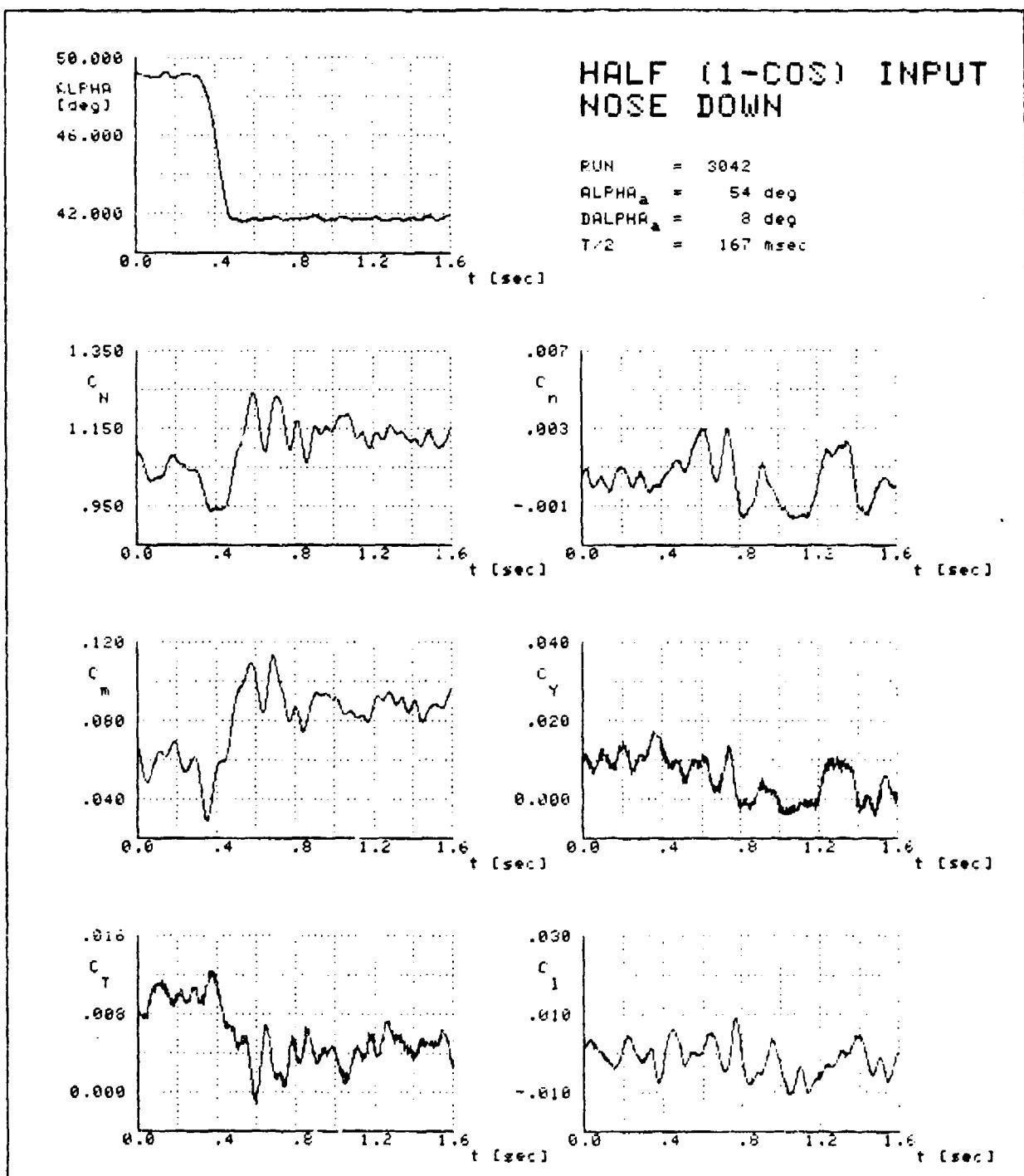


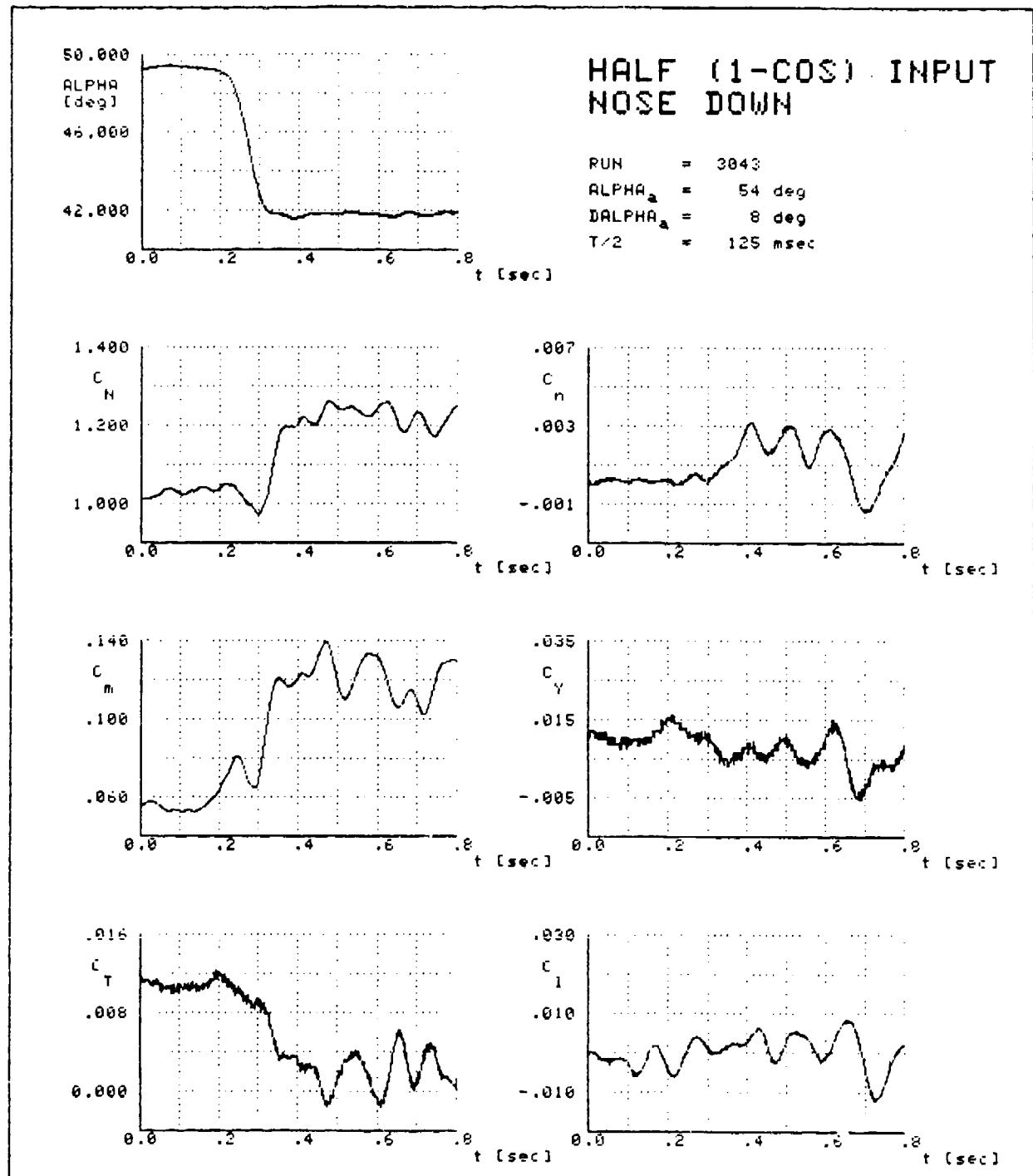
HALF (1-COS) INPUT
NOSE DOWN

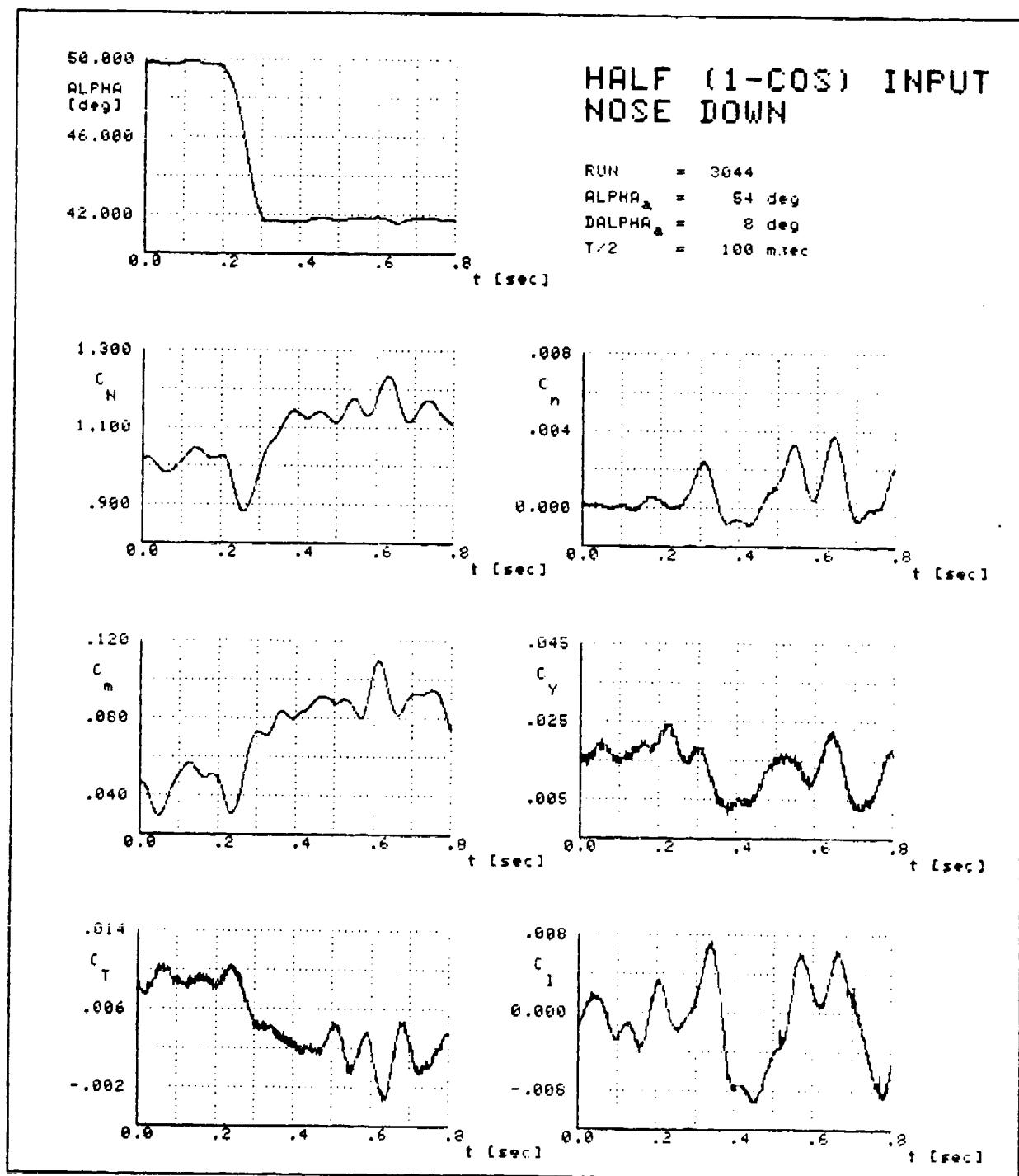
RUN = 3040
 ALPHA_a = 54 deg
 $\text{D}\Delta\text{ALPHA}_a$ = 16 deg
 $T/2$ = 63 msec

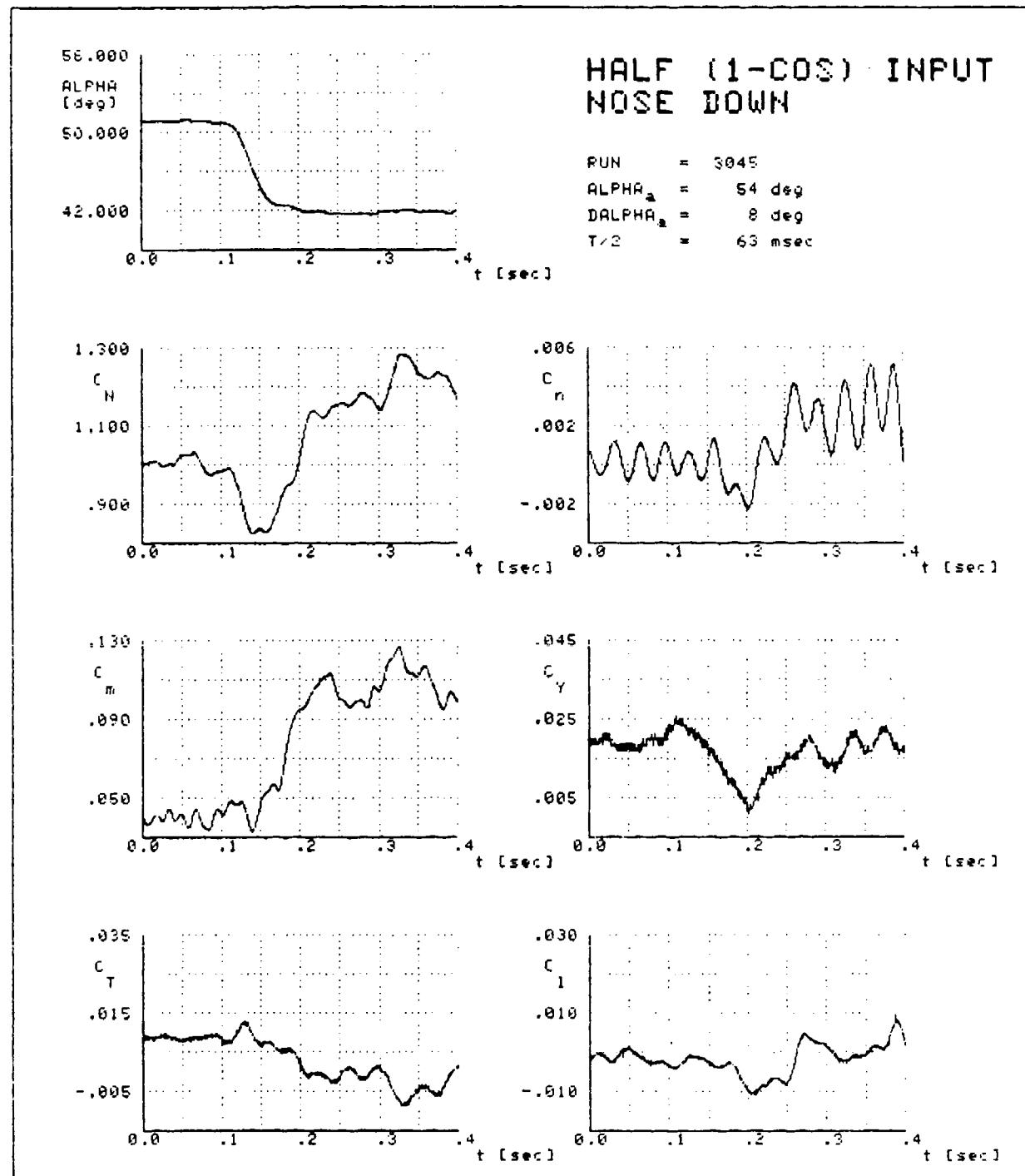


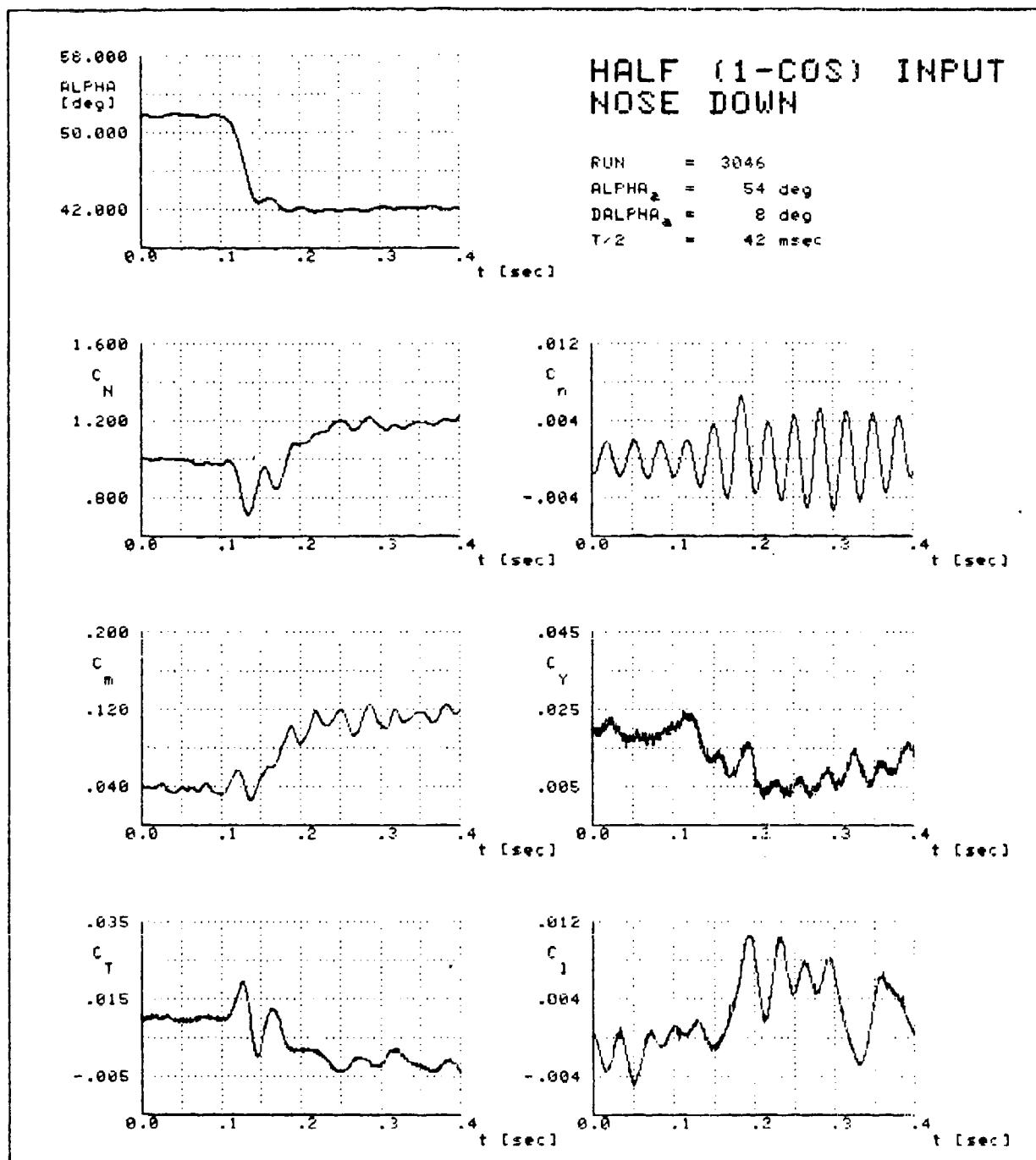


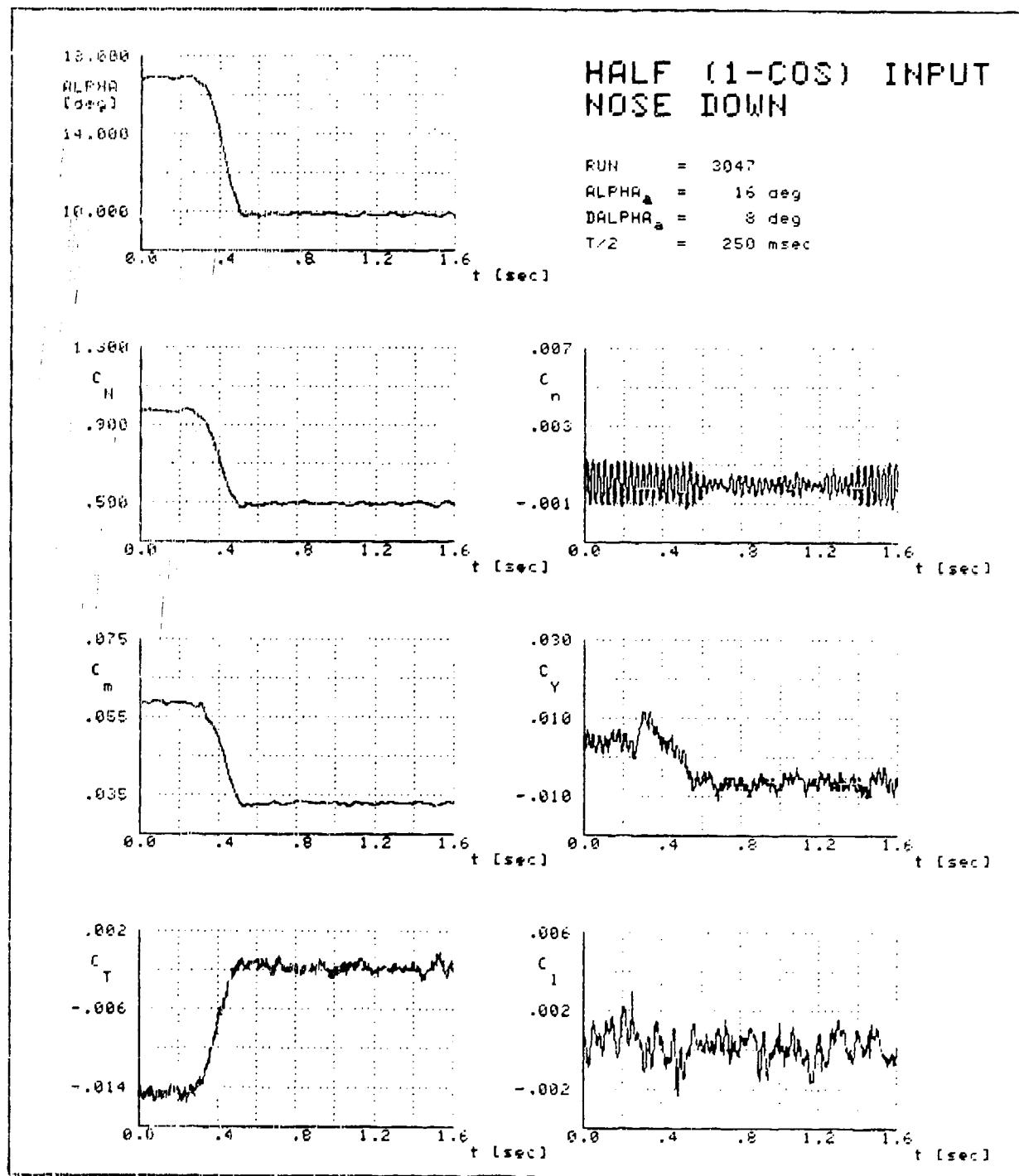


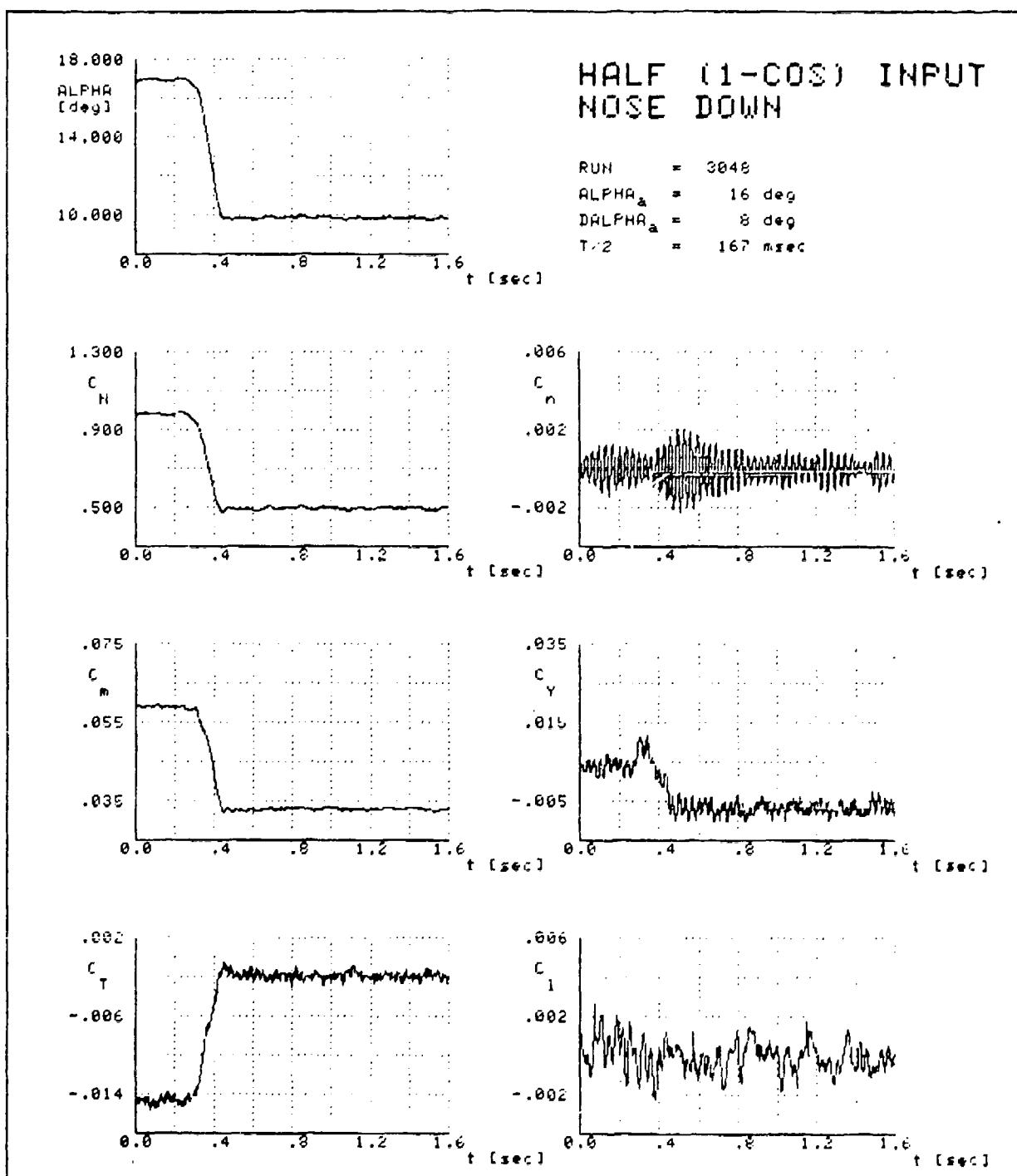


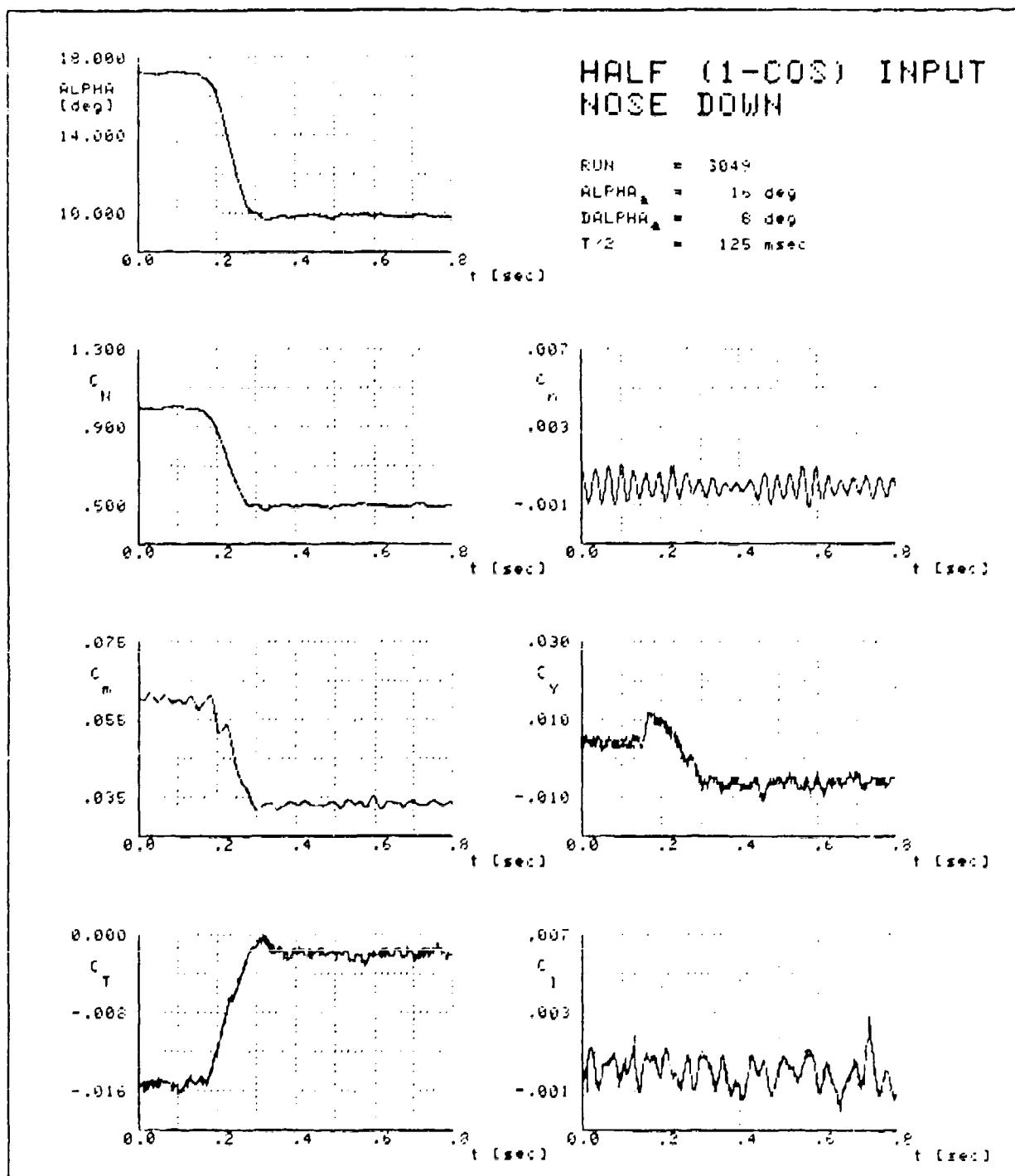


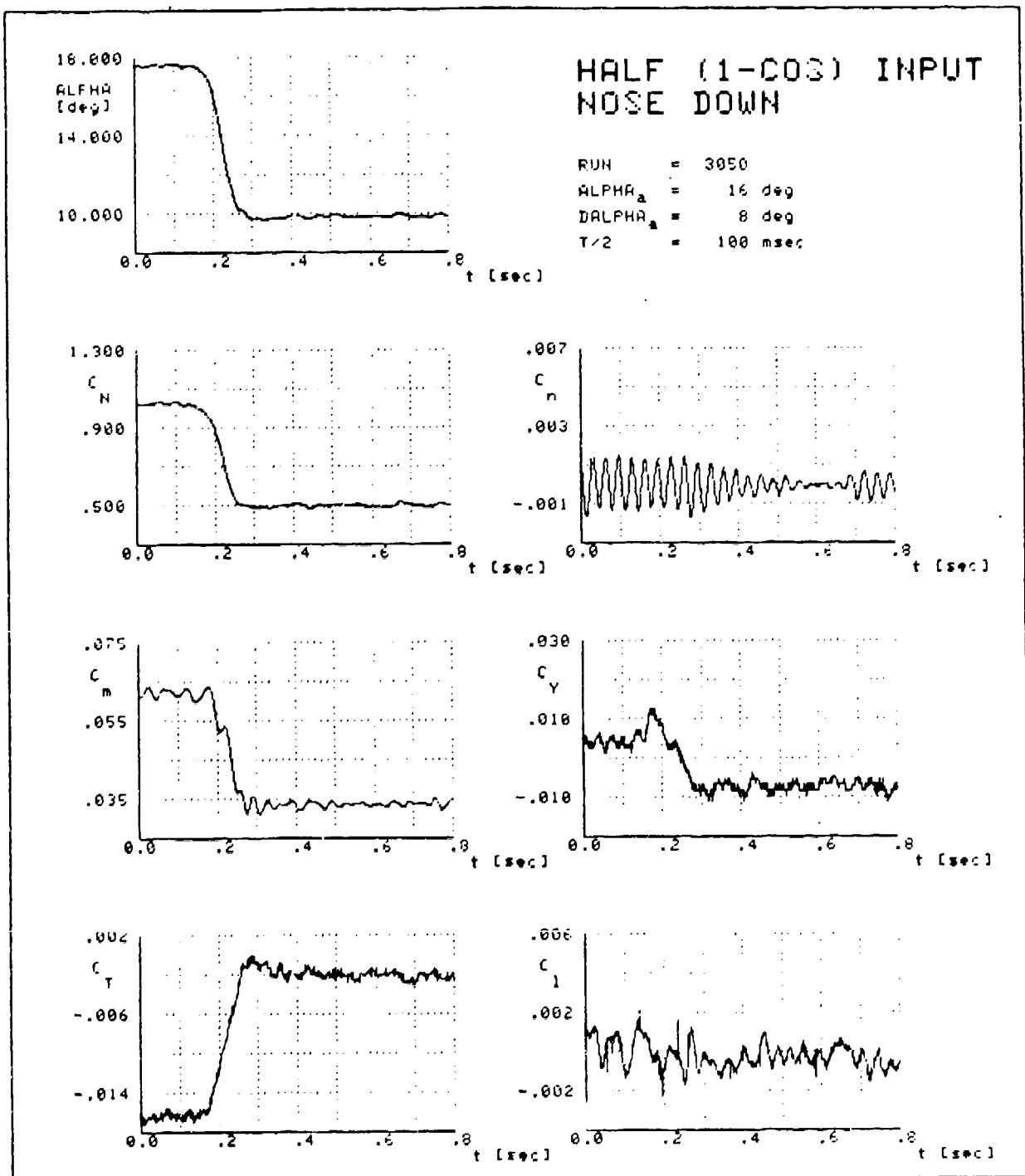


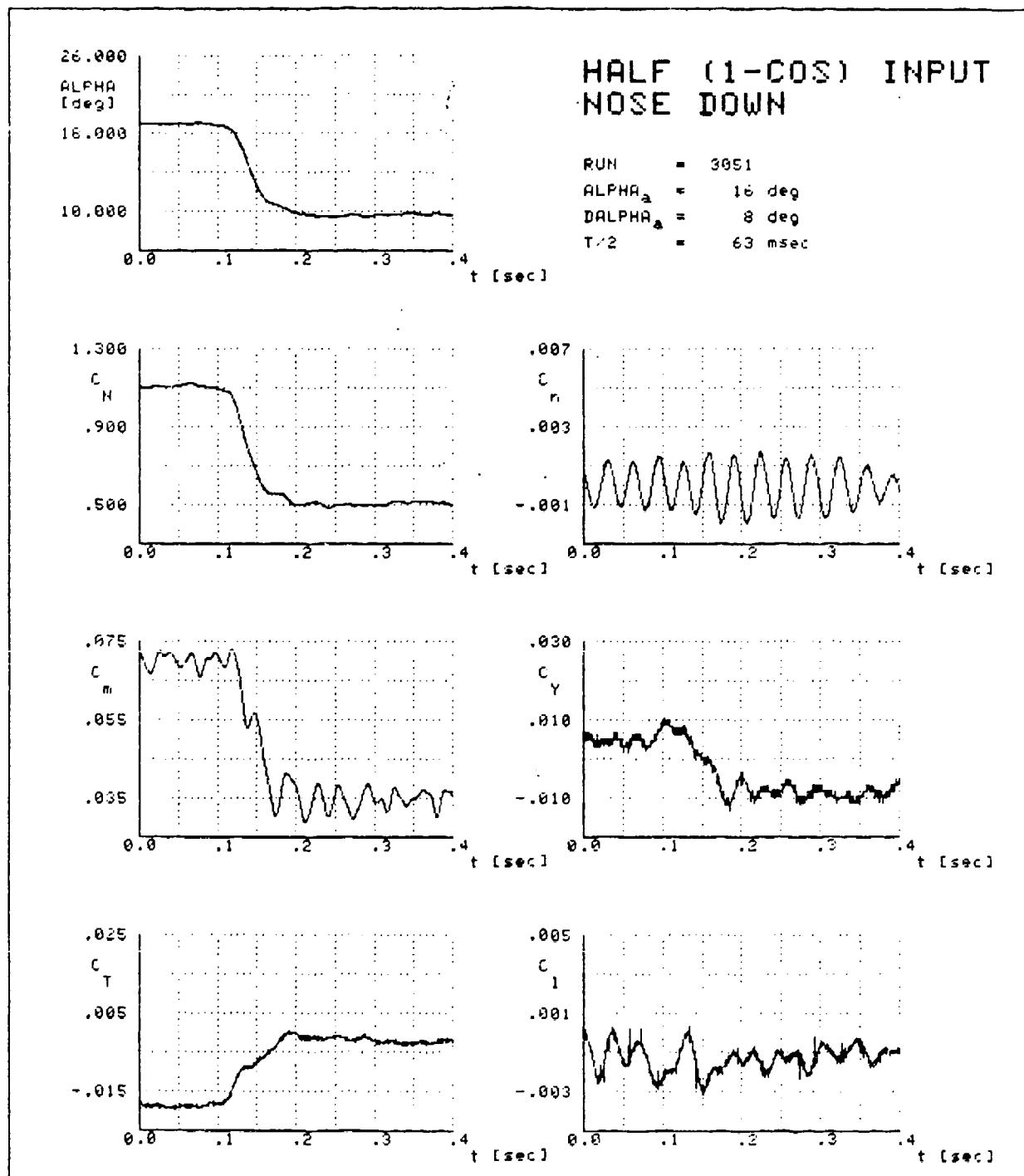


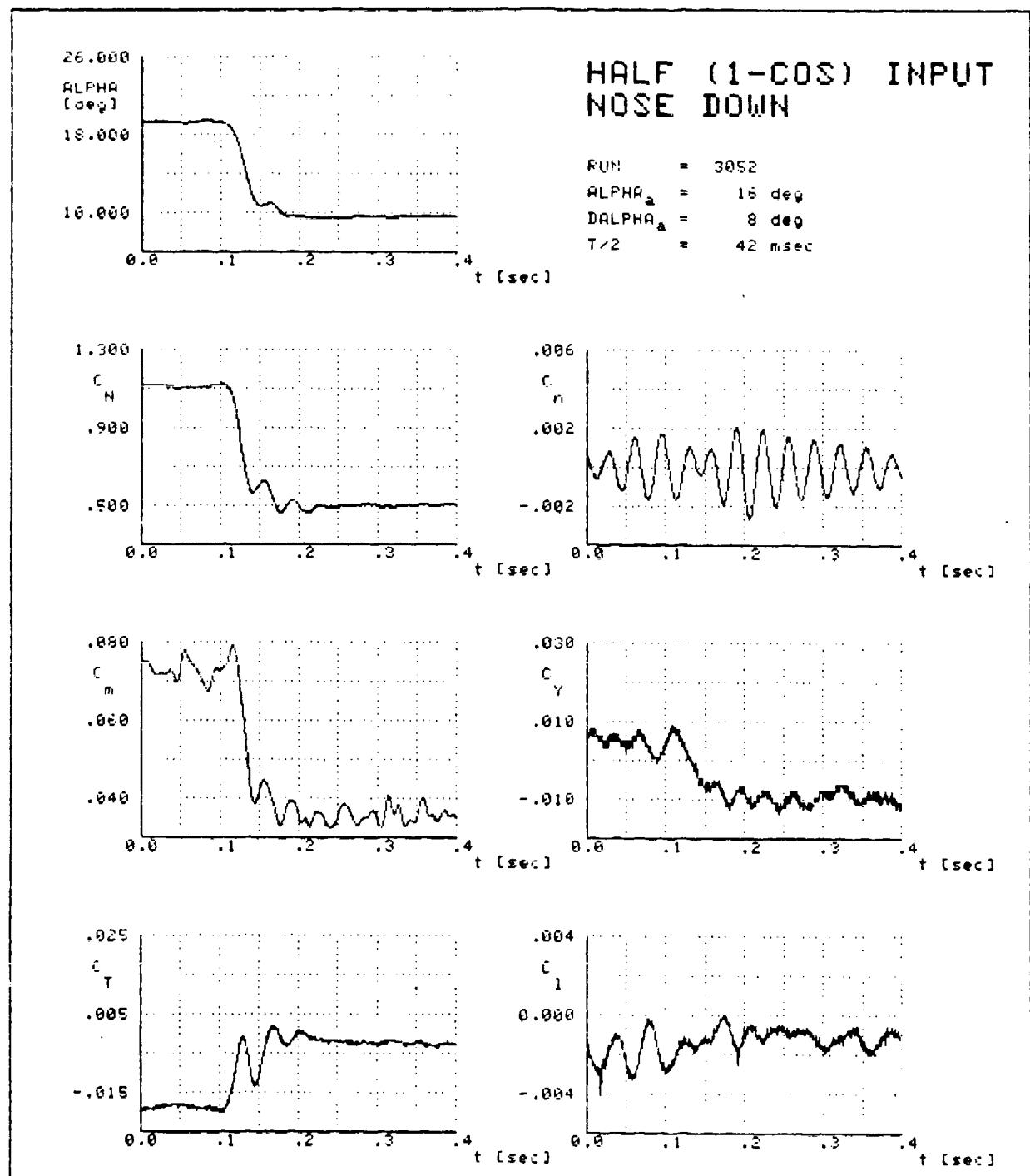


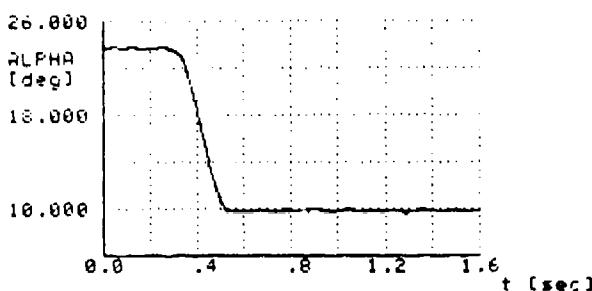






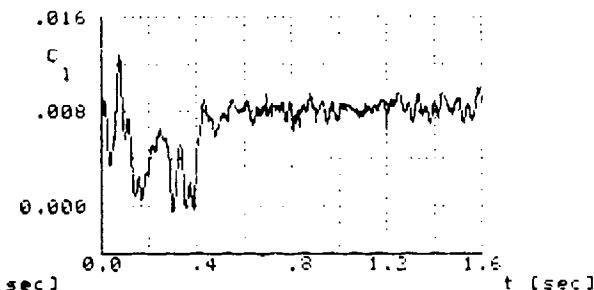
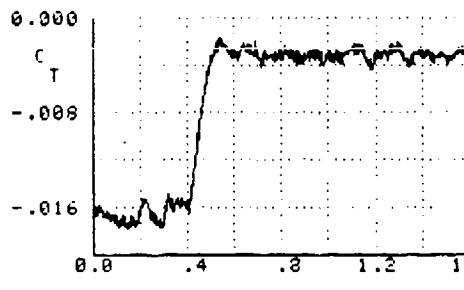
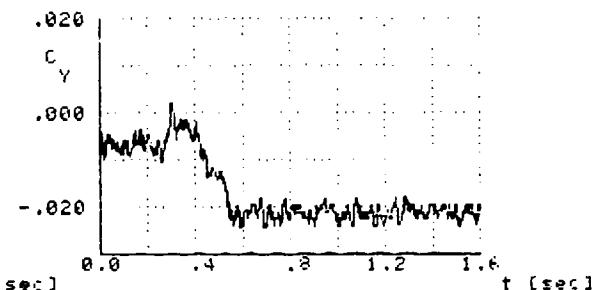
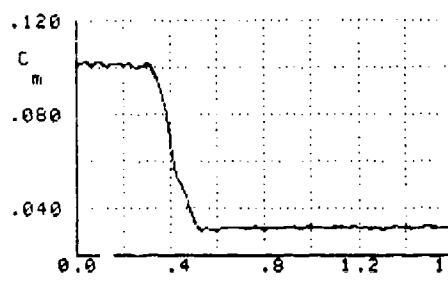
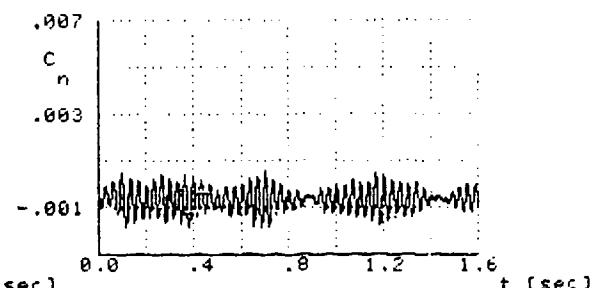
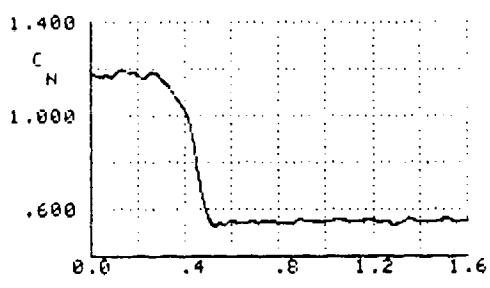


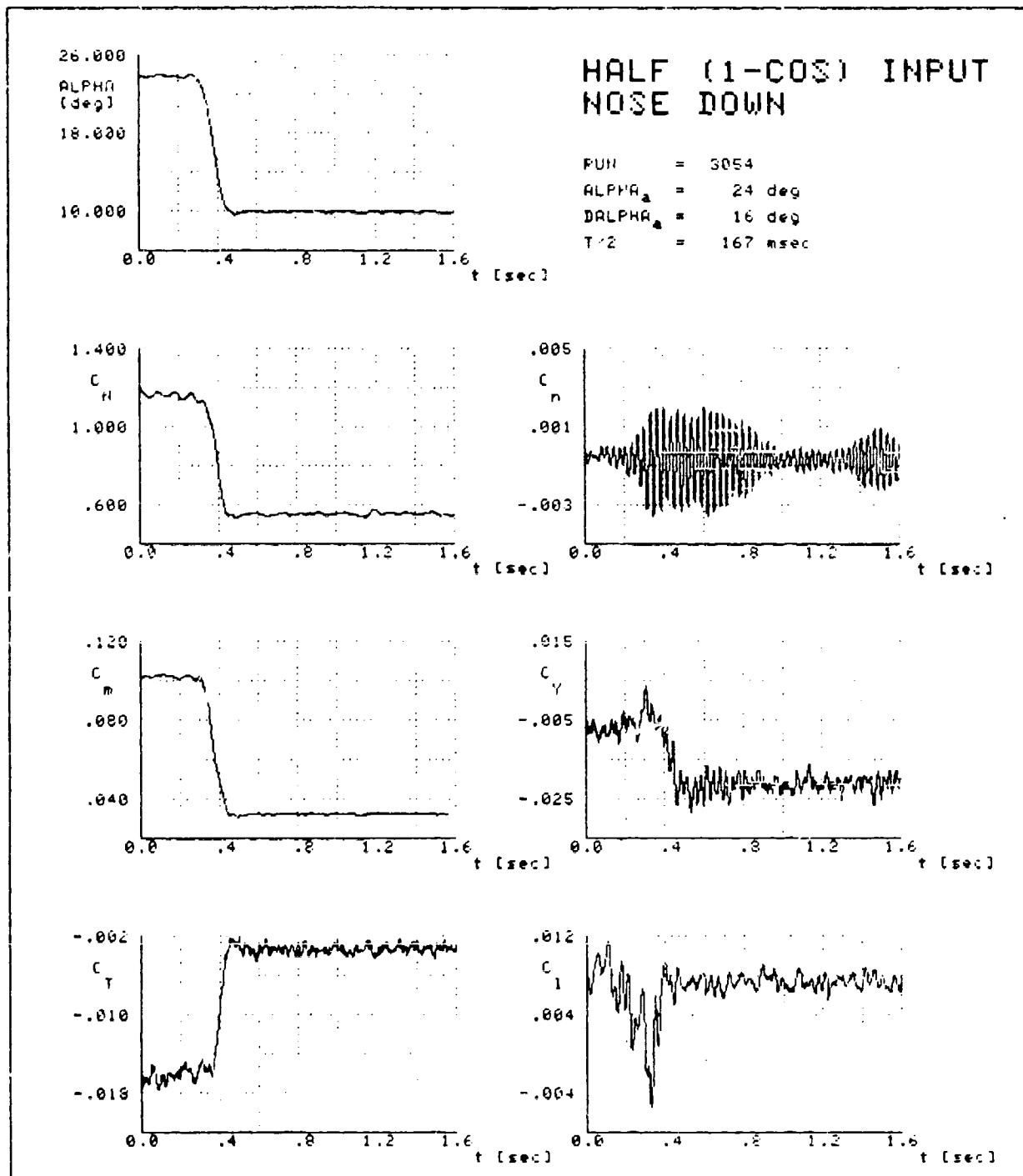


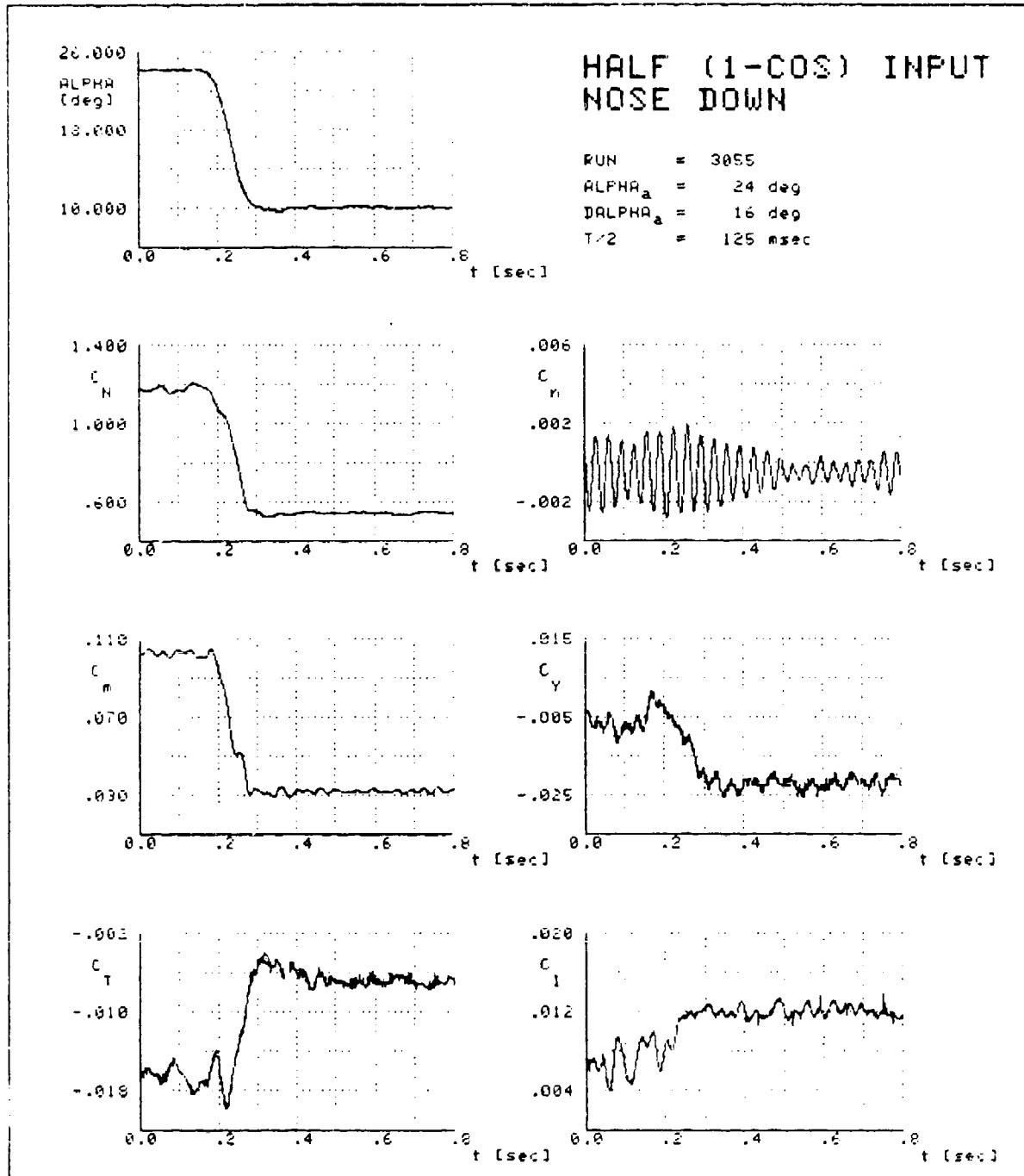


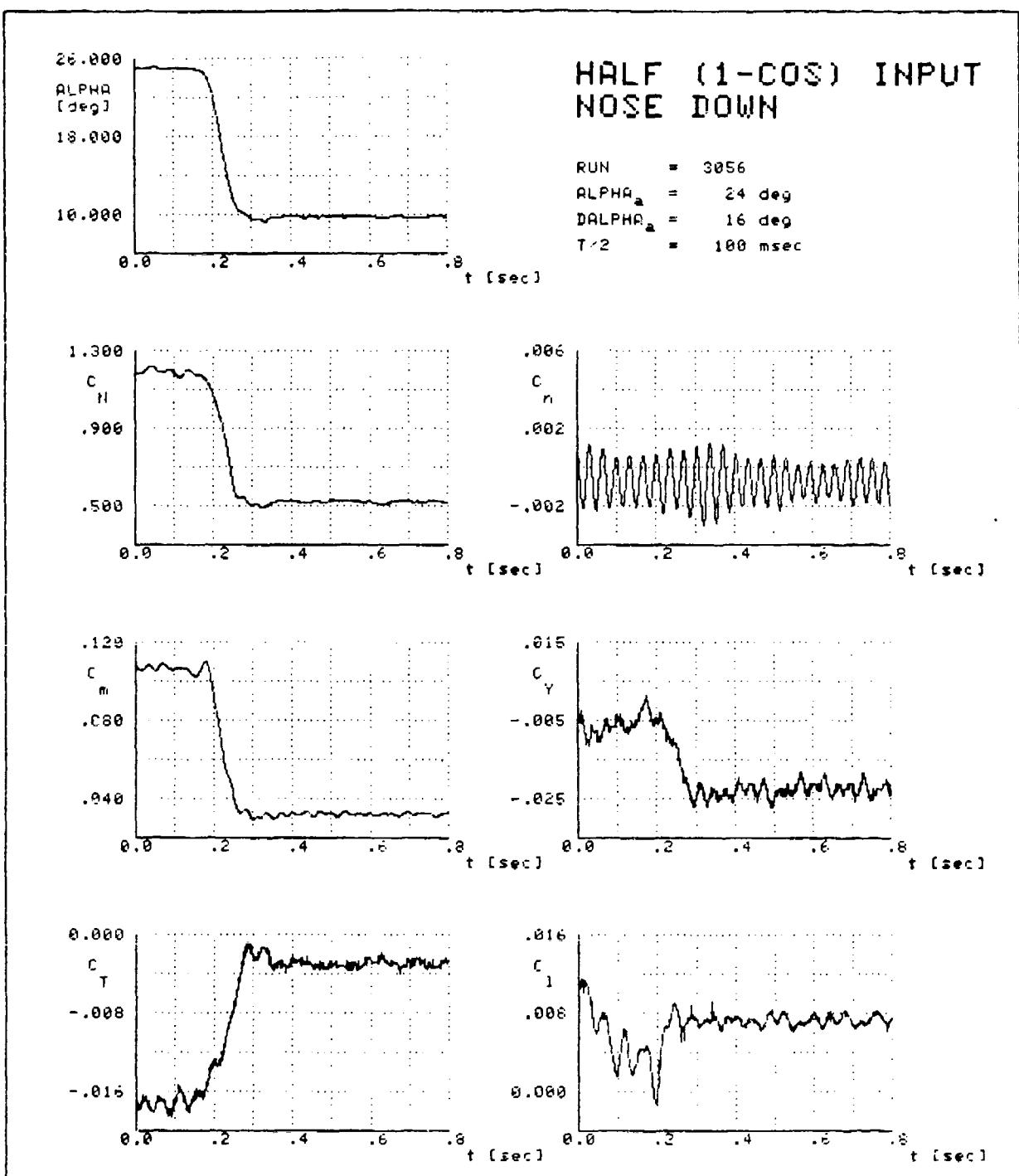
HALF (1-COS) INPUT NOSE DOWN

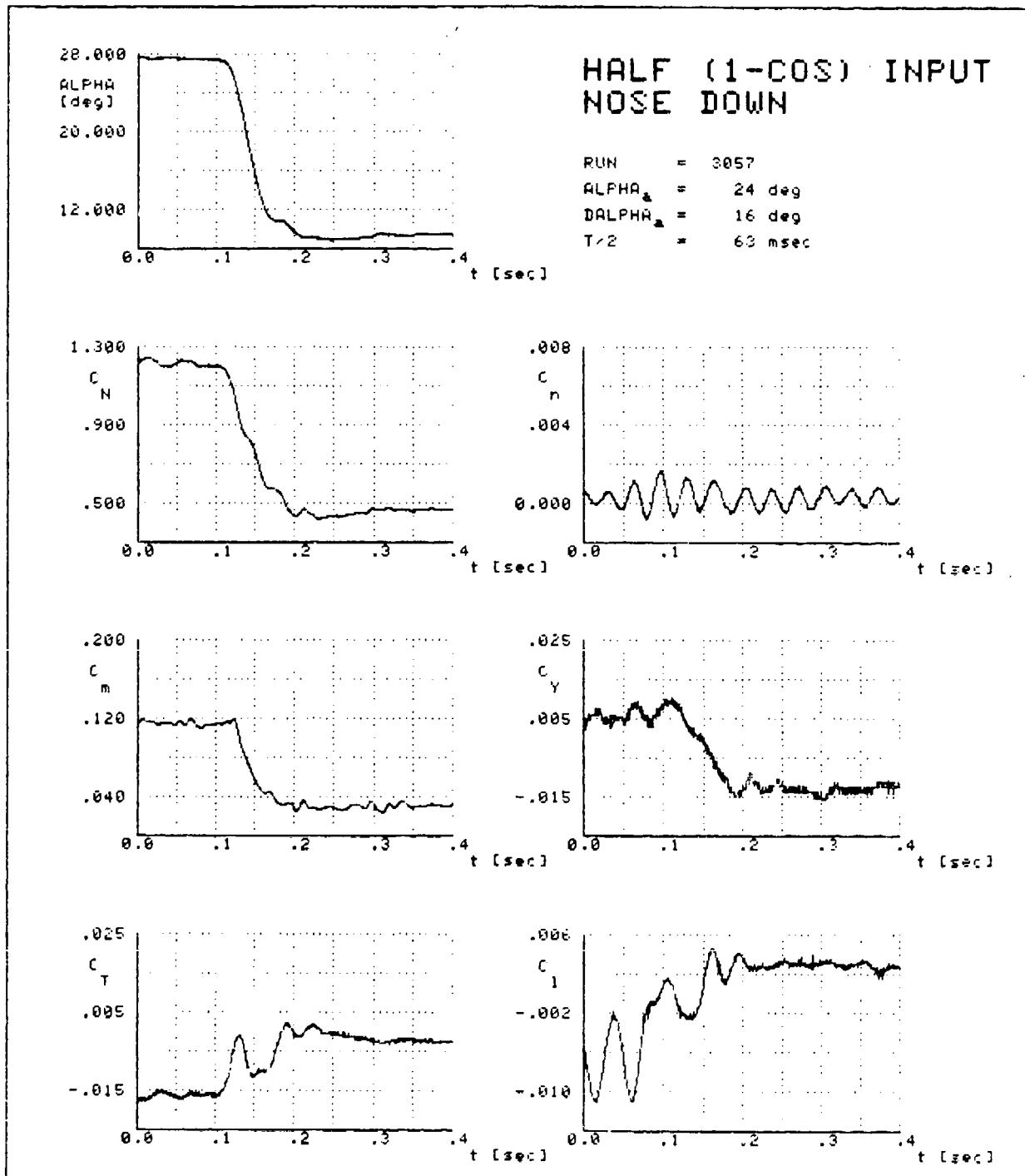
RUN = 3053
ALPHA_a = 24 deg
DALPHA_a = 16 deg
T/2 = 250 msec

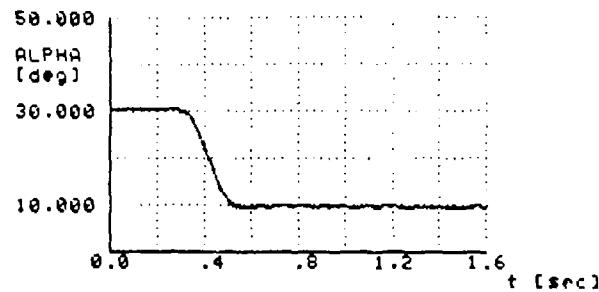






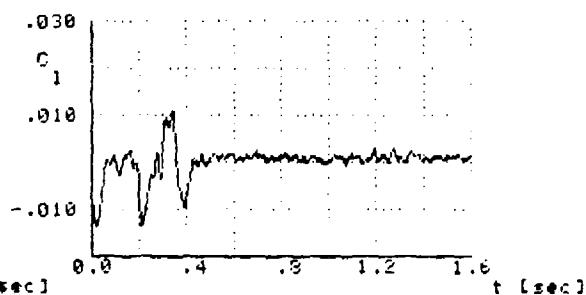
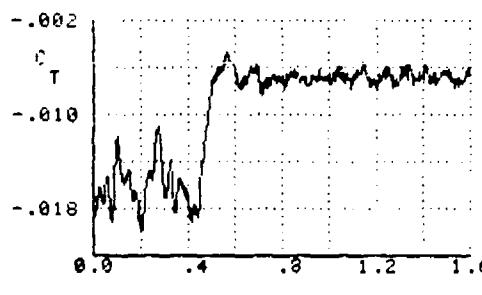
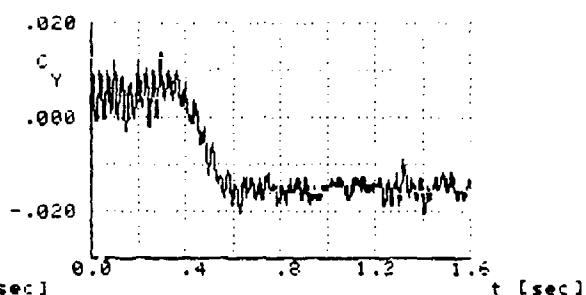
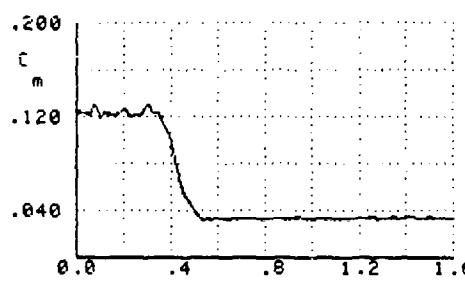
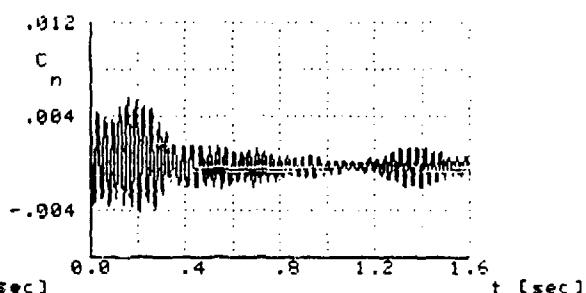
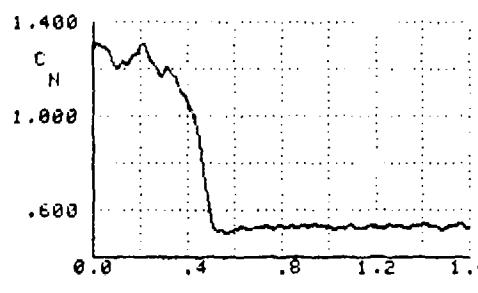


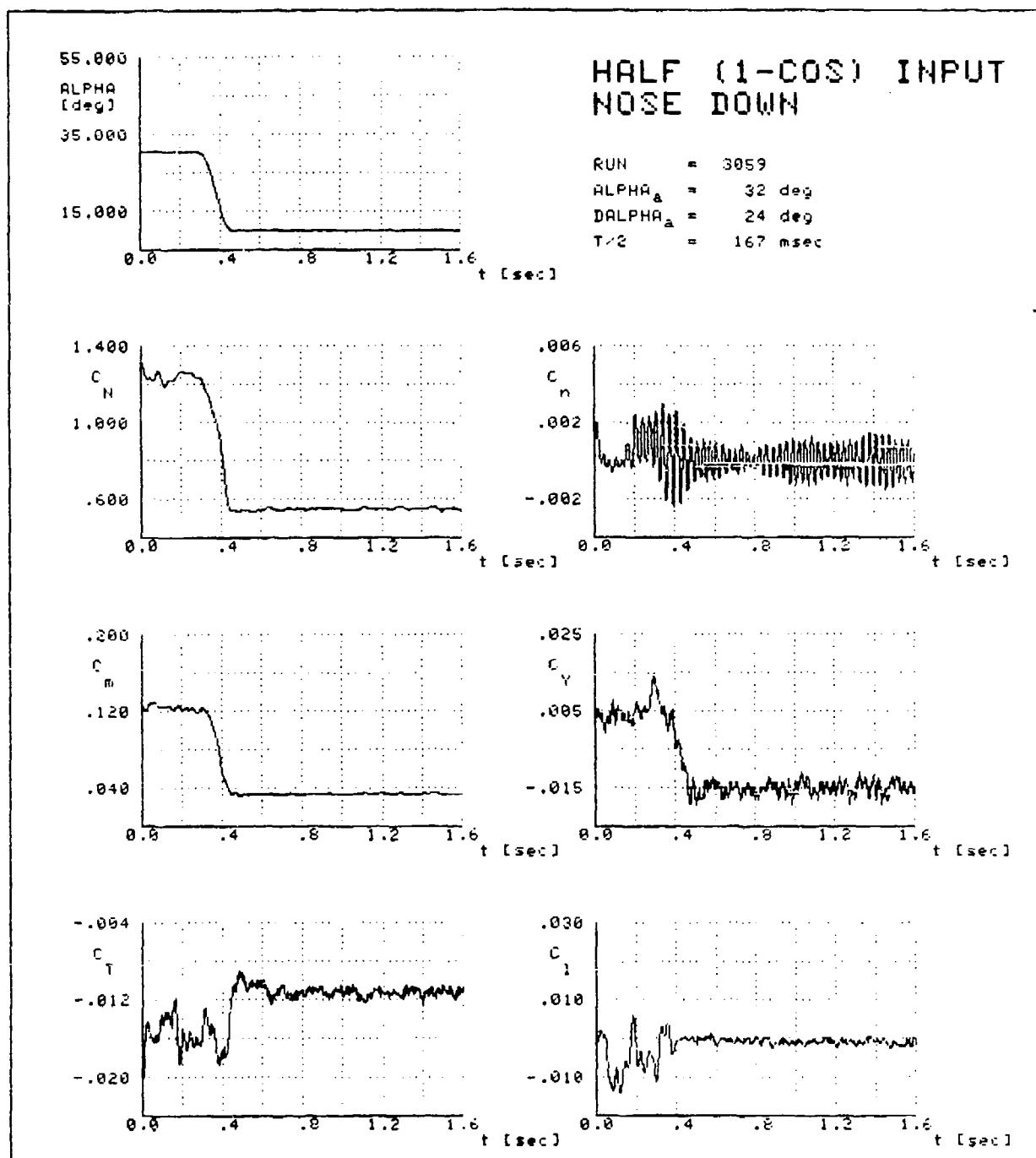


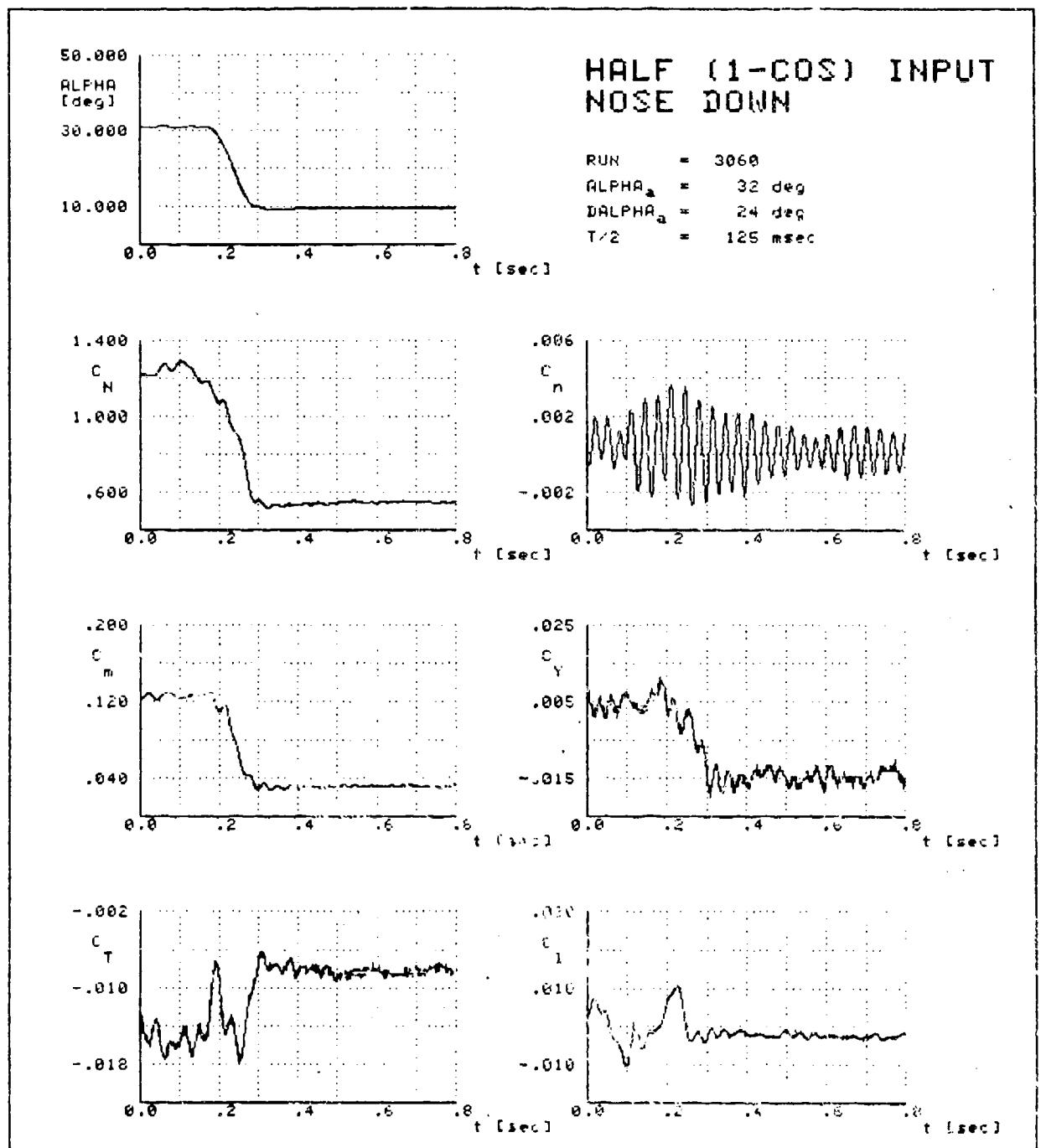


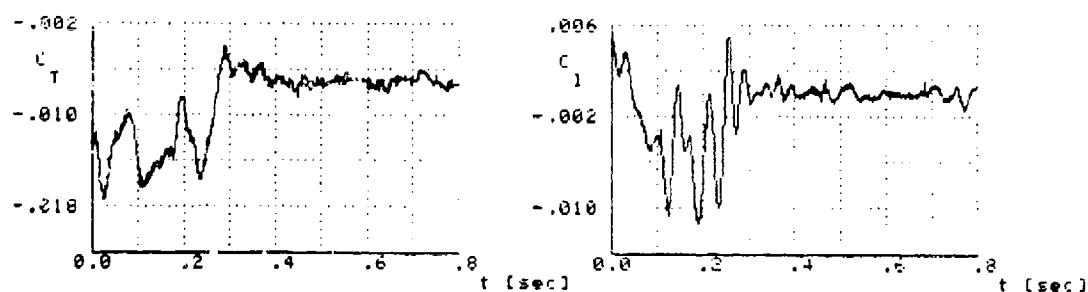
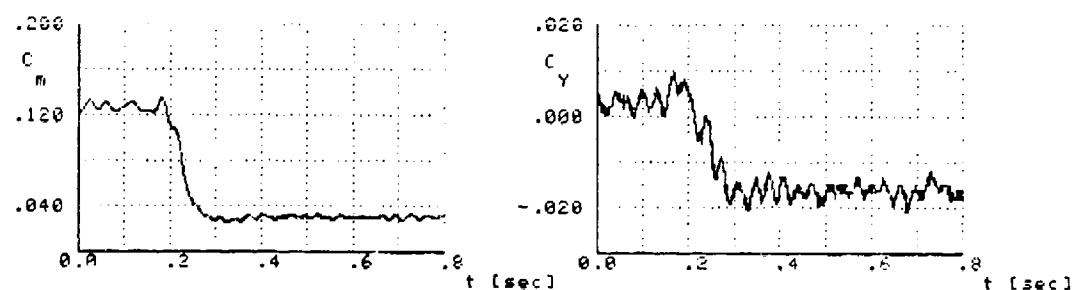
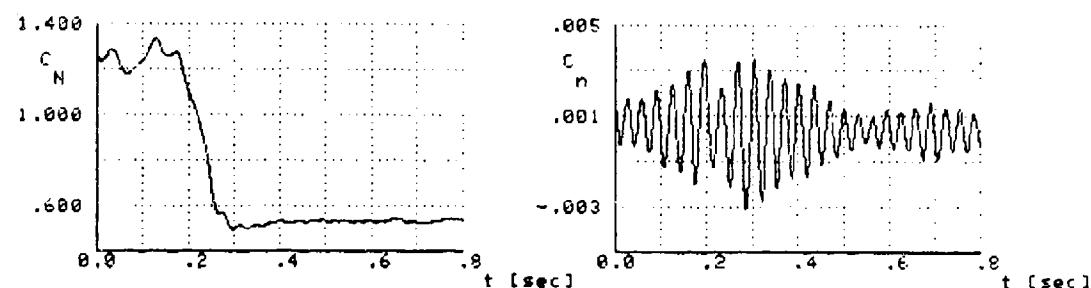
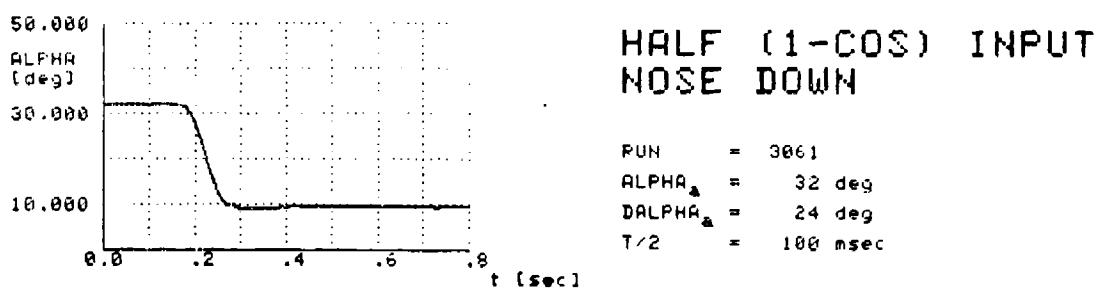
HALF (1-COS) INPUT
NOSE DOWN

RUN = 3058
 $\text{ALPHA}_a = 32 \text{ deg}$
 $\Delta\text{ALPHA}_a = 24 \text{ deg}$
 $T/2 = 250 \text{ msec}$

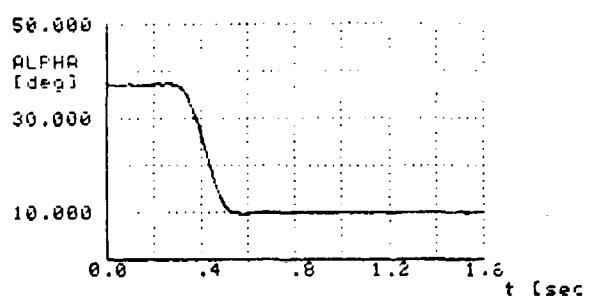




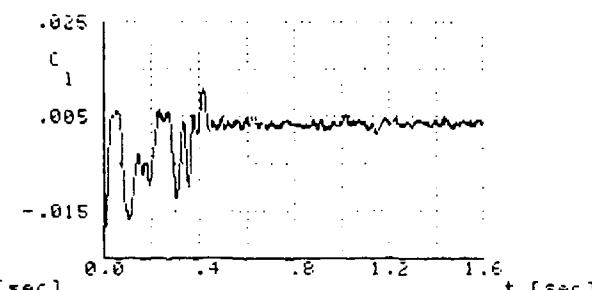
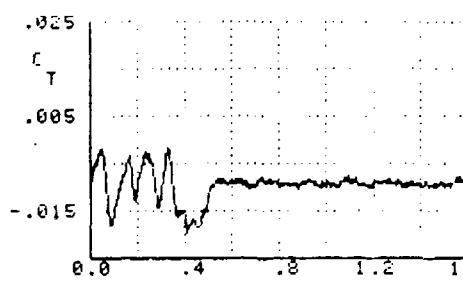
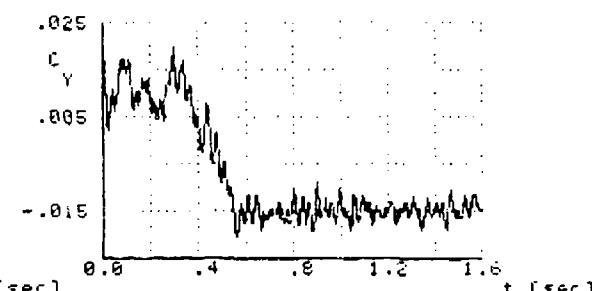
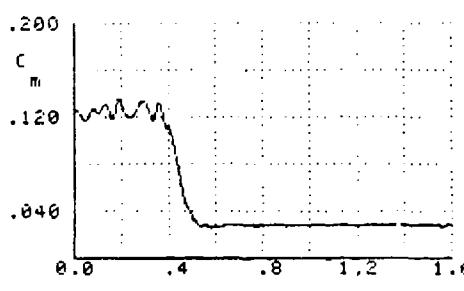
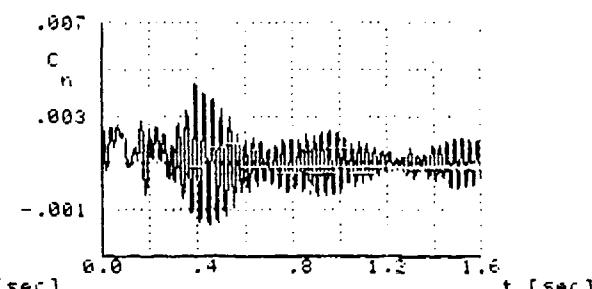
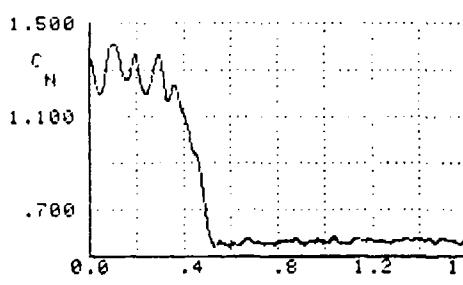


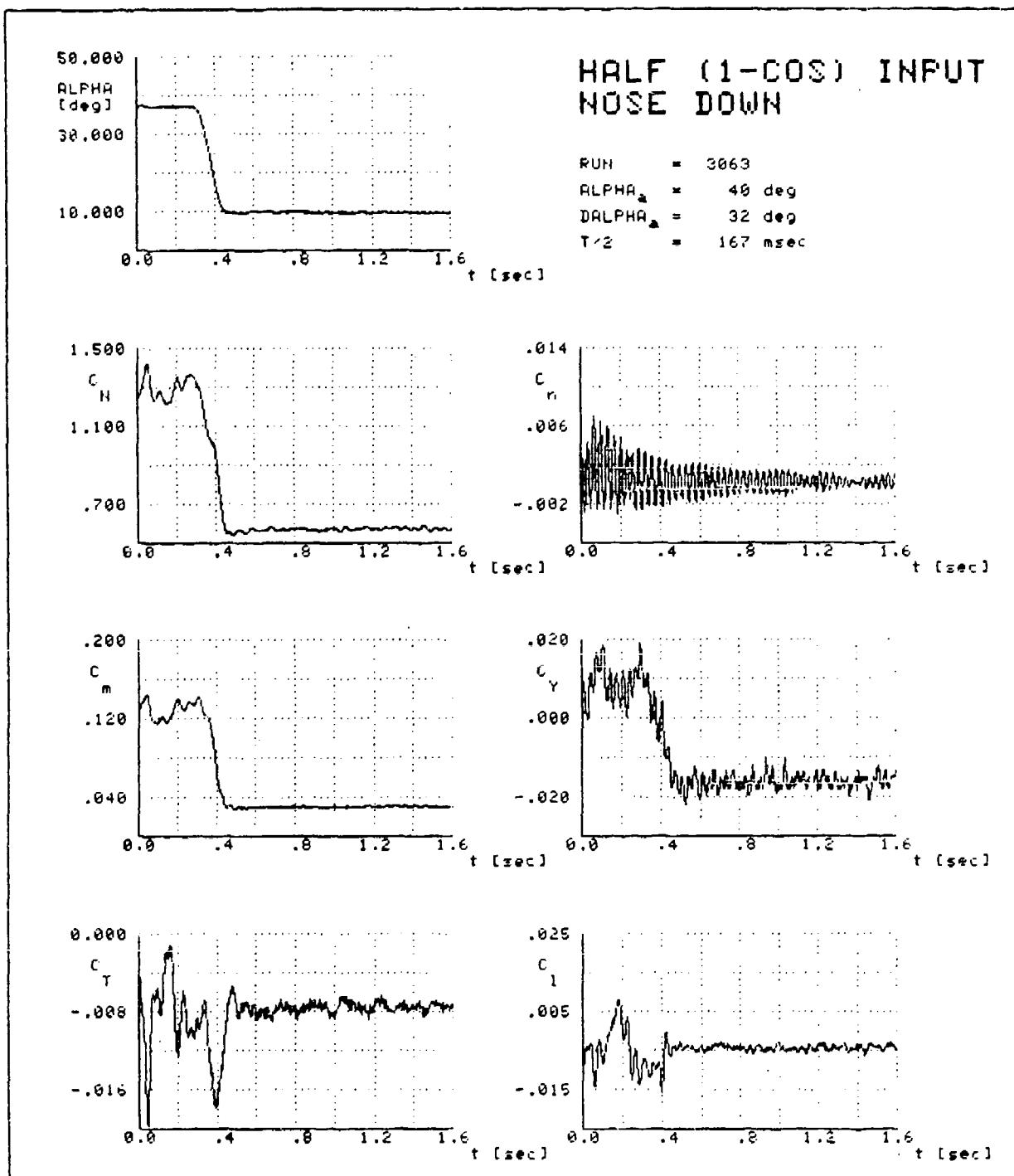


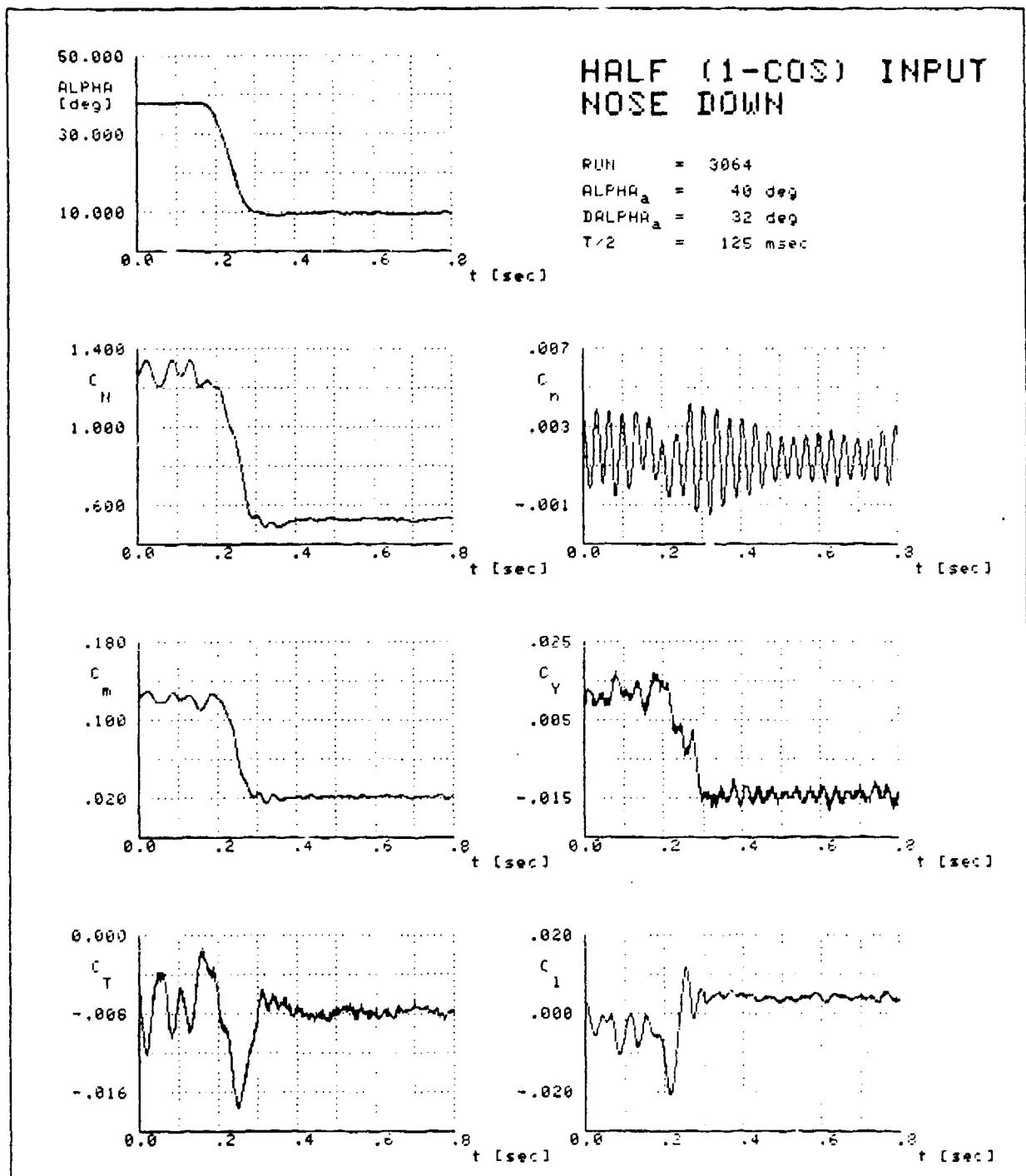
HALF (1-COS) INPUT
NOSE DOWN

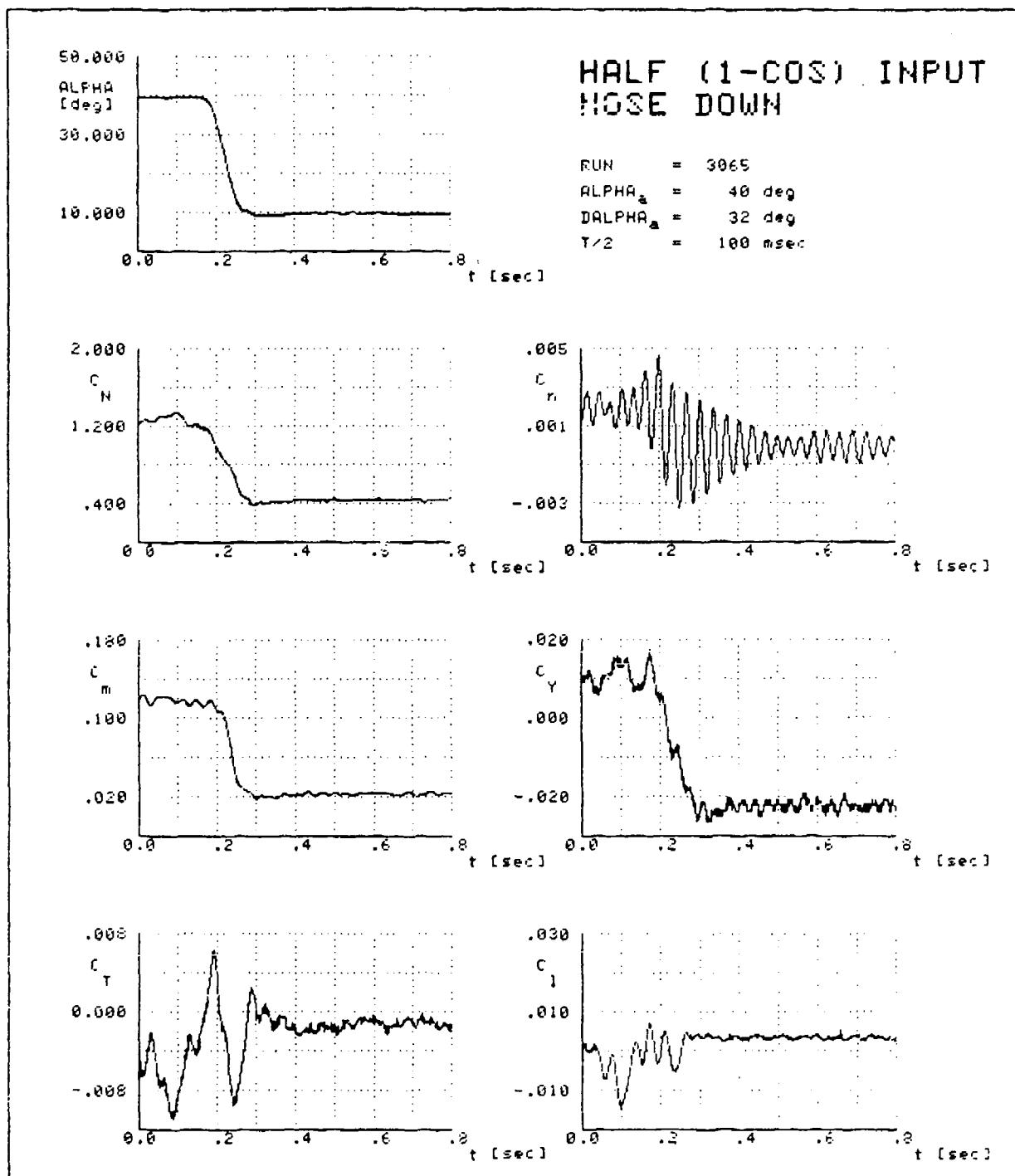


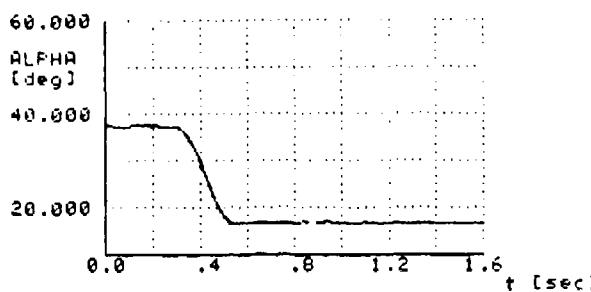
RUN = 3062
ALPHA_a = 40 deg
DALPHA_a = 32 deg
T/2 = 250 msec





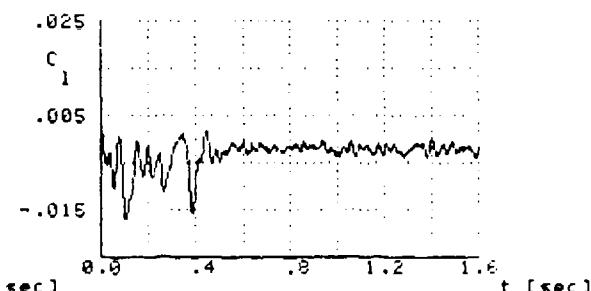
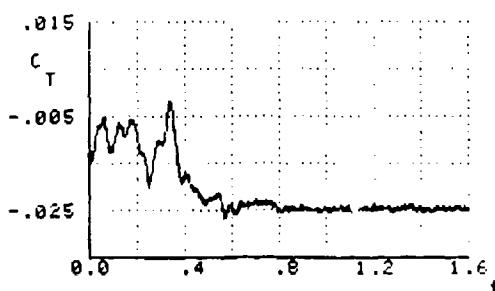
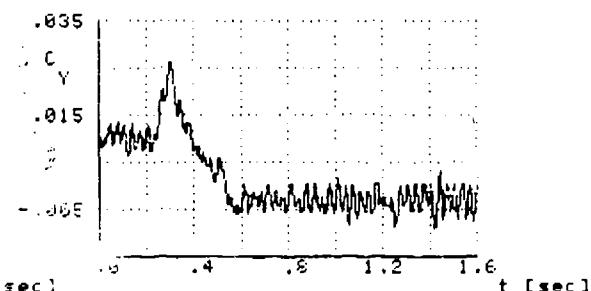
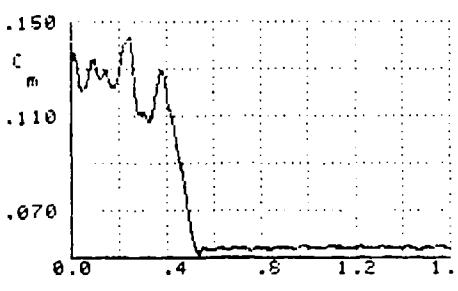
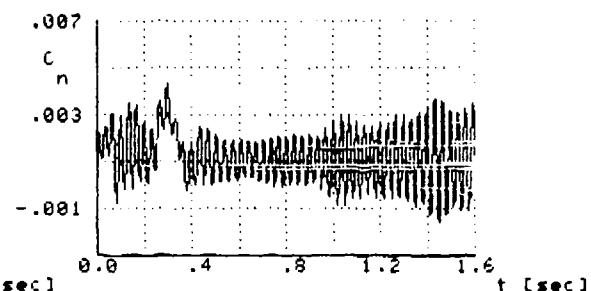
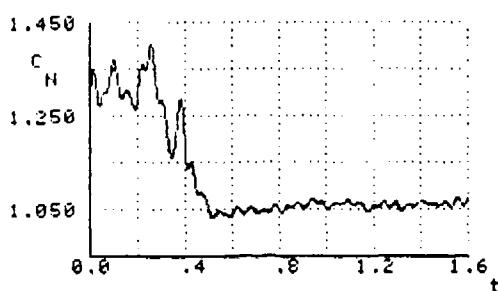


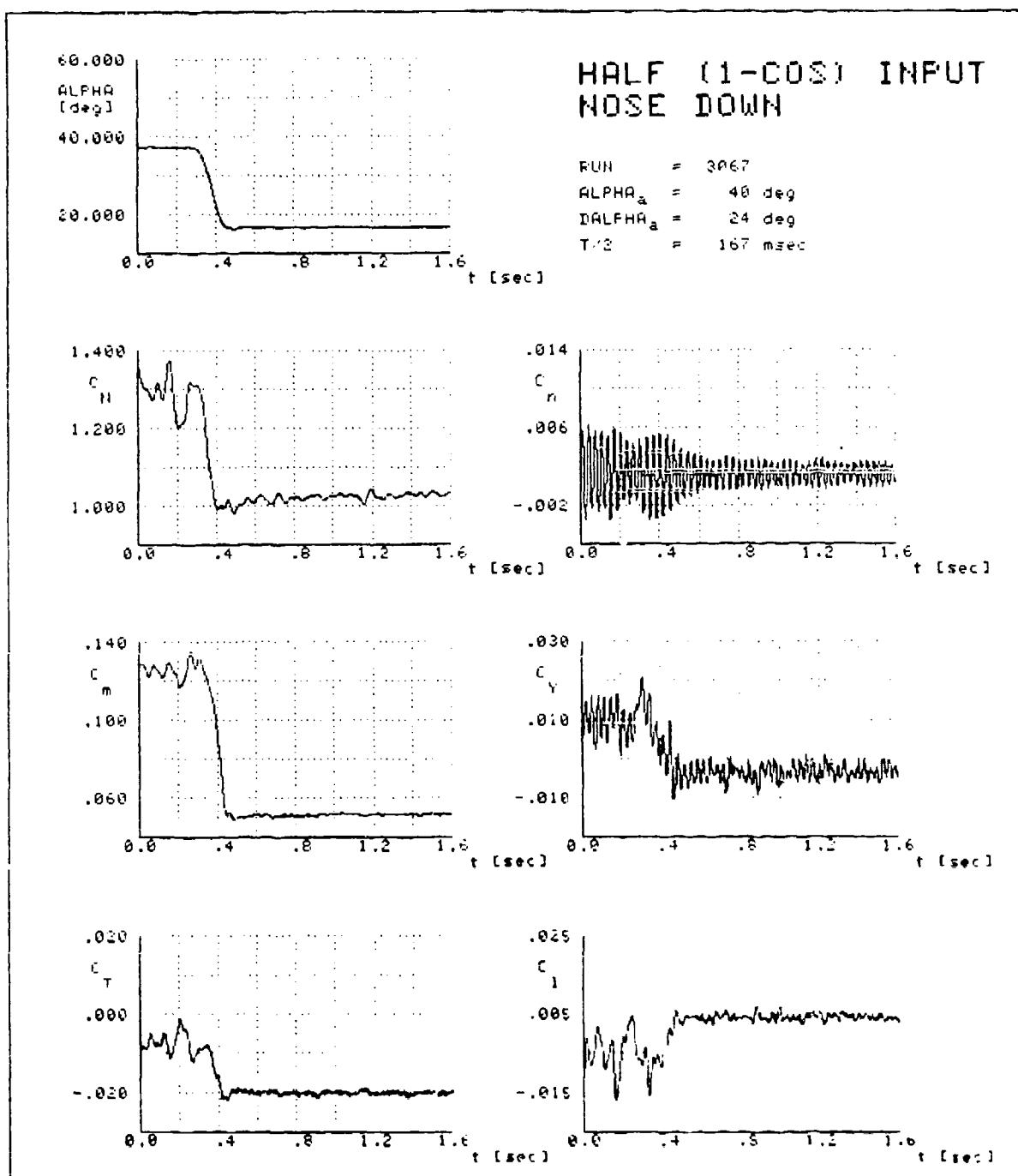


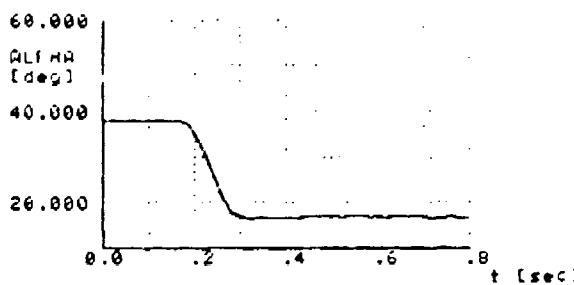


HALF (1-COS) INPUT NOSE DOWN

RUN = 3066
ALPHA_a = 40 deg
DALPHA_a = 24 deg
T/2 = 250 msec

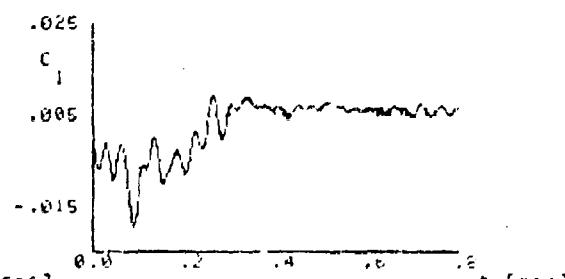
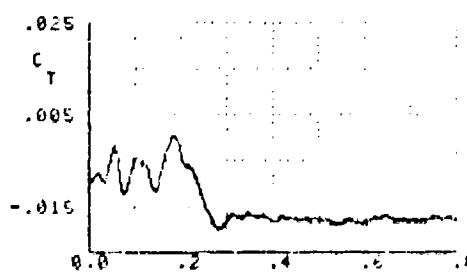
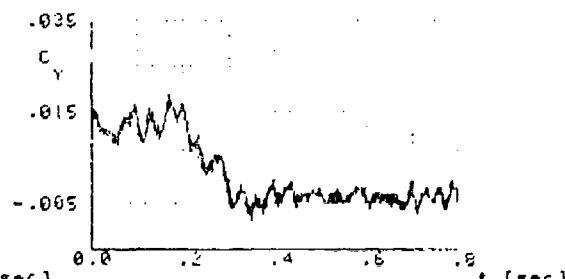
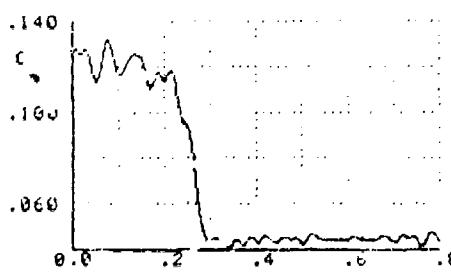
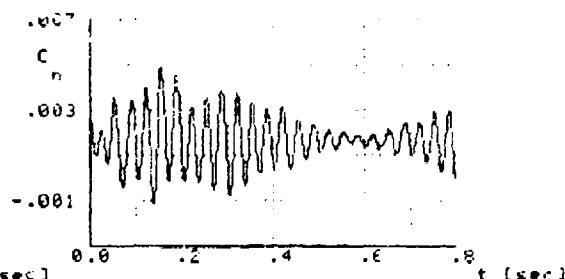
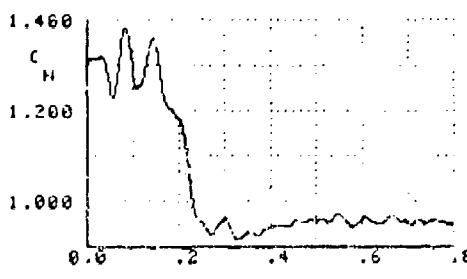


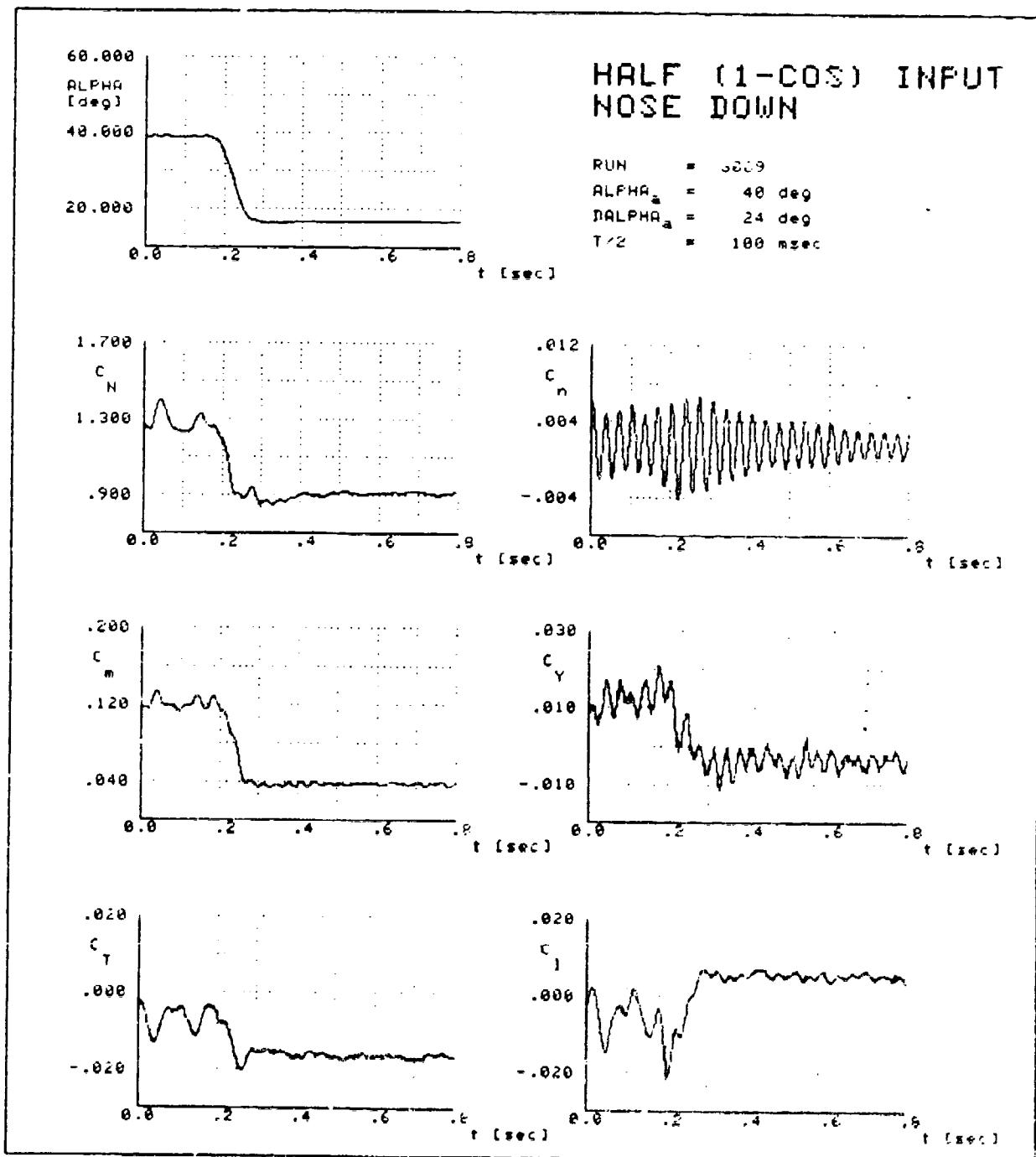


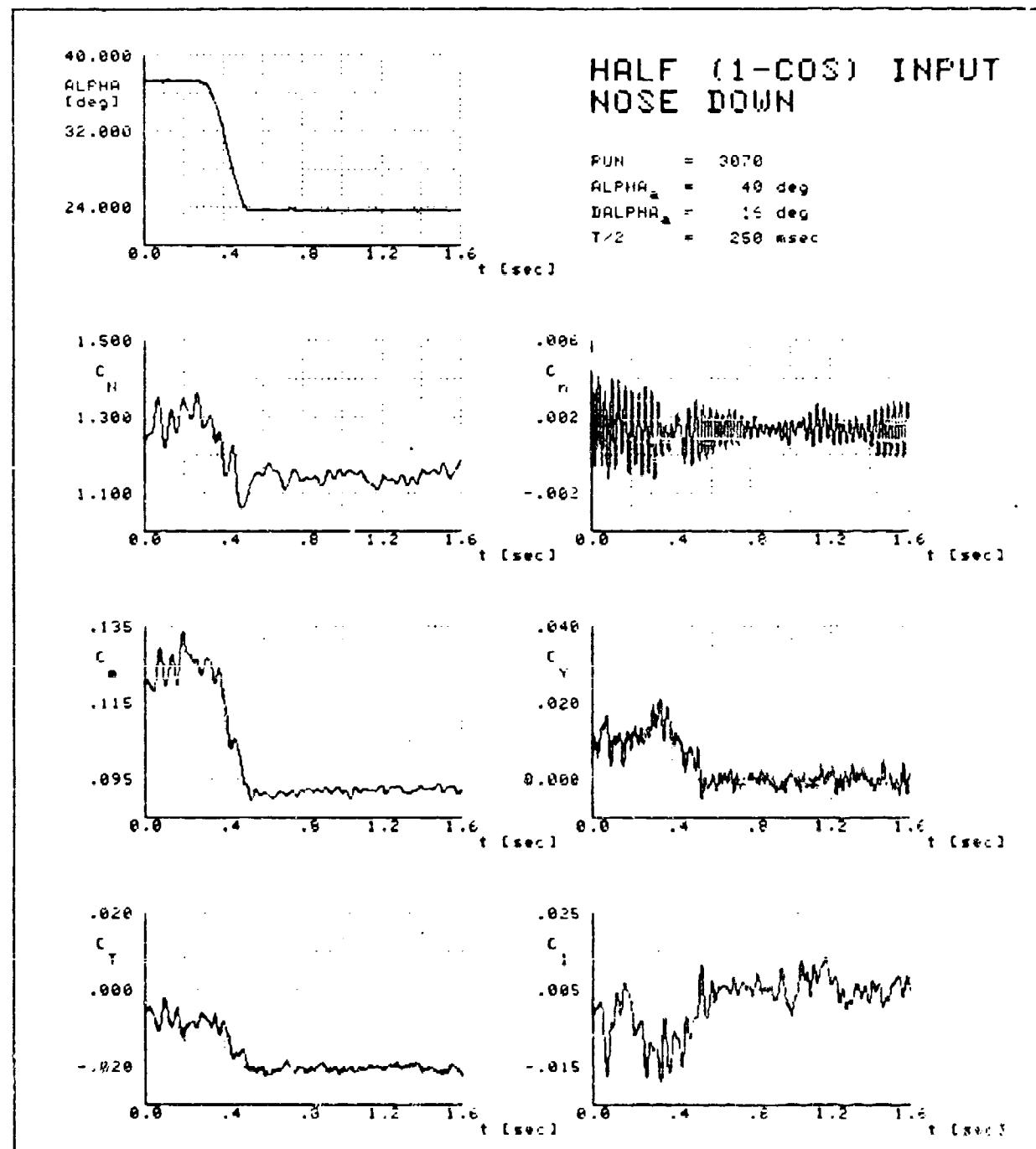


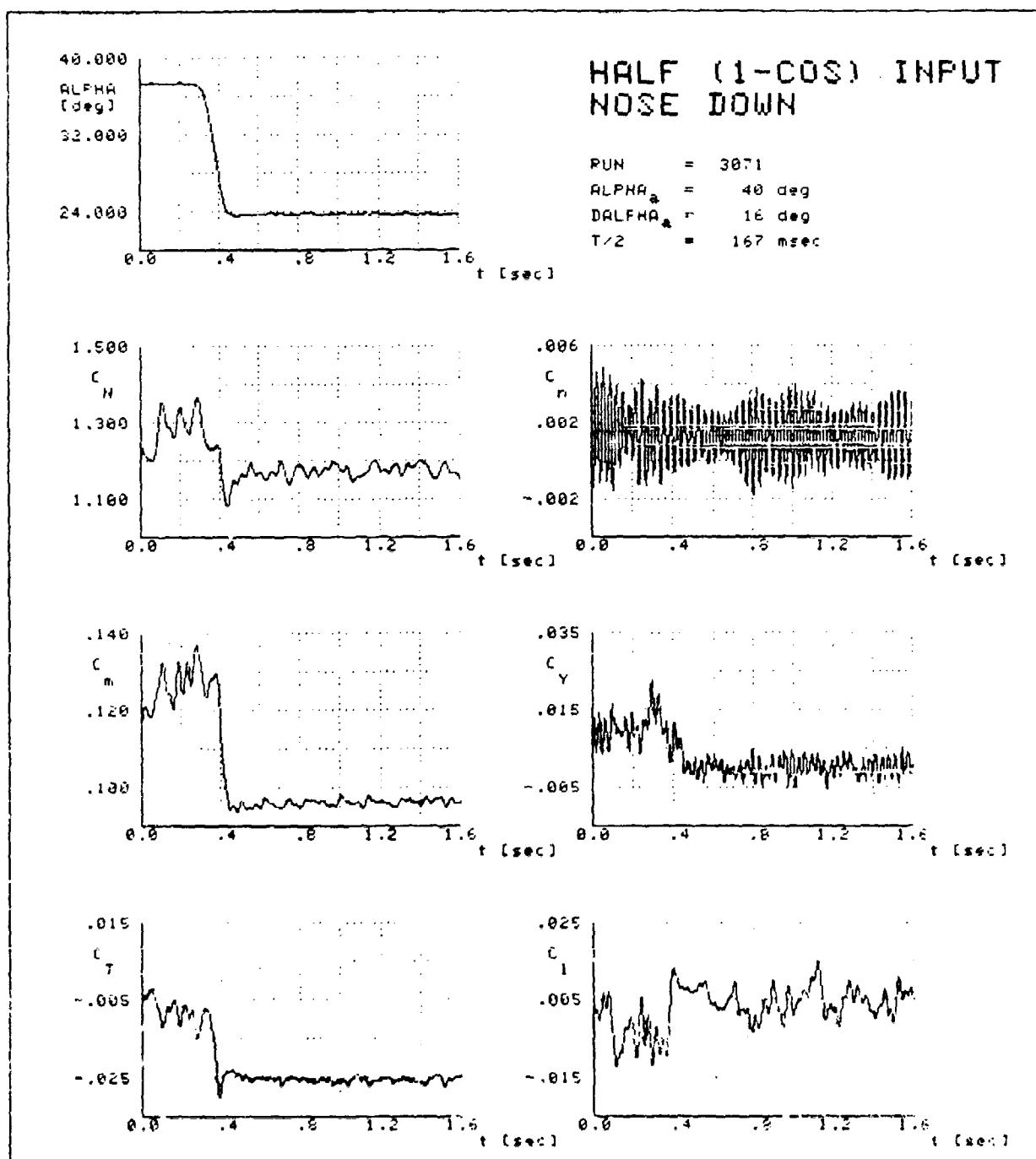
HALF (1-COS) INPUT NOSE DOWN

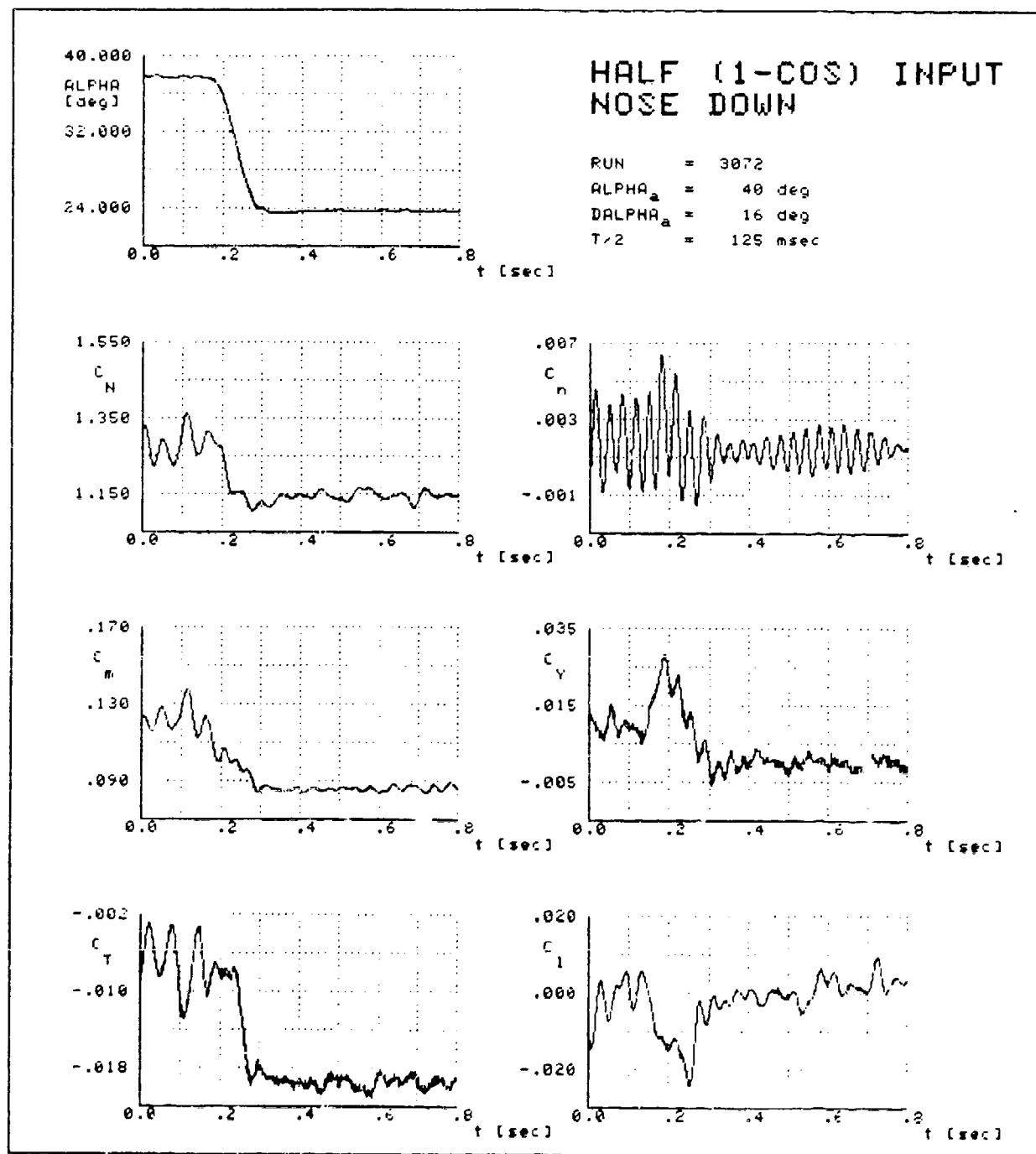
RUN = 3068
ALPHA_a = 40 deg
DALPHA_a = 24 deg
T/2 = 125 msec

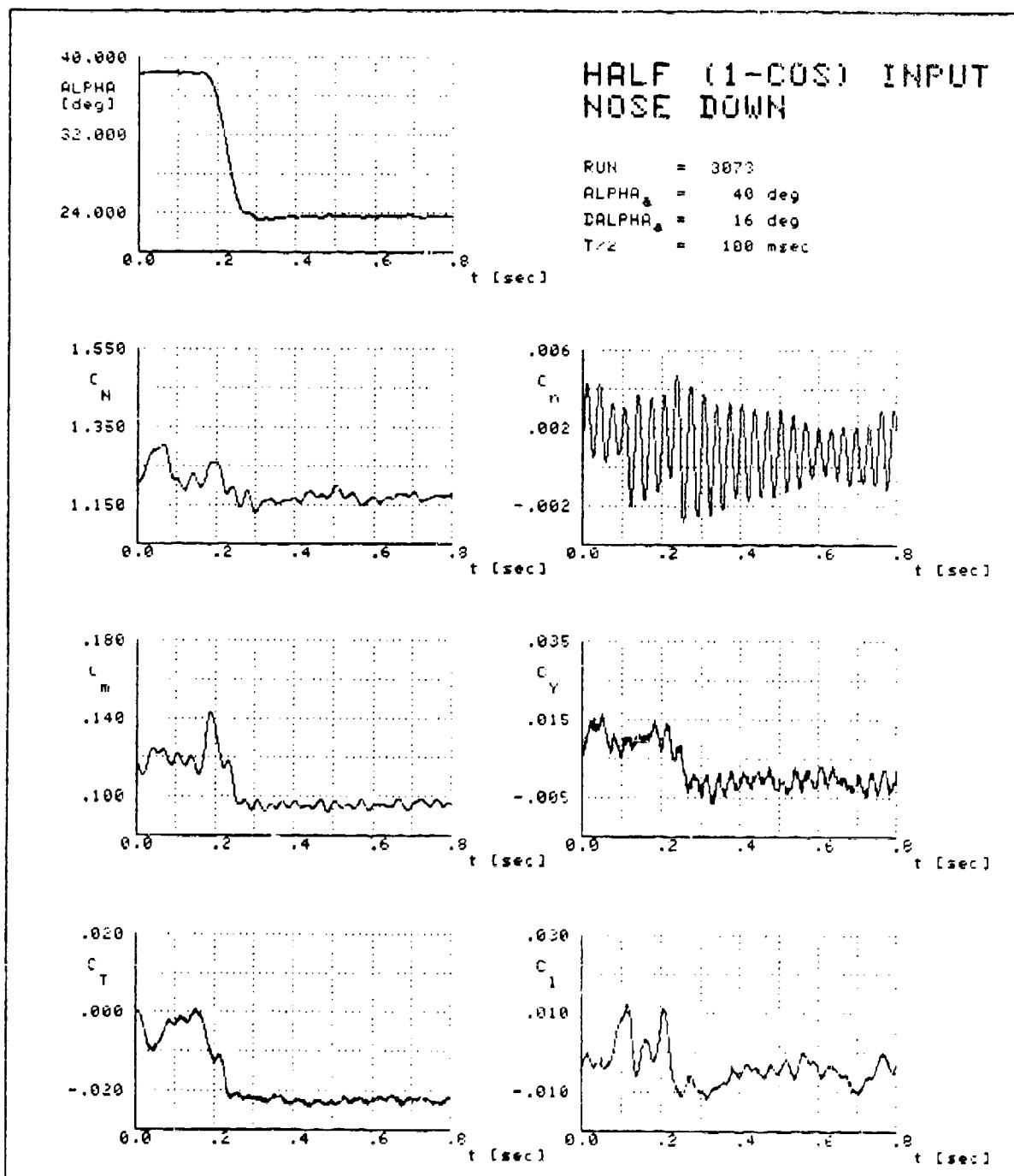












HALF (1-COS) INPUT
NOSE DOWN

42.000

ALPHA

[deg]

34.003

26.000

0.0 .1 .2 .3 .4
t [sec]

RUN = 3074

ALPHA_a = 40 deg

DALPHHA_a = 16 deg

T/2 = 63 msec

1.400

C

H

1.200

1.000

0.800

0.0 .1 .2 .3 .4
t [sec]

.010

C

n

.002

-.004

-.006

0.0 .1 .2 .3 .4
t [sec]

.150

C

R

.110

.070

0.0 .1 .2 .3 .4
t [sec]

.030

C

Y

.010

-.010

0.0 .1 .2 .3 .4
t [sec]

.020

C

T

.000

-.020

.025

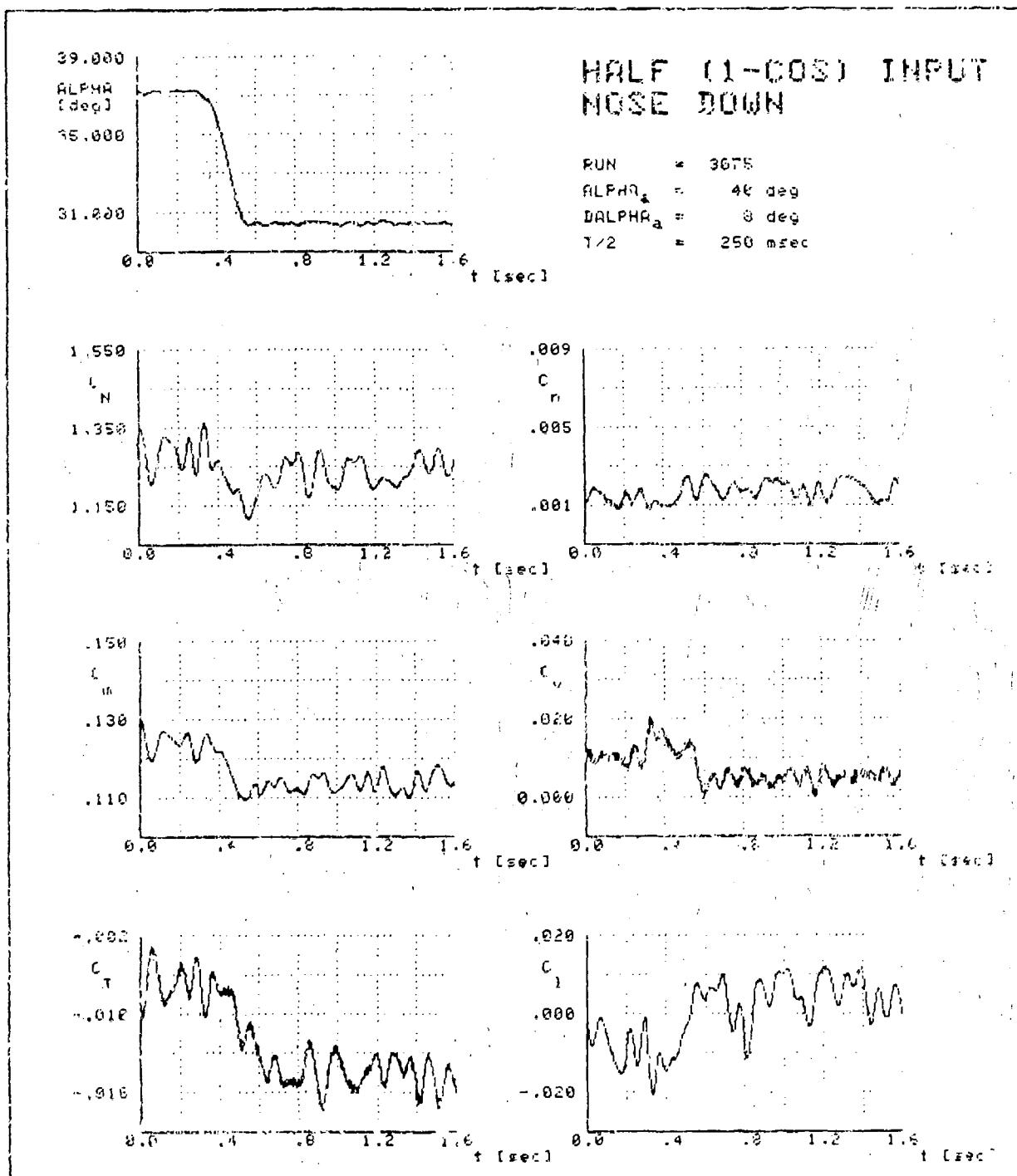
C

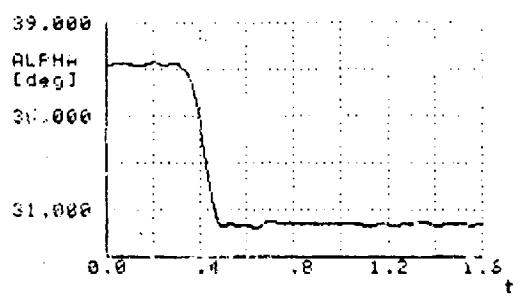
I

.005

-.015

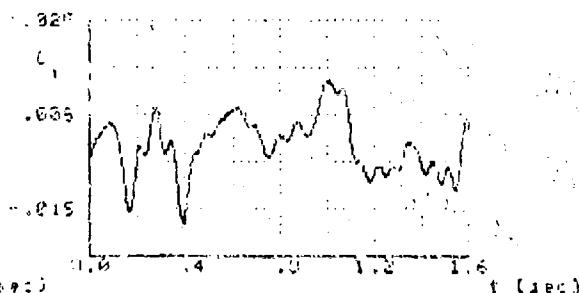
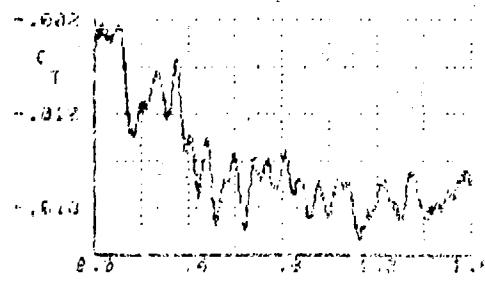
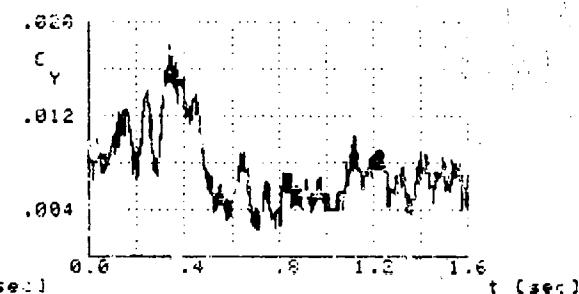
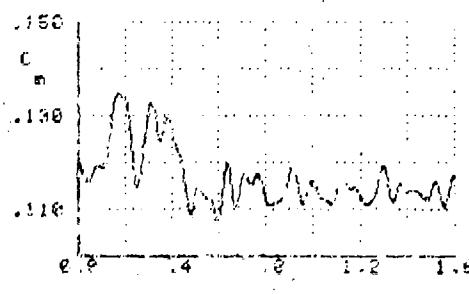
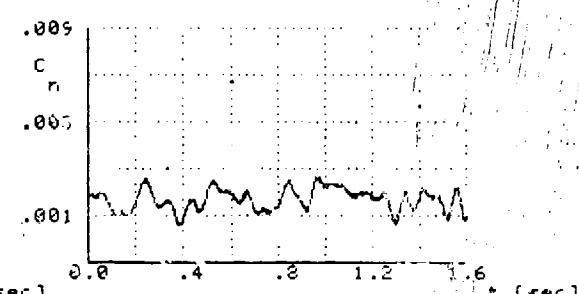
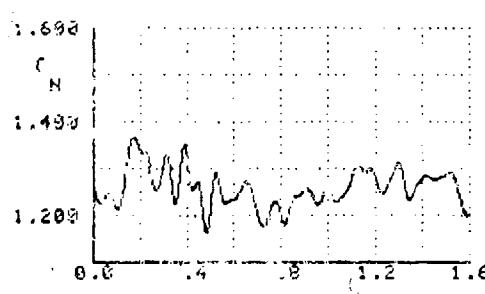
0.0 .1 .2 .3 .4
t [sec]

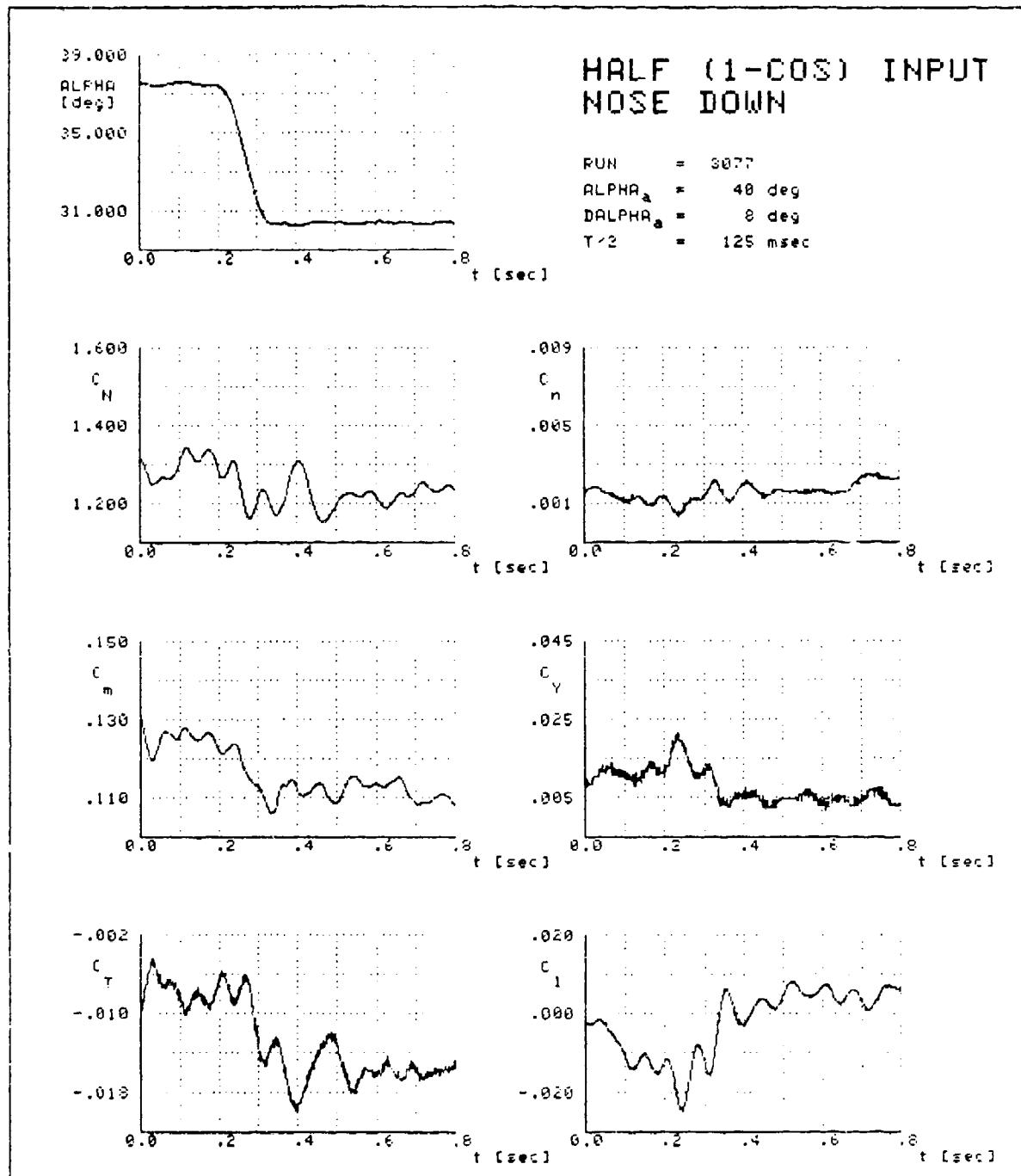


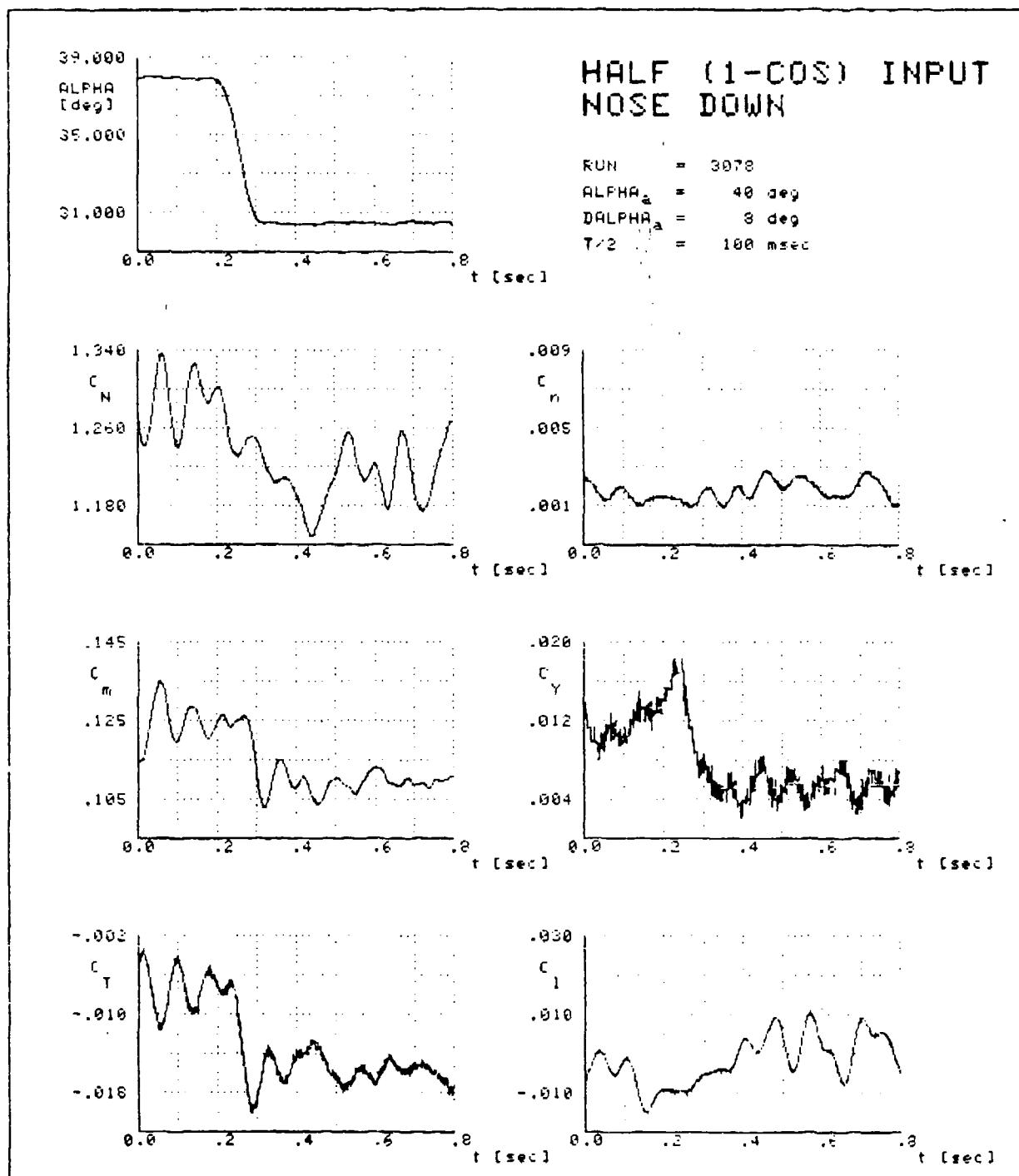


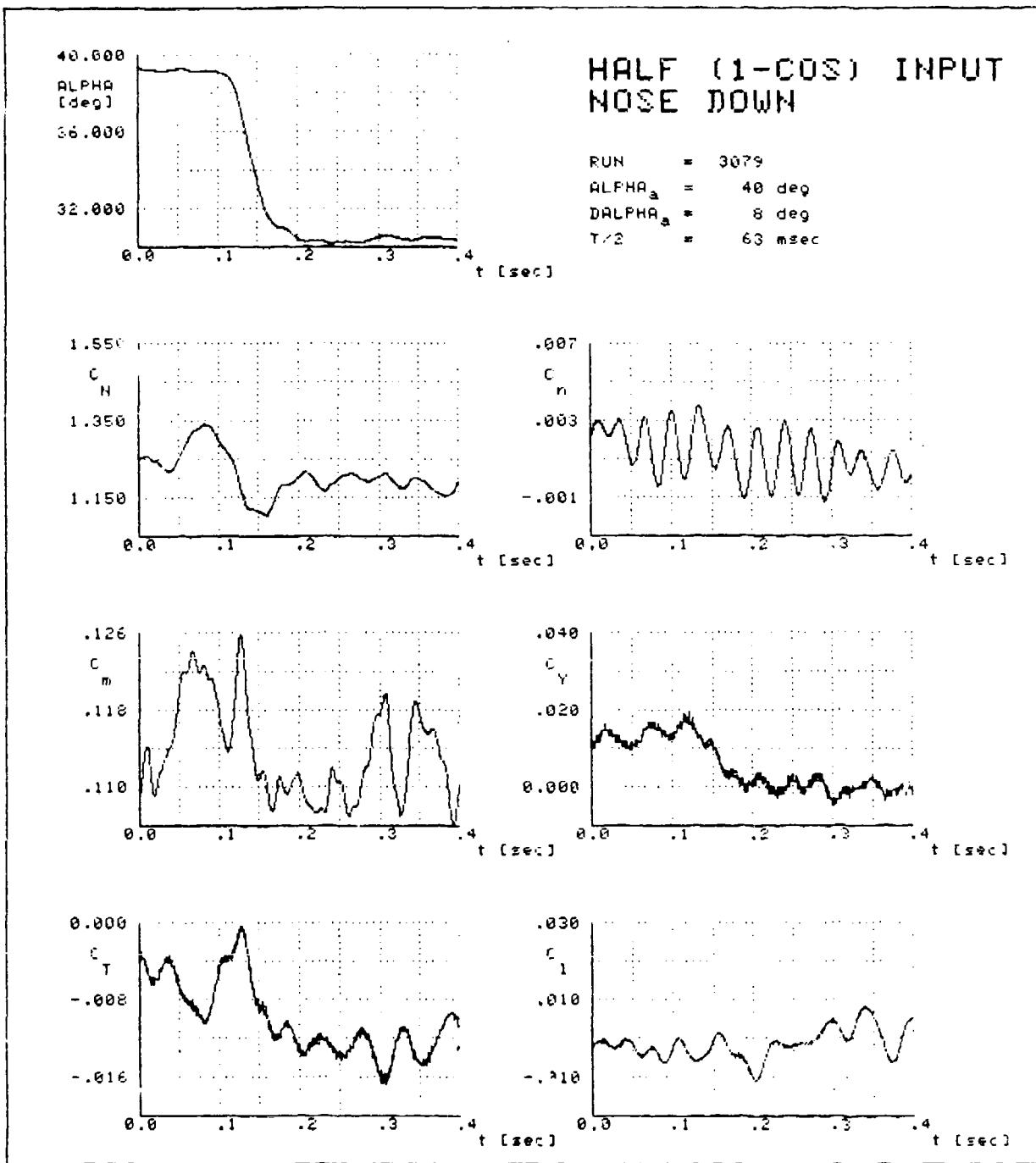
HALF (1-COS) INPUT NOSE DOWN

RUN = 3976
ALPHA_a = 40 deg
DALPHA_a = 8 deg
T/2 = 167 msec



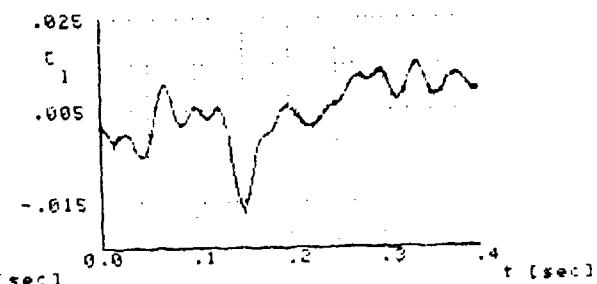
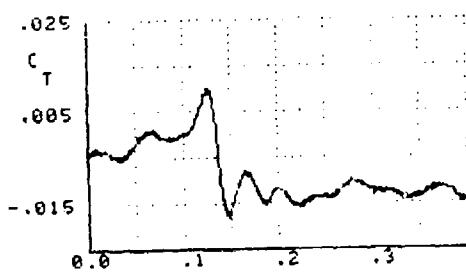
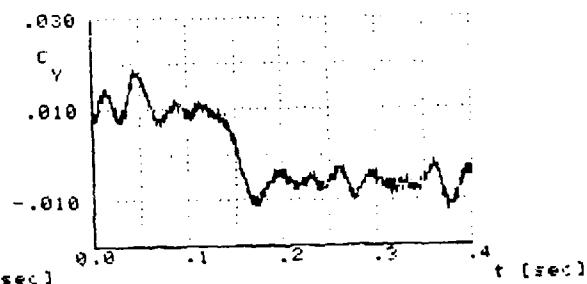
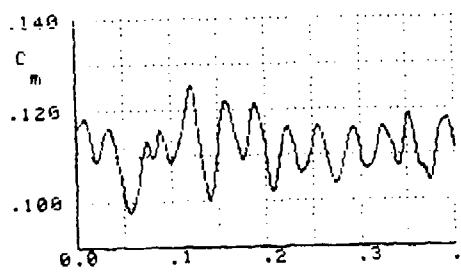
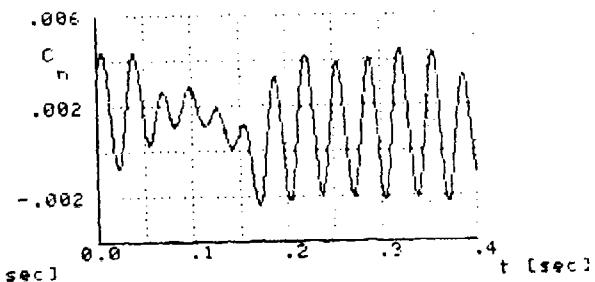
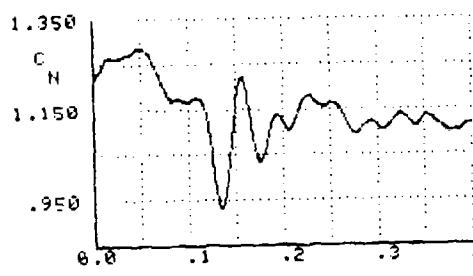
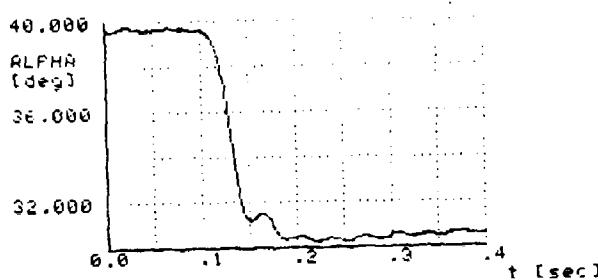




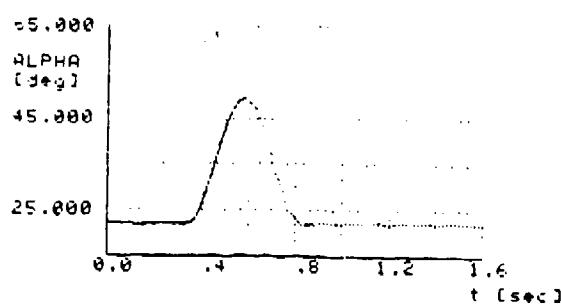


HALF (1-COS) INPUT
NOSE DOWN

RUN = 3080
 ALPHA_a = 40 deg
 DALPHA_a = 8 deg
 $T/2$ = 42 msec

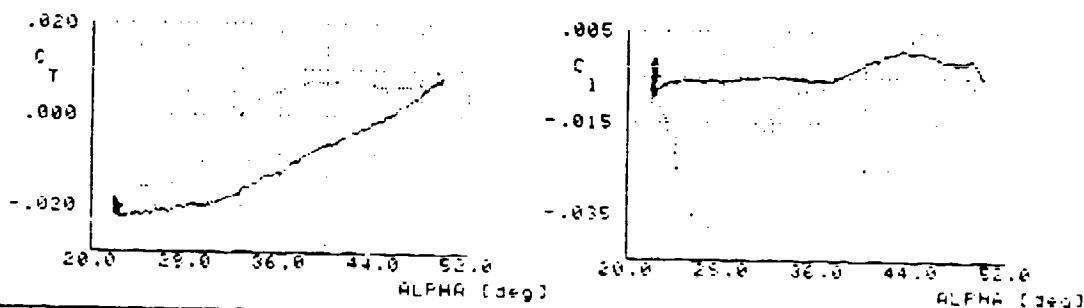
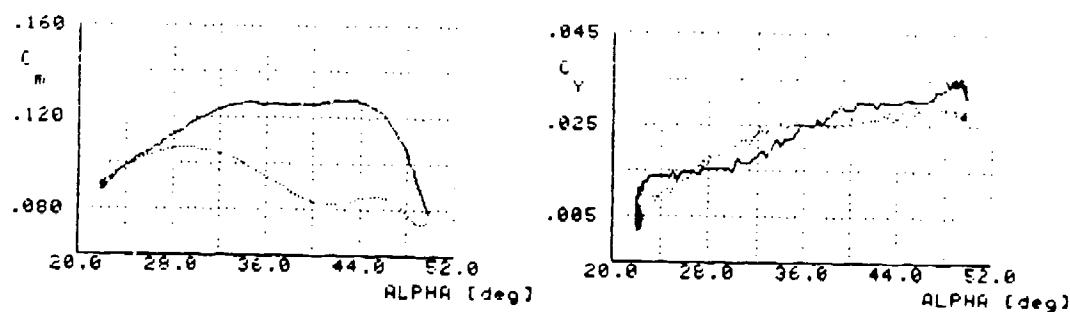
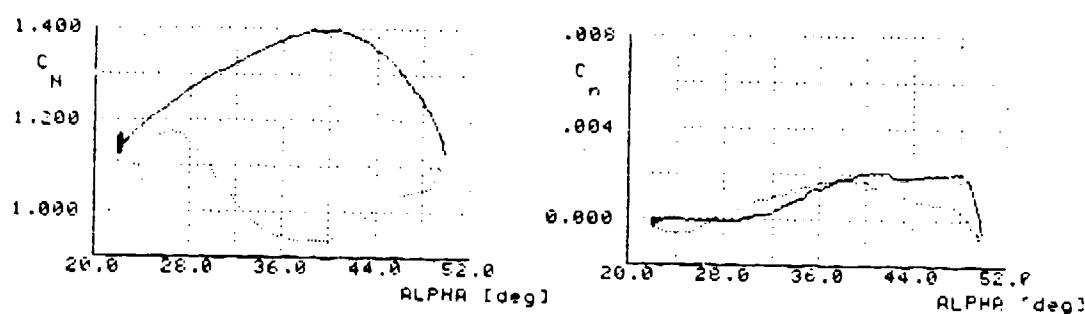


C1



(1-COS) INPUT

RUN = 3026
 α_0 = 22 deg
 $\Delta\alpha_a$ = 32 deg
T = 500 msec



FIRST INPUT

C2

65.000

ALPHA
[deg]

45.000

25.000

0.000

0.0 .4 .8 1.2 1.6

t [sec]

(1-COS) INPUT

RUN = 3028

ALPHA_a = 22 deg

DALPHA_a = 32 deg

T = 500 msec

1.900

C
N

1.500

1.100

0.700

0.300

-0.100

-0.500

-0.900

-1.300

-1.700

-2.100

-2.500

-2.900

-3.300

-3.700

-4.100

-4.500

-4.900

-5.300

-5.700

-6.100

-6.500

-6.900

-7.300

-7.700

-8.100

-8.500

-8.900

-9.300

-9.700

-10.100

-10.500

-10.900

-11.300

-11.700

-12.100

-12.500

-12.900

-13.300

-13.700

-14.100

-14.500

-14.900

-15.300

-15.700

-16.100

-16.500

-16.900

-17.300

-17.700

-18.100

-18.500

-18.900

-19.300

-19.700

-20.100

-20.500

-20.900

-21.300

-21.700

-22.100

-22.500

-22.900

-23.300

-23.700

-24.100

-24.500

-24.900

-25.300

-25.700

-26.100

-26.500

-26.900

-27.300

-27.700

-28.100

-28.500

-28.900

-29.300

-29.700

-30.100

-30.500

-30.900

-31.300

-31.700

-32.100

-32.500

-32.900

-33.300

-33.700

-34.100

-34.500

-34.900

-35.300

-35.700

-36.100

-36.500

-36.900

-37.300

-37.700

-38.100

-38.500

-38.900

-39.300

-39.700

-40.100

-40.500

-40.900

-41.300

-41.700

-42.100

-42.500

-42.900

-43.300

-43.700

-44.100

-44.500

-44.900

-45.300

-45.700

-46.100

-46.500

-46.900

-47.300

0.000

-0.100

-0.200

-0.300

-0.400

-0.500

-0.600

-0.700

-0.800

-0.900

-1.000

-1.100

-1.200

-1.300

-1.400

-1.500

-1.600

-1.700

-1.800

-1.900

-2.000

-2.100

-2.200

-2.300

-2.400

-2.500

-2.600

-2.700

-2.800

-2.900

-3.000

0.000

-0.100

-0.200

-0.300

-0.400

-0.500

-0.600

-0.700

-0.800

-0.900

-1.000

-1.100

-1.200

-1.300

-1.400

-1.500

-1.600

-1.700

-1.800

-1.900

-2.000

-2.100

-2.200

-2.300

-2.400

-2.500

-2.600

-2.700

-2.800

-2.900

-3.000

-3.100

-3.200

-3.300

-3.400

-3.500

-3.600

-3.700

-3.800

-3.900

-4.000

-4.100

-4.200

-4.300

-4.400

-4.500

-4.600

-4.700

-4.800

-4.900

-5.000

-5.100

-5.200

-5.300

-5.400

-5.500

-5.600

-5.700

-5.800

-5.900

-6.000

-6.100

-6.200

-6.300

-6.400

-6.500

-6.600

-6.700

-6.800

-6.900

-7.000

-7.100

-7.200

-7.300

-7.400

-7.500

-7.600

-7.700

-7.800

-7.900

-8.000

-8.100

-8.200

-8.300

-8.400

-8.500

-8.600

-8.700

-8.800

-8.900

-9.000

-9.100

-9.200

-9.300

-9.400

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-9.600

-9.700

-9.800

-9.900

-10.000

-10.100

-10.200

-10.300

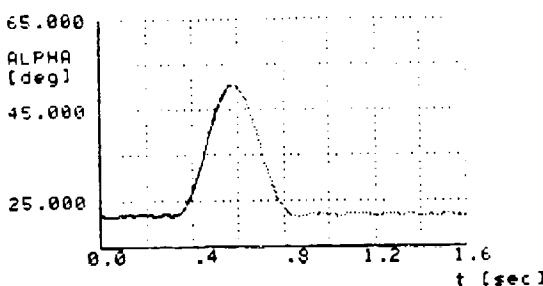
-10.400

-10.500

-10.600

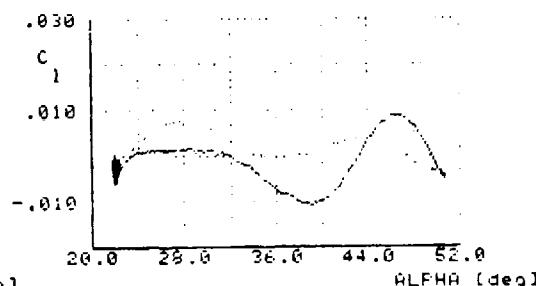
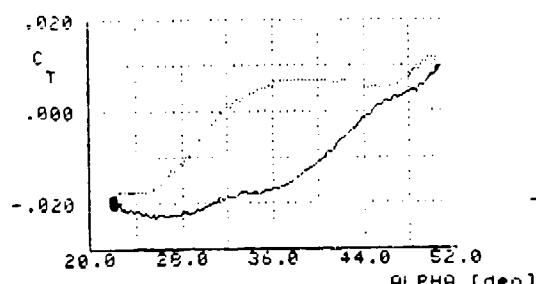
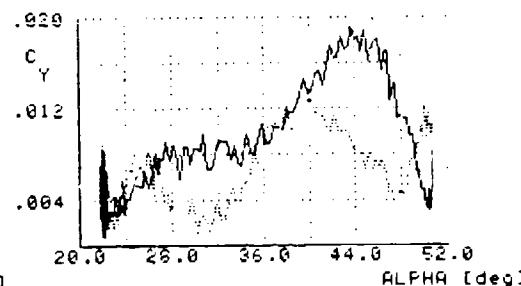
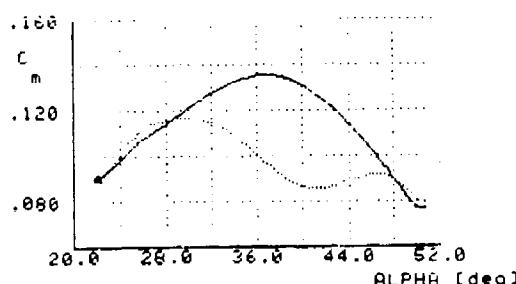
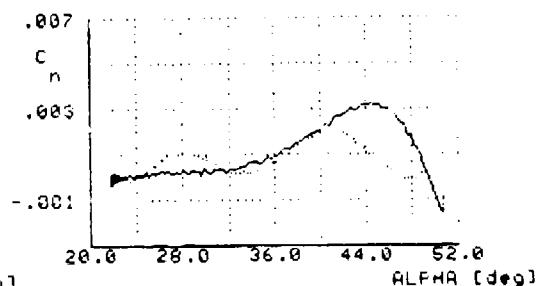
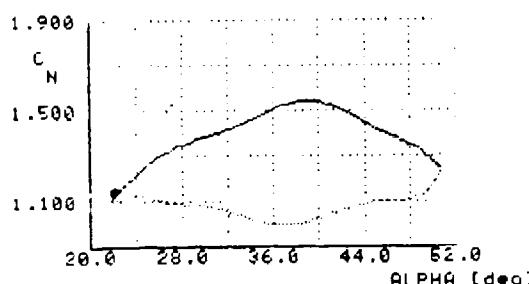
-10.700

C3



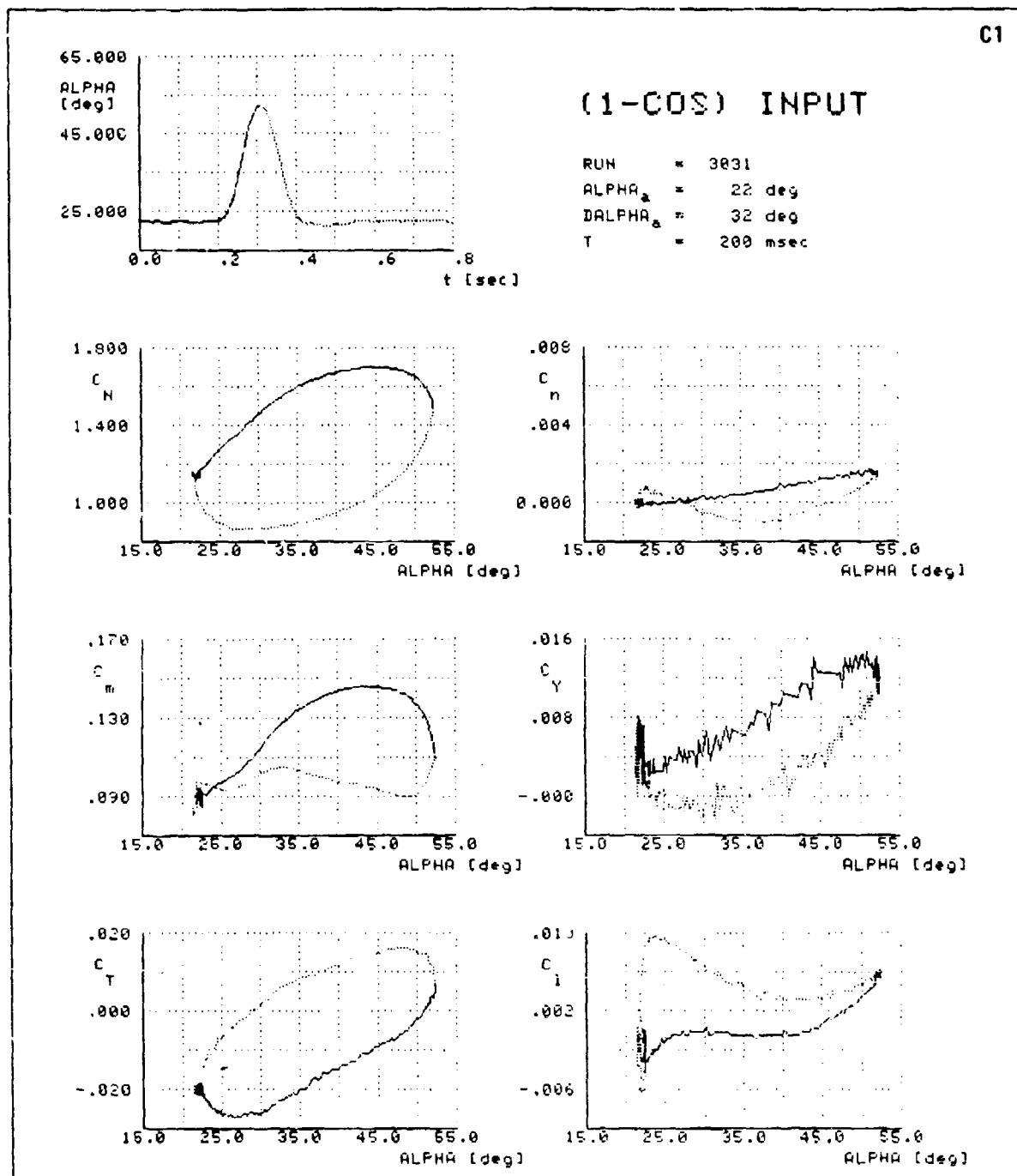
(1-COS) INPUT

RUN = 3028
 $\text{ALPHA}_a = 22$ deg
 $\Delta\text{ALPHA}_a = 32$ deg
 $T = 500$ msec



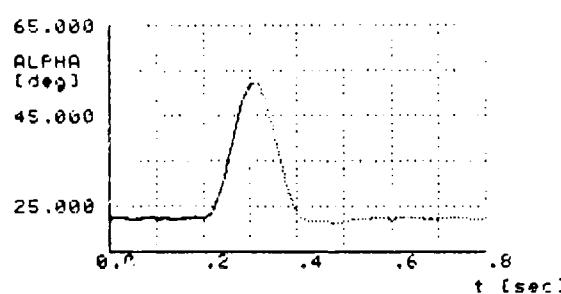
THIRD INPUT

C1



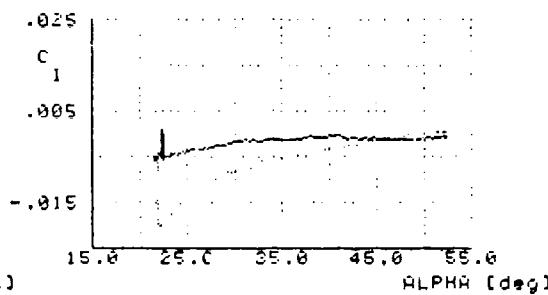
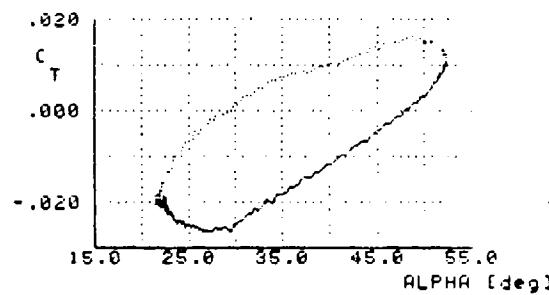
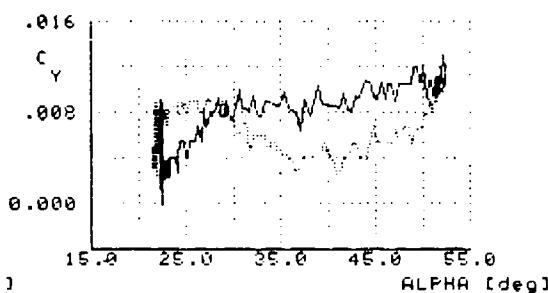
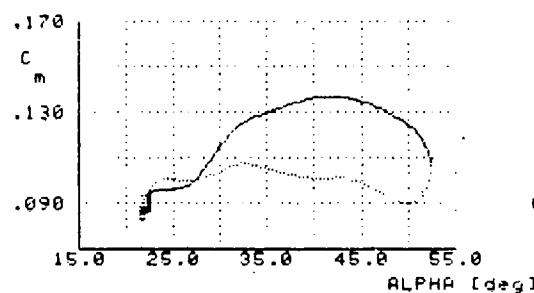
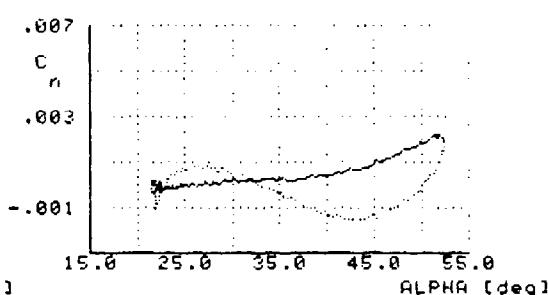
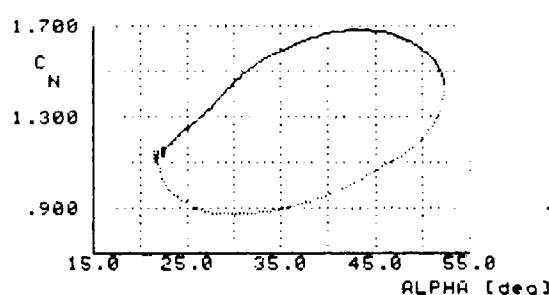
FIRST INPUT

C2



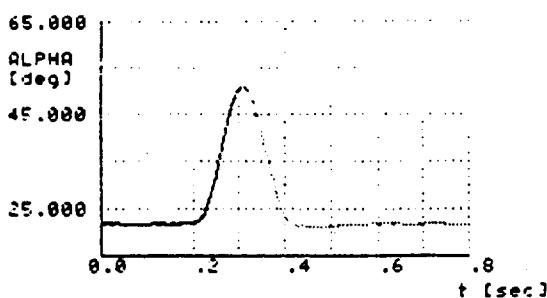
(1-COS) INPUT

RUN = 3031
ALPHA_a = 22 deg
DALPHA_a = 32 deg
T = 200 msec



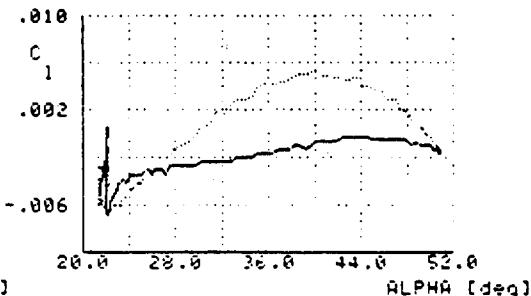
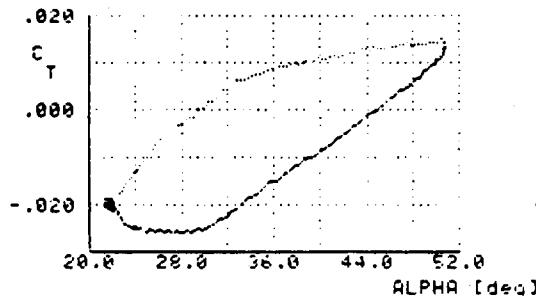
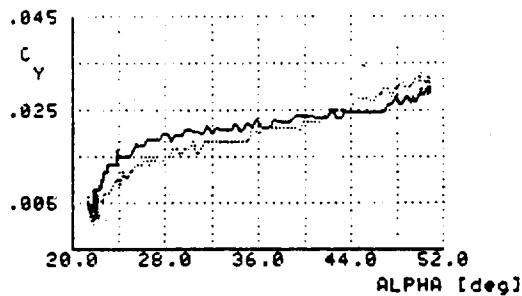
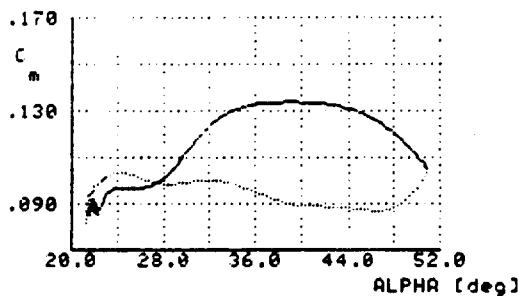
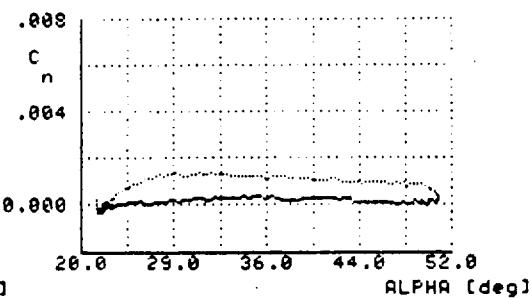
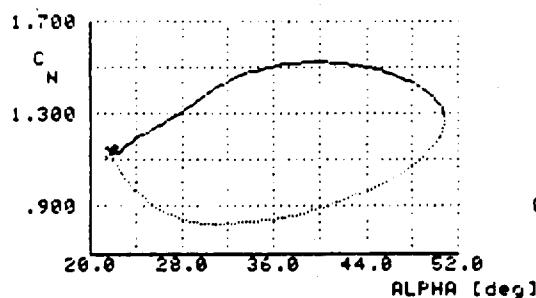
SECOND INPUT

C3



(1-COS) INPUT

RUN = 3031
 $\text{ALPHA}_a = 22 \text{ deg}$
 $\text{DALPHA}_a = 32 \text{ deg}$
 $T = 200 \text{ msec}$



THIRD INPUT